

*Regional Cooperation for  
Limited Area Modeling in Central Europe*



A Consortium for COnvection-scale modelling  
Research and Development

# Setting dynamics options in VHR

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Czech  
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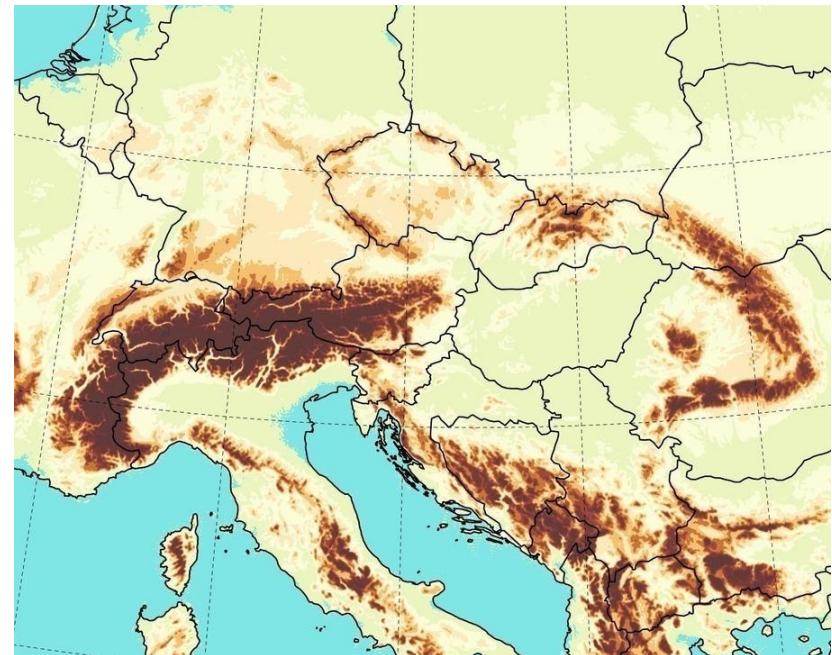


ARSO METEO  
Slovenia

# Basic choices

Set already during the preparation of clim files or PGD:

- ▶ Points in x: NDLON -> NDLUX=NDLON-11 (without extension zone)  
Points in y: NDGL -> NDGUX=NDGL-11
- ▶ Truncation in x: NMSMAX  
in y: NSMAX
- ▶ Coupling zone half-width in x: NBZONL  
in y: NBZONG
- ▶ Horizontal resolution in x: EDELX  
in y: EDELY
- ▶ Central point: ELATC, ELONC
- ▶ Projection reference point: ELATO, ELONO
- ▶ Vertical levels through As and Bs



# Time scheme

- ▶ Semi-implicit or iterative centered implicit scheme

$$\frac{R_F^{+(0)} - R_{O^{(0)}}^0}{\Delta t} = \mathcal{L} \left( \frac{R_F^{+(0)} + R_{O^{(0)}}^0}{2} \right) + (\mathcal{M} - \mathcal{L}) \left( R_M^{m(0)} \right)$$

$$\frac{R_F^{+(n)} - R_{O^{(n)}}^0}{\Delta t} = \mathcal{L} \left( \frac{R_F^{+(n)} + R_{O^{(n)}}^0}{2} \right) + (\mathcal{M} - \mathcal{L}) \left( R_M^{m(n)} \right)$$

- ▶ How many times the Helmholtz equation is being solved? n times

$$\left( 1 - \frac{\Delta t}{2} \mathcal{L} \right) R_F^{+(n)} = \left( 1 + \frac{\Delta t}{2} \mathcal{L} \right) R_{O^{(n)}}^0 + (\mathcal{M} - \mathcal{L}) \left( R_M^{m(n)} \right)$$

**NSITER=0,1,2,3**  
**corresponds to last n**

**LPC\_FULL=T for NSITER>0**  
**LPC\_CHEAP=T for**

$$O^{(n)} = O^{(0)}$$

# Time scheme

- ▶ How  $R_M^{m(0)}$ ,  $R_M^{(n)}$  is calculated?
- ▶ Extrapolating scheme SETTLS or non-extrapolating scheme NESC may be applied:

$$R_M^{m(0)} = \frac{R_F^0 + R_O^0}{2}$$

$$R_M^{m(0)} = \frac{R_F^0 + 2R_O^0 - R_O^-}{2}$$

$$R_M^{m(n)} = \frac{R_F^{+(n-1)} + R_O^0}{2}$$

- ▶ Similar choice is done for the calculation of the semi-Lagrangian trajectory:
  - ▶ in horizontal
  - ▶ in vertical
  - ▶ trajectory search is also iterative with NITMP iterations, one iteration ~1%CPU

**LSETTLS=T & LNESC=F**

or

**LSETTLS=F & LNESC=T**

**LSETTSLT=T & LNESCT=F**

**LSETTLSV=T & LNESCV=F**

or the opposite

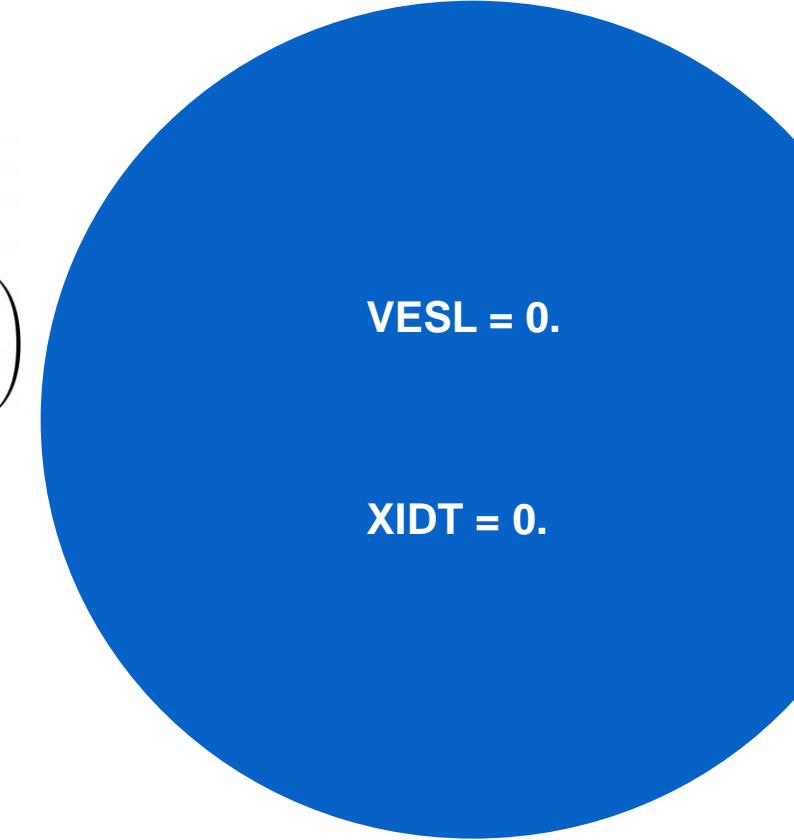
**NITMP = 3, 4, 5, ...**

# Time scheme decentering

- ▶ First order decentering: VESL

$$\begin{aligned}\frac{R_F^{+(n)} - R_O^0}{\Delta t} &= \mathcal{L} \left( \frac{(1 + \epsilon)R_F^{+(n)} + (1 - \epsilon)R_O^0}{2} \right) \\ &\quad + (\mathcal{M} - \mathcal{L}) \left( \frac{(1 + \epsilon)R_F^{+(n-1)} + (1 - \epsilon)R_O^0}{2} \right)\end{aligned}$$

- ▶ Pseudo-second order decentering: XIDT
  - for linear terms only
- ▶ Brings more stability, but less accuracy



# Time scheme

- ▶ Stability/efficiency trade-off:

Time scheme price depends on the number of iterations of the time scheme,  
the chosen complexity of the time scheme and the chosen time step

- ▶ Iterative schemes (PC): NSITER iterations

Helmholtz solver – iterated

spectral transformations – iterated

trajectory search – not iterated for LPC\_CHEAP=T

SL interpolations – not iterated for LPC\_CHEAP=T

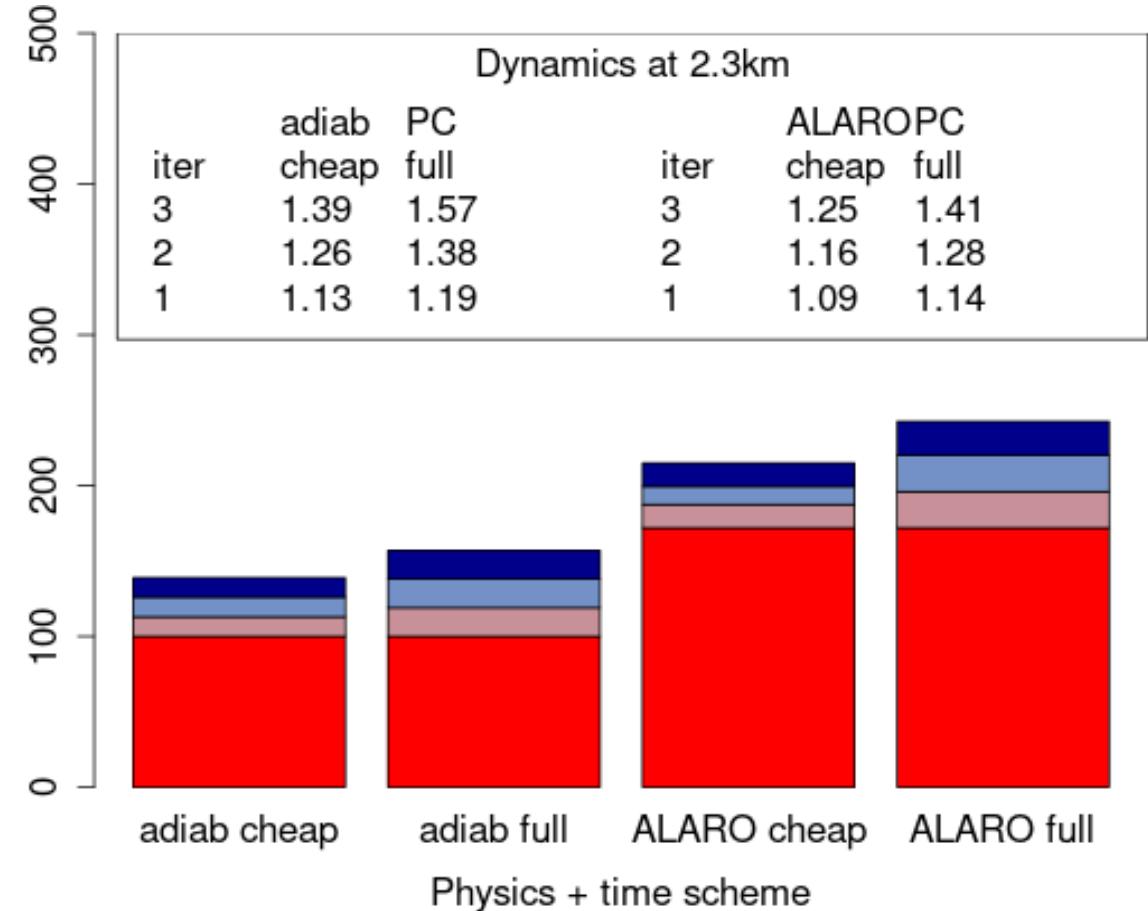
horizontal diffusion – not iterated for LRHDI\_LASTITERPC=T (default)

physics – not iterated

# Time scheme

- ▶ Stability/efficiency trade-off:

1 iteration of PC CHEAP  
needs only about 10% of  
additional CPU time when  
compared to ALARO run



# Linear model definition

- ▶ Reference temperature:

$$\text{SITR} = 350\text{K}$$

$$\text{SITRA} \leq 100\text{K}$$

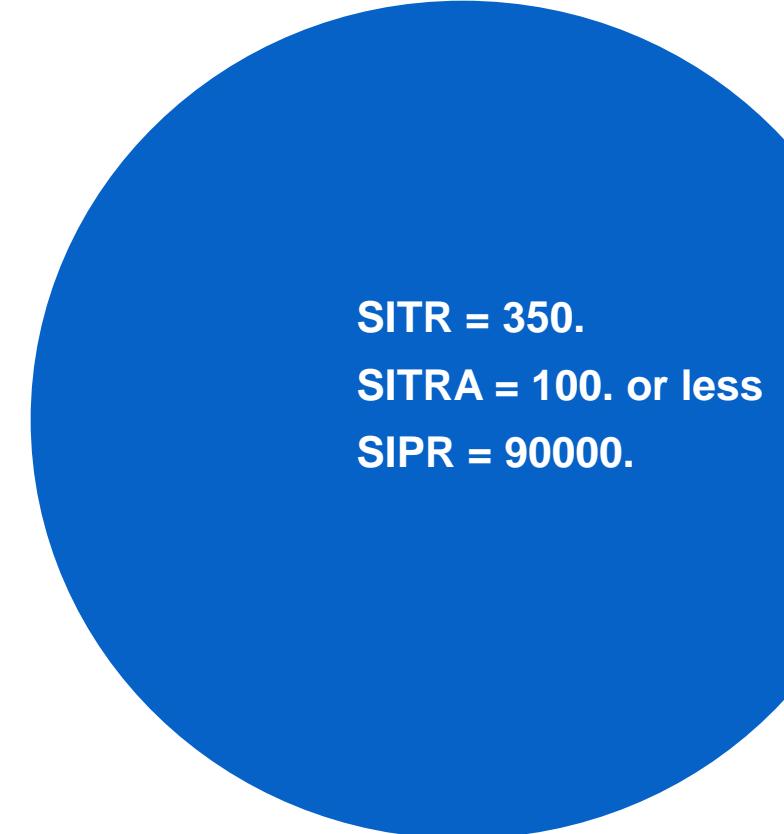
Bénard: The 2TL scheme for the EE systém is stable if

$$\text{SITRA} < T < \text{SITR}$$

everywhere in the domain.

- ▶ Reference pressure:

relatively high SIPR recommended



# Spectral diffusion

$$\left( \frac{dX}{dt} \right)_{HD} = -\mathcal{K}_X M \nabla^r X$$
$$\mathcal{K}_X = \Omega_X \cdot g(l) \cdot f(n, N, \dots)$$

- ▶ Order r = REXPDH
- ▶ Strength

$$\Omega_X = \frac{RDXTAU}{RDAMPX} \left( 1 + \frac{i}{2} \right)^{2.5} [\Delta X]_{GP}$$

- ▶ Vertical profile

$$g(l) = \min(SLEVDH \frac{\pi_{ref}}{\pi_{st}(l)}, \frac{1}{SLEVDH3}) - s_{dred}$$

with NPROFILEHD=1-3

in listing under PDILEV=...

**REXPDH = 4.**

**RDAMPX = 1. (smaller->stronger)**

**RRDXTAU = 123. (bigger-> stronger)**

**SDRED = 0.**

**SLEVDH = 1.**

**SLEVDH3 = 100./VP00**

**NPROFILEHD = 3**

# Spectral diffusion

$$\left( \frac{dX}{dt} \right)_{HD} = -\mathcal{K}_X M \nabla^r X$$

$$\mathcal{K}_X = \Omega_X \cdot g(l) \cdot f(n, N, \dots)$$

- ▶ Order r = REXPDH
- ▶ Strength

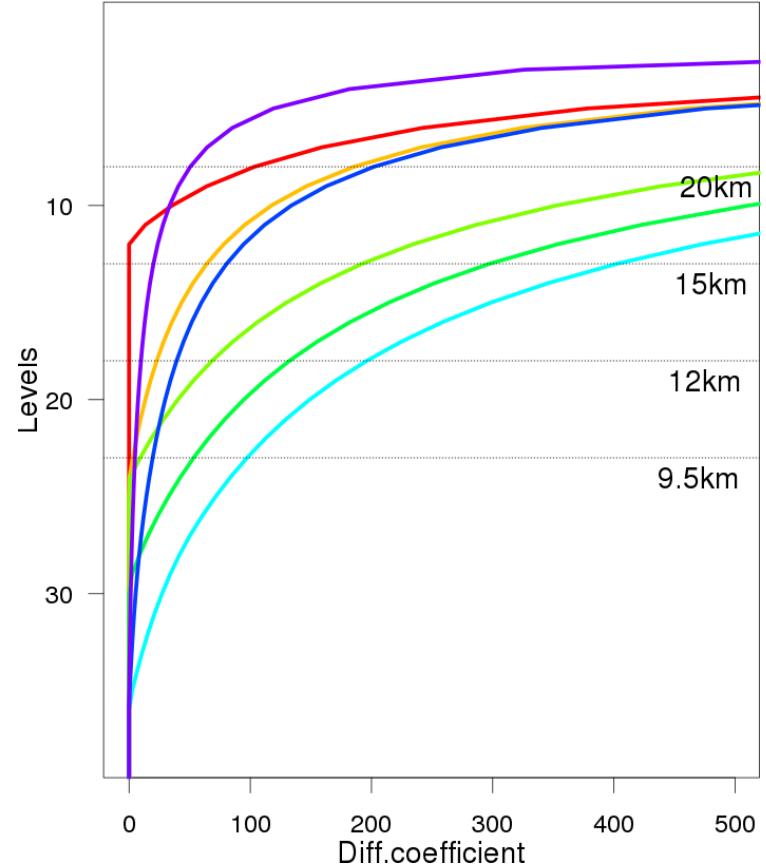
$$\Omega_X = \frac{RDXTAU}{RDAMPX} \left( 1 + \frac{i}{2} \right)^{2.5} [\Delta X]_{GP}$$

- ▶ Vertical profile

$$g(l) = \min(SLEV DH \frac{\pi_{ref}}{\pi_{st}(l)}, \frac{1}{SLEV DH 3}) - s_{dred}$$

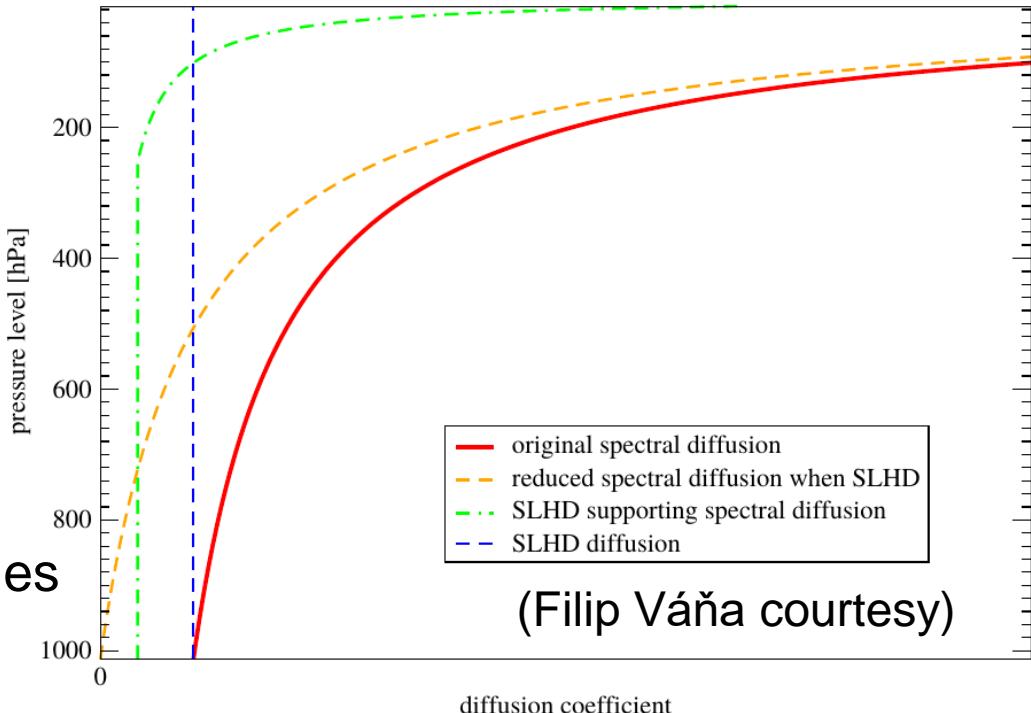
with NPROFILEHD=1-3

in listing under PDILEV=...



- ▶ Still spectral diffusion is needed, even two kinds:
  - ▶ reduced spectral diffusion
    - ▶ Order
    - ▶ Strength
    - ▶ Vertical profile
  - ▶ supporting spectral diffusion
    - ▶ Order
    - ▶ Strength
    - ▶ Vertical profile
- ▶ May be applied on grid point variables (GFL) as well

Vertical profile of horizontal diffusions in ALADIN



- ▶ Still spectral diffusion is needed, even two kinds:
  - ▶ reduced spectral diffusion
    - ▶ Order
    - ▶ Strength
    - ▶ Vertical
  - ▶ supporting spectral diffusion
    - ▶ Order
    - ▶ Strength
    - ▶ Vertical profile
- ▶ May be applied on grid point variables (GFL) as well

**REXPDH=2.**

**RDAMPX=...**

**SLEVDH=0.5**

**SDRED=1.**

**In listing in PDILEV\_SLHD**

**REXPDHS=6.**

**RDAMPXS=...**

**SLEVDHS = 1.**

**in listing in PDILEVS**

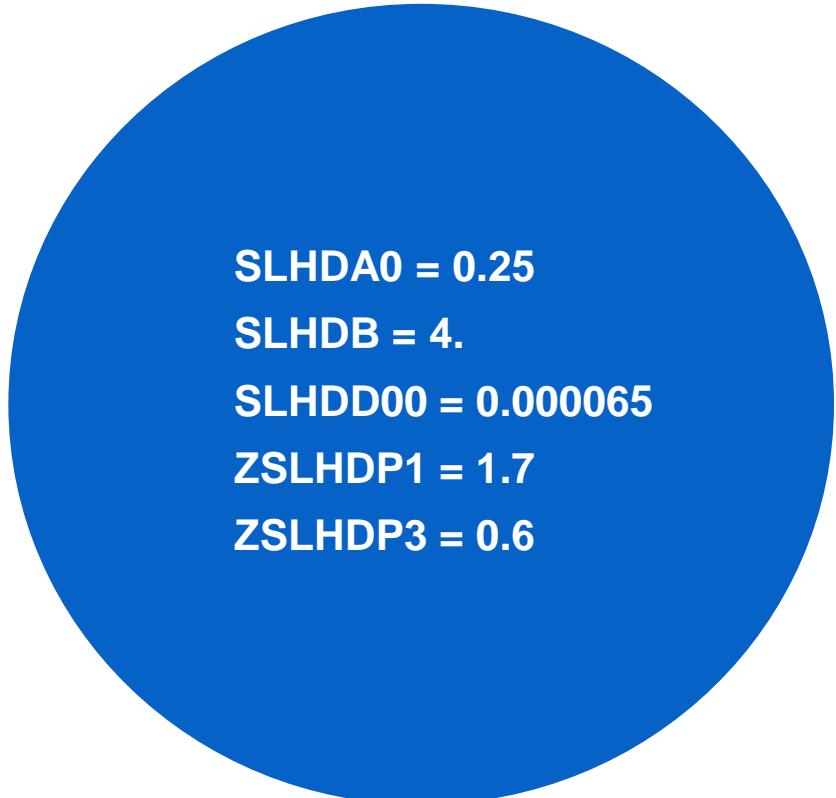
- ▶ Flow dependent diffusion coefficient kappa:

$$f(d) = a \cdot d \left( \max \left[ 1, \frac{d}{d_0} \right] \right)^{SLHDB}$$

$$a = 2 \cdot SLHDA0 \left( \frac{\Delta x_{ref}}{\Delta x} \right)^{ZSLHDP1}$$

$$d_0 = 0.5 \cdot SLHDD00 \left( \frac{\Delta x_{ref}}{\Delta x} \right)^{ZSLHDP3}$$

$$\kappa = \frac{f(d)\Delta t}{1 + f(d)\Delta t}$$



- ▶ SL interpolations according to kappa  
=> controlled diffusivity

# Vertical motion variable

- ▶ Modified vertical divergence in linear part

$$d_4 = \underbrace{-g \frac{p}{mRT} \frac{\partial w}{\partial \eta}}_{d_3} + \underbrace{\frac{p}{mRT} \nabla \phi \frac{\partial V}{\partial \eta}}_X$$

- ▶ Modified vertical velocity in non-linear part

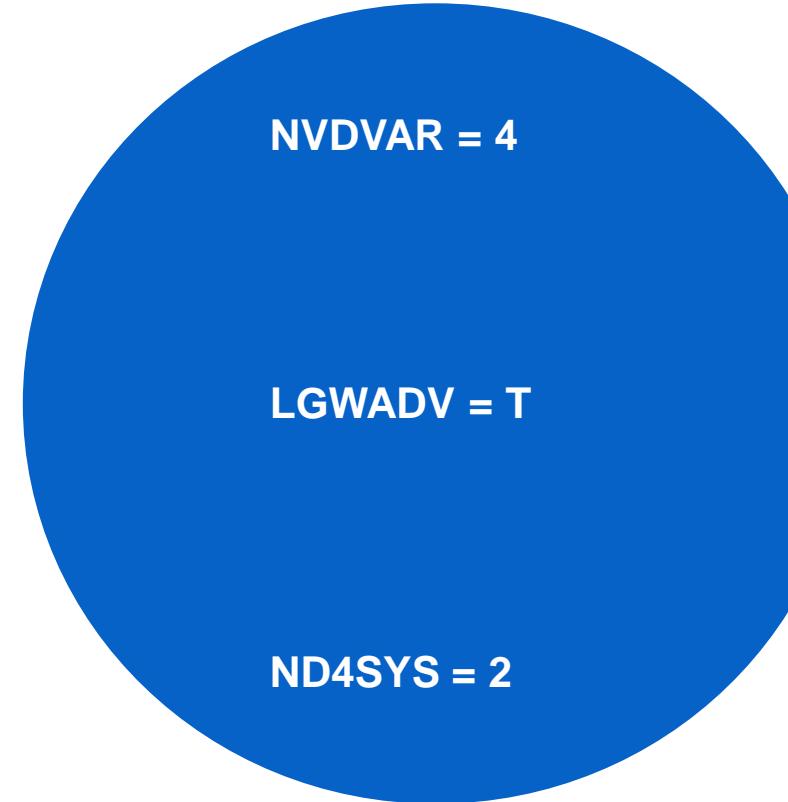
$$w = w_S + \frac{1}{g} \int_{\eta}^1 \frac{mRT}{p} (d_4 - X) d\eta$$

- ▶ X-term treatment  $\frac{dd_4}{dt} = \frac{dd_3}{dt} + \frac{dX}{dt}$

$$ND4SYS = 1 : \quad \frac{dX}{dt} = \frac{X_M^m - X_O^0}{\Delta t} \quad \text{iterated}$$

$$ND4SYS = 2 : \quad \frac{dX}{dt} = \frac{X_F^{+0} - X_F^0}{\Delta t} + \frac{X_F^0 - X_O^0}{\Delta t}$$

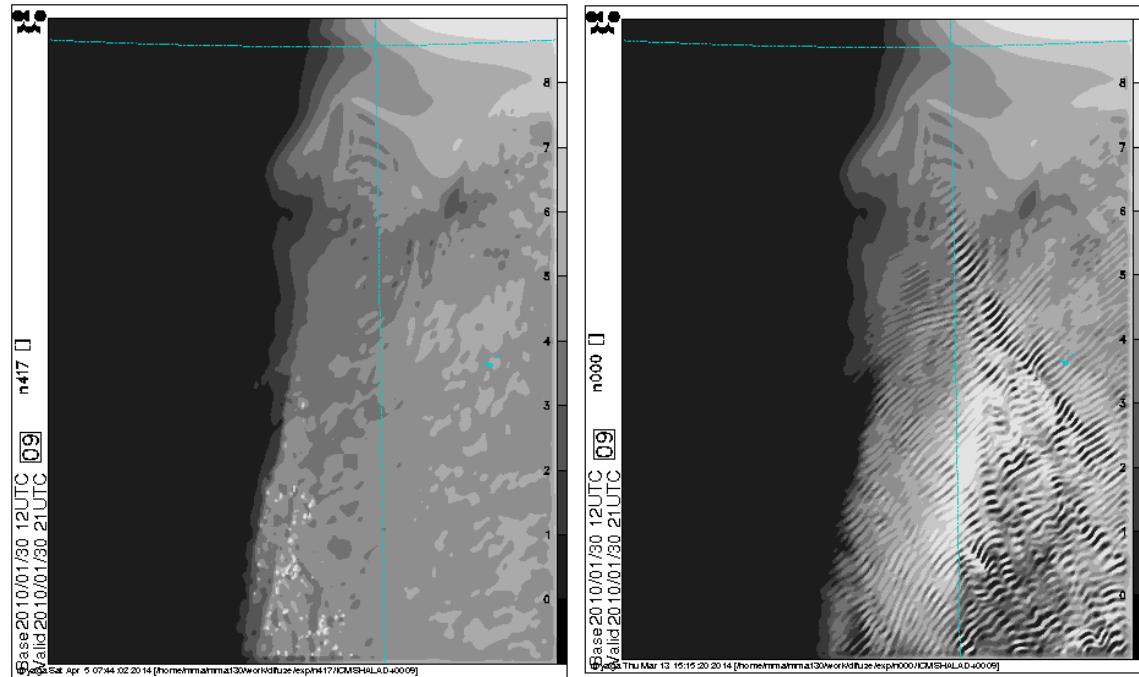
last corrector      iterated



# Vertical motion variable

- ▶ Using only d3 (NVDVAR=3) is less stable and potentially dangerous
- ▶ Using only d variable (LGWADV = F) is dangerous, even with LRDBBC=T; this piece of code is not maintained

Cloudiness with d4 and d3



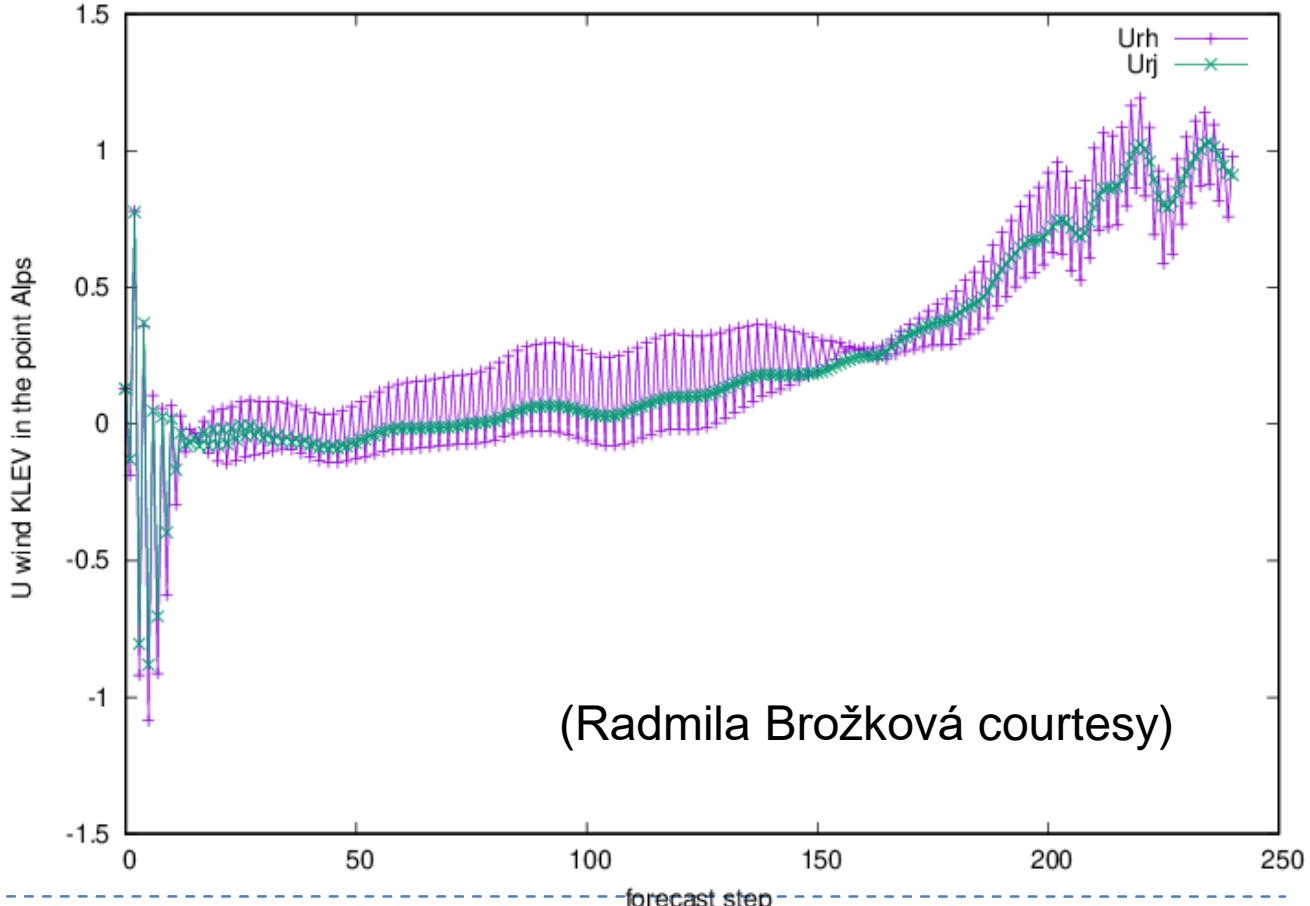
# Vertical motion variable

- ▶ Using ND4SYS = 1 is dangerous:

**ND4SYS = 1**

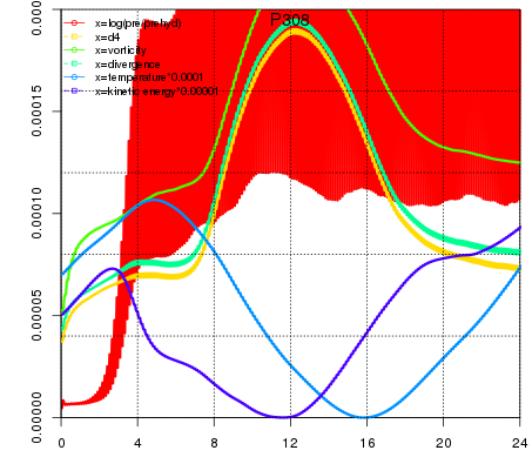
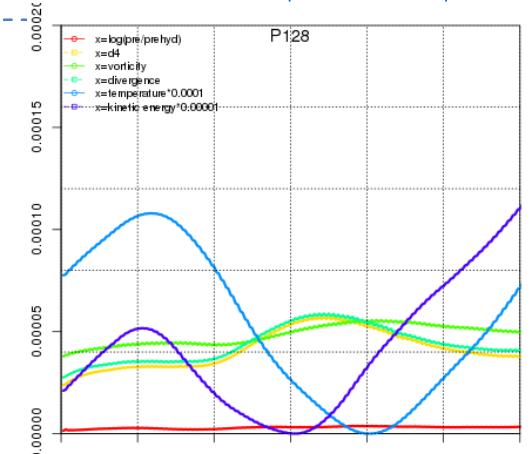
**ND4SYS = 2**

- ▶ Time evolution of U -wind at the surface at one grid point in Alps



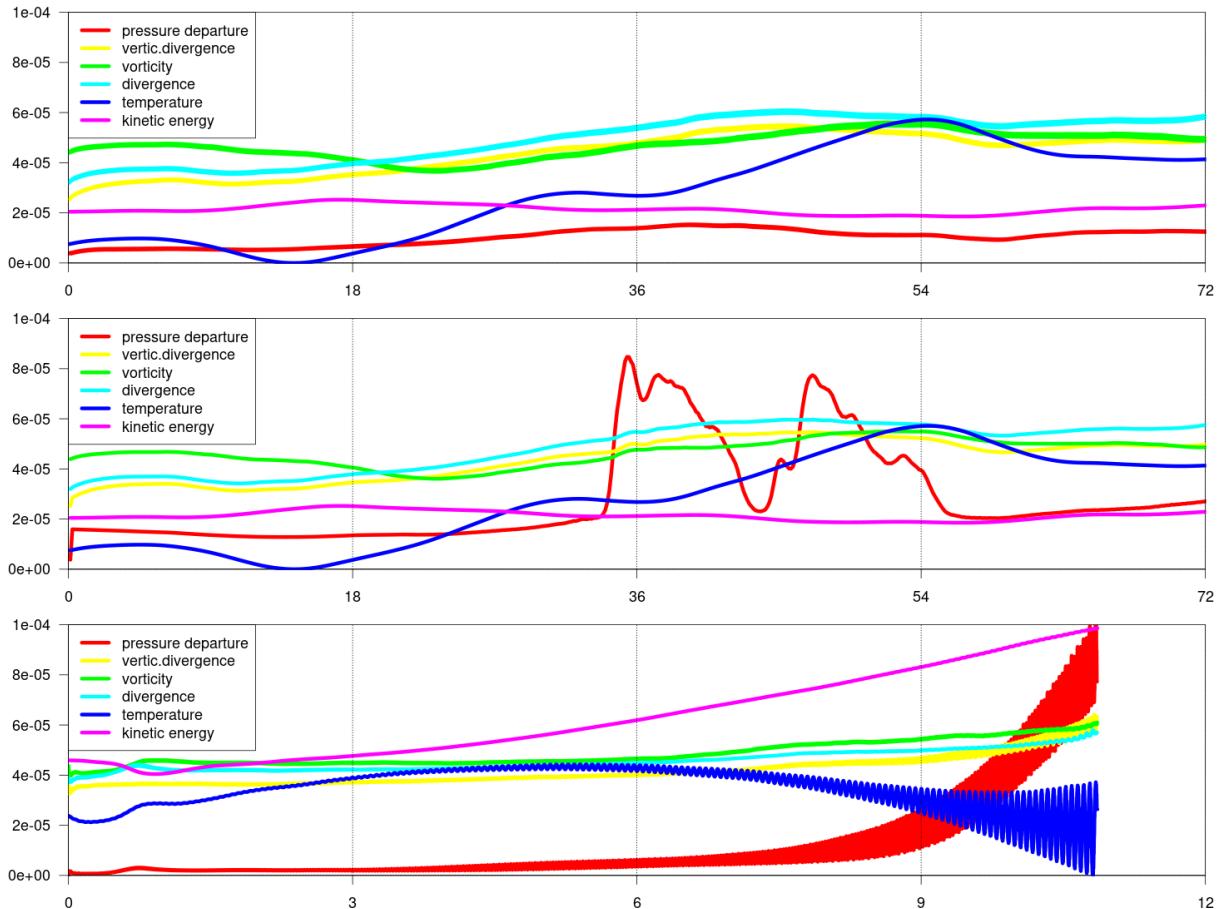
# Tests of the new configuration

- 1) temporal evolution of spectral norms
- 2) kinetic energy spectra and vertical velocity spectra
- 3) visualization of some fields (vertical velocity, precipitation)
- 4) objective scores (RMSE, BIAS, STDE)
  - compared to previous operational results



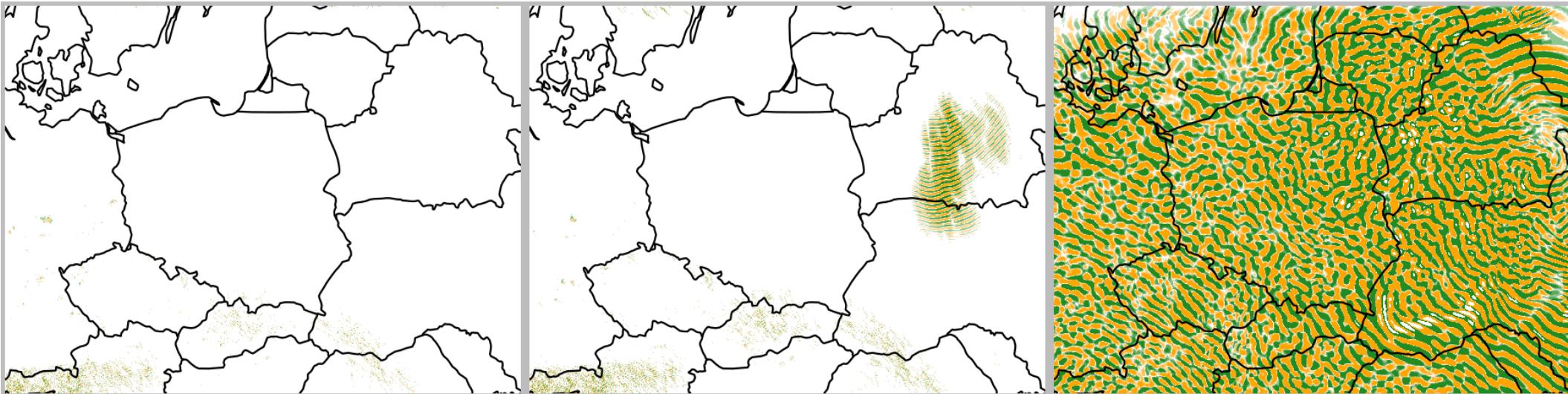
# How to detect problems

## ▶ Evolution of spectral norms



# How to detect problems

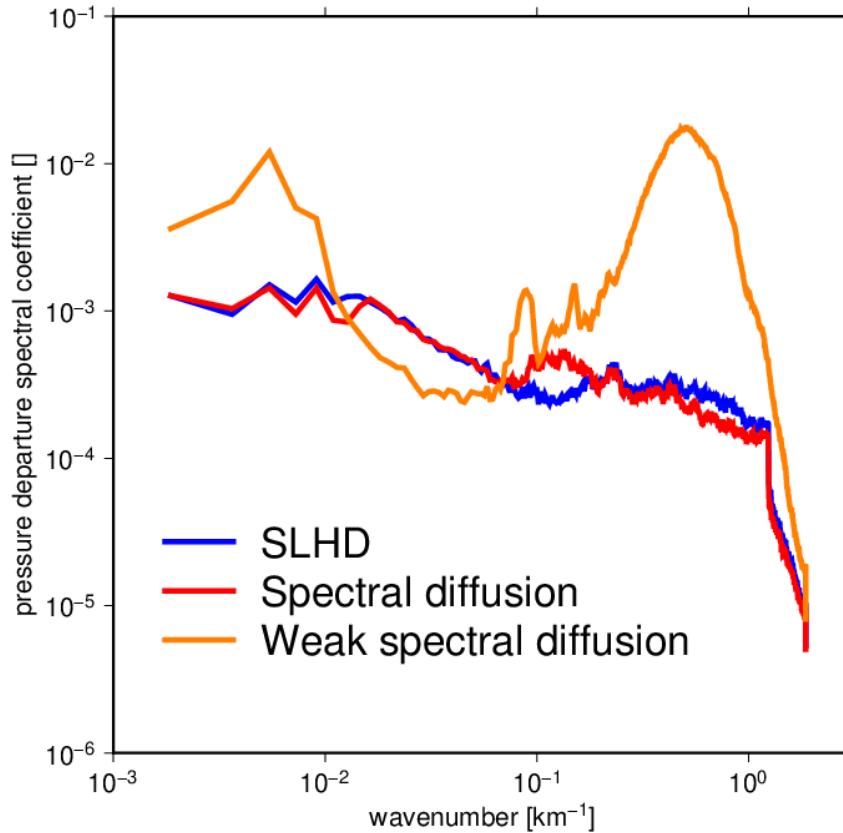
- ▶ Check some arrays



- ▶ Pressure departure at 20 hPa

# How to detect problems

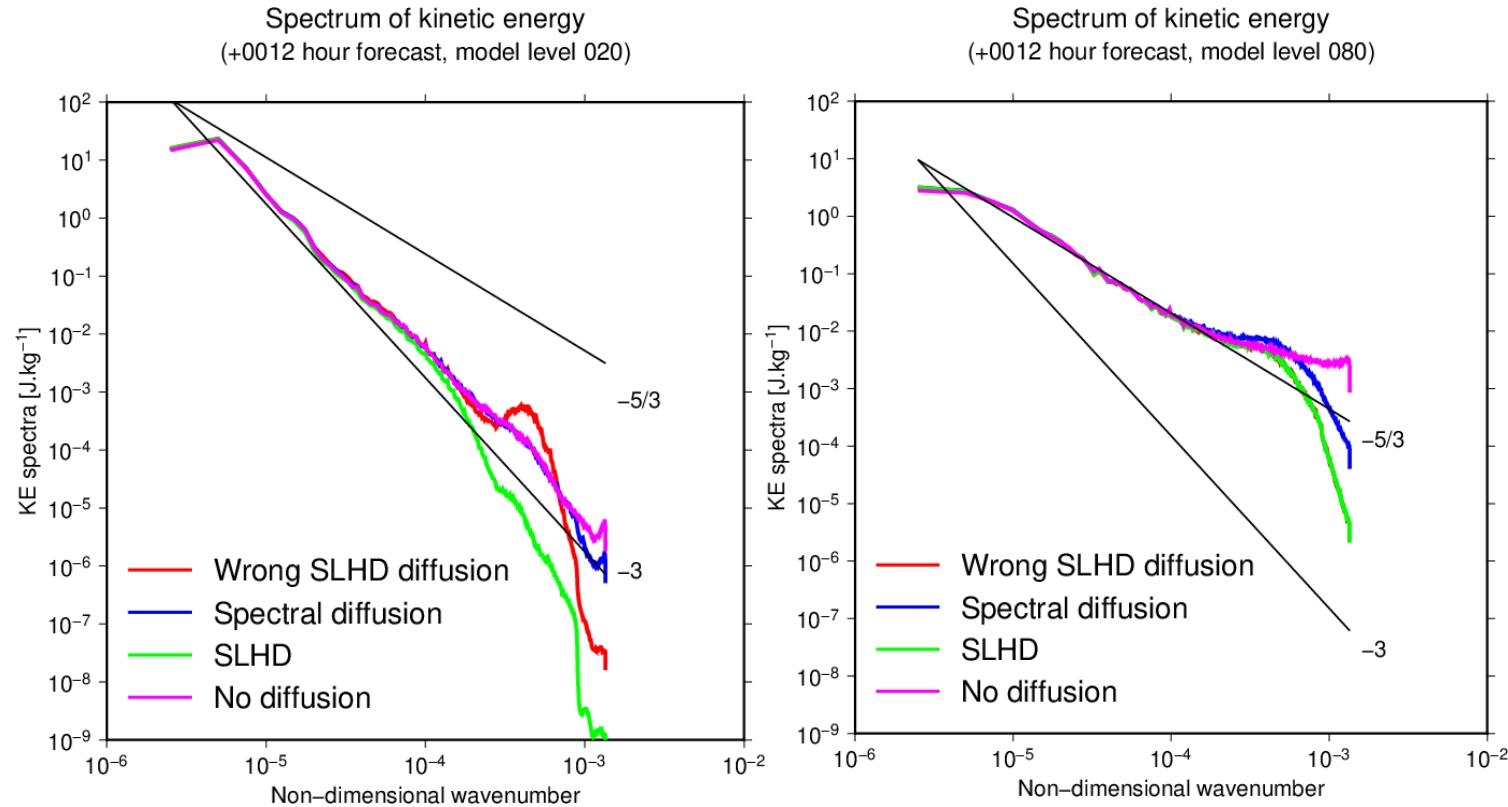
- ▶ Arrays spectra



- ▶ Pressure departure at 20 hPa

# How to detect problems

## ► Kinetic energy spectra



# Summary – an example with SLHD

## &NAMDYN

LADVF=.T.,  
LQMXX=.F.,  
SIPR=90000.,  
SITR=350.,  
SITRA=100.,  
NSITER=2,  
NSPDLAG=3,  
NSVLAG=3,  
NTLAG=3,  
NVLAG=3,  
NWLAG=3,  
VESL=0.,  
XIDT=0.,  
NITMP=5,  
RRDXTAU=123.,

RDAMPDIV=5.,  
RDAMPVOR=5.,  
RDAMPPD=5.,  
RDAMPQ=20.,  
RDAMPT=20.,  
RDAMPVD=20.,  
RDAMPVORS=10.,  
RDAMPDIVS=10.,  
RDAMPVDS=15.,  
REXPDH=2.,  
REXPDH=6.,  
SDRED=1.,  
SLEVDH=0.5,  
SLEVDHS=1.,

## &NAMDYNA

LGWADV=.T.,  
LRDBBC=.F.,  
LNESC=.T.,  
LSETTLS=.F.,  
LNESCT=.F.,  
LNESCV=.F.,  
LSETTLST=.T.,  
LSETTLSV=.T.,  
LPC\_FULL=.T.,  
LPC\_CHEAP=.T.,  
ND4SYS=2,  
NDLNPR=1,  
NPDVAR=2,  
NVDVAR=4,

LSLHD\_GFL=.T.,  
LSLHD\_OLD=.F.,  
LSLHD\_XX=.T.,  
SLHDEPSH=0.016,  
SLHDEPSV=0.,  
SLHDKMAX=6.,  
SLHDKMIN=-0.6,

## &NAMGFL

YXX\_NL%LPC=.T.,  
YXX\_NL%LSLHD=.T.,

XX stands for a variable

# Summary – an example without SLHD

## &NAMDYN

LADVF=.T.,  
LQMXX=.F.,  
SIPR=90000.,  
SITR=350.,  
SITRA=100.,  
NSITER=2,  
NSPDLAG=3,  
NSVLAG=3,  
NTLAG=3,  
NVLAG=3,  
NWLAG=3,  
VESL=0.,  
XIDT=0.,  
NITMP=5,  
RRDXTAU=205.,

## &NAMDYNA

RDAMPDIV=20.,  
RDAMPVOR=20.,  
RDAMPPD=20.,  
RDAMPQ=0.,  
RDAMPT=0.,  
RDAMPVD=20.,  
  
LGWADV=.T.,  
LRDBBC=.F.,  
LNESC=.T.,  
LSETTLS=.F.,  
LNESCT=.T.,  
LNESCV=.T.,  
LSETTLST=.F.,  
LSETTLSV=.F.,  
LPC\_FULL=.T.,  
LPC\_CHEAP=.F.,  
ND4SYS=2,  
NDLNPR=1,  
NPDVAR=2,  
NVDVAR=4,

SLHDEPSH=0.08,  
SLHDEPSV=0.,  
SLHDKMAX=6.,  
SLHDKMIN=-0.6,

## &NAMGFL

YXX\_NL%LPC=.T.,  
YXX\_NL%LSLHD=.F.,

XX stands for a variable

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# Thank you for your attention.

ACC  RD

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