

REPORT

Smoothing of Soil Wetness Index (SWI) in ALADIN/LACE domain

Stjepan Ivatek-Šahdan
Meteorological and Hydrological Service of Croatia
ivateks@cirus.dhz.hr

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1. Introduction

During the period 15th – 20th June 2002 Slovakian colleague Jan Masek noticed that during the day hot spots appear in 2m Temperature field (http://www.shmu.sk/aladin_lace/). They occur in flat areas, e.g. N Austria, SW Slovakia, Hungary. Hot spots do not move and they can be observed on the same place for several days. There is no corresponding pattern in 925hPa level. At these areas 2m Temperature was affected by too warm soil. The cause of hot spots problem in ALADIN/LACE is very probably the same as the cause of similar problems observed already in ARPEGE and ALADIN-France. The explanation is in the too strong horizontal variability of soil moisture in the model. The origins of this variability are multiple: long time scale evolution of total soil moisture, necessity of using switching conditions in the soil moisture analysis since the correlation's between 2m errors and soil moisture errors are mostly situation dependent.

On Figure 1, 2m Temperature field and Soil Wetness Index for June 18th 2002 15 UTC are shown, 15 hours forecast. There is good correlation between areas with high 2m Temperature and dry areas.

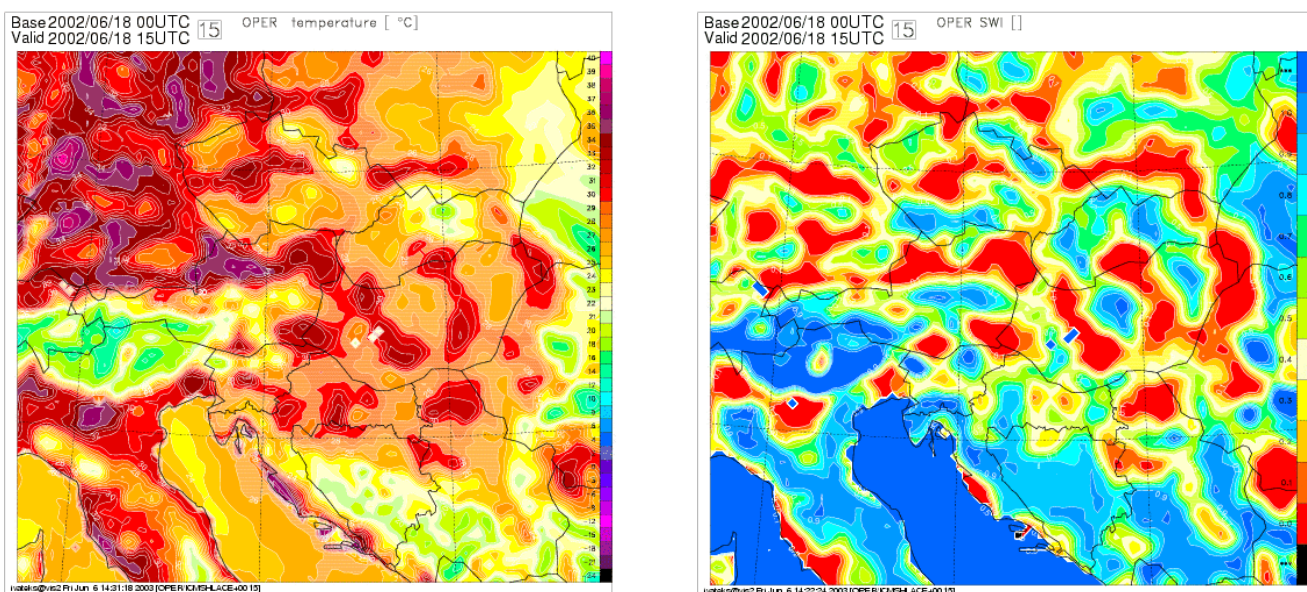


Figure 1 2m Temperature and Soil Wetness Index for June 18th 2002 15 UTC, 15 hours fcast

The aim of this work is to reduce the current unrealistic spatial heterogeneity of soil moisture by smoothing spatially the Soil Wetness Index (SWI). That heterogeneity caused hot spots in forecasted 2m Temperature during period 15th –20th June 2002 in ALADIN/LACE forecast. This period was tested first, with different combinations of smoothed SWI. Afterwards, the chosen combinations were tested on six cases in year 2003; January-3 days, April-2 days and May-1 day.

2. How Optimum Interpolation surface analysis works?

The Optimum Interpolation (OI) surface analysis is operational analysis in global model ARPEGE. As input for OI surface observation of 2m Temperature and Humidity are used. As it is known, in ALADIN or ARPEGE model we do not have level which corespond to that height, and a vertical interpolation is requied to compare the model fields with 2m observations. It interpolates the surface and the lowest model layer values supposing that the fluxes are calculated according to Monin Obukhov theory.

Analysis is sequential, with frequency of 6 hours, at that time observations are assimilated to corect background field.

After the OI, surface analysis of 2m SYNOP observations are interpolated at the model grid-point (by a 2m analysis). Because we don't have model level on 2m correction of surface parameters using 2m

increments ($\Delta T_{2m} = T_{2m}^a - T_{2m}^f$ & $\Delta RH_{2m} = RH_{2m}^a - RH_{2m}^f$) between analysed and forecasted values is needed. Surface parameters which are changed according the increments of 2m Temperature and Humidity are T_s – Surface temperature, T_p – Mean soil temperature, W_s – Superficial (liquid) soil water content and W_p – Total liquid soil water content.

On figure on a right hand side evolution of Total soil water according the increments of 2m Temperature and Humidity. Increments for surface prognostic variables are defined by the following expressions:

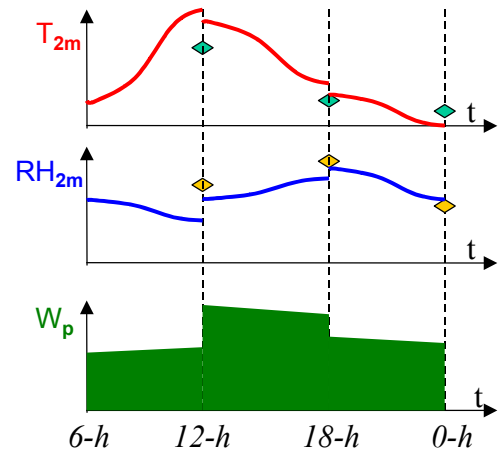
- for Temperatures:

$$T_s^a - T_s^f = \Delta T_{2m} \text{ \& } T_p^a - T_p^f = \Delta T_{2m} / 2\pi.$$

- for Soil water contents:

$$W_s^a - W_s^f = \alpha_{W_s T} \Delta T_{2m} + \alpha_{W_s RH} \Delta RH_{2m} \text{ \& } W_p^a - W_p^f = \alpha_{W_p T} \Delta T_{2m} + \alpha_{W_p RH} \Delta RH_{2m}.$$

Of coefficients $\alpha_{W_p/sT/RH}$ are function of local time, percentage of vegetation, LAI/Rsmin, texture, atmospheric conditions.



After the Analysis is finished, only surface data are stored as model variables, and 2m variables are recalculated from lowest model level and surface variables. The measurements are not distributed homogeneously, the surface analysis and forecast of convective precipitation have high degree of uncertainties which produce small scale features in the soil moisture. Surface analysis is done in ARPEGE (resolution from 20-200 km).

3. Soil Wetness Index (SWI)

The initialisation of soil moisture is very important in meteorological models since the repartition between sensible and latent heat fluxes at the surface depends on the quantity of water in the ground available for evapotranspiration.

The soil moisture in the LSS ISBA is represented by the superficial soil moisture W_s (quantity of water in 1 cm) and the total soil moisture W_p (quantity of water in the total reservoir depth dz). The total soil moisture is much more important to be initialised than W_s since the superficial reservoir has small capacity and W_s is relaxed towards W_p with a time scale of 2 days. The volumetric soil water content (W_p/dz) is not the best field to compare the available soil moisture for transpiration between grid-point. We often prefer the Soil Wetness Index (SWI), which represents the hydric stress of the vegetation. If $SWI \leq 0$ that means the transpiration of the plants is zero (dry soils) and if $SWI \geq 1$, the vegetation evaporate at the potential (maximal) rate (wet soils). Definition of SWI is shown bellow:

$$SWI = \frac{W_p + W_{pi} - W_{wilt}}{W_{fc} - W_{wilt}},$$

where is:

W_p - Total soil water content liquid (water),

W_{pi} - Total soil water content frozen (ice),

W_{wilt} - Soil water content at wilting point,

W_{fc} - Soil water content at field capacity.

Because SWI field has big gradients, it is possible to find completely dry and saturated soil on a distance of a few grid-points (~100 km), what is not realistic. The SWI field evolves on very long time scales, like W_p , because of the large capacity of the total soil reservoir in ISBA.

Smoothing is performed with subroutine elislap, which smooths a field by adding its laplacian times a constant factor (a length scale). Smoothing is performed just for land points, without snow cover and without ice in the ground, in the ALADIN model. The laplacian is calculated with the 5 nearest grid-points.

After that, because there is not **SWI** in ALADIN files, it was needed to convert SWI_{smooth} and put back $(W_p)_{smooth}$ and in ALADIN file. $(W_p)_{smooth}$ is calculated with these formulae:

$$(W_p)_{smooth} = SWI_{smooth} \cdot W_{fc} + (1 - SWI_{smooth}) \cdot W_{wilt},$$

and two more checks:

$$\text{if } (W_p)_{smooth} \leq \text{veg} \cdot W_{wilt} \text{ then } (W_p)_{smooth} = \max(W_p, (W_p)_{smooth})$$

$$\text{if } (W_p)_{smooth} \geq W_{fc} \text{ then } (W_p)_{smooth} = \min(W_p, (W_p)_{smooth})$$

$$(W_p)_{smooth} = \max(\max(W_s, dz), (W_p)_{smooth})$$

where is:

- veg** - Percentage of vegetation,
- W_s** - Surface soil water content liquid (water),
- dz** - Soil depth or reservoir depth.

To be able to make calculation of SWI next fields are needed in ALADIN or ARPEGE FA-file: Land/sea mask (SURFIND.TERREMER), Snow depth (SURFRESERV.NEIGE), Frozen deep soil wetness (PROFRESERV.GLACE), Percentage of vegetation (SURFPROP.VEGETAT), Soil depth (SURFEPAIS.SOL), Percentage of clay within soil (SURFPROP.ARGILE), Liquid (water) surface soil wetness (SURFRESERV.EAU), Liquid (water) deep soil wetness (PROFRESERV.EAU)

Smoothing is performed just for land points (Land/sea mask SUFRIND.TERREMER=1), points without snow cower (SURFRESERV.NEIGE=0), and without ice in a ground (Frozen deep soil wetness PROFRESERV.GLACE=0).

On Figure 2, analyzed and 6, 12 and 15 hour forecasts SWI are shown. There is no important change between analysis and forecasts. Dry areas remain dry and wet areas remain wet after 15 hours of forecast. SWI field has big gradients, on a distance of less than 100 km, it is possible to find completely dry and saturated soil, what is not realistic. With smoothing of SWI we would like to reduce the current unrealistic spatial heterogeneity of soil moisture.

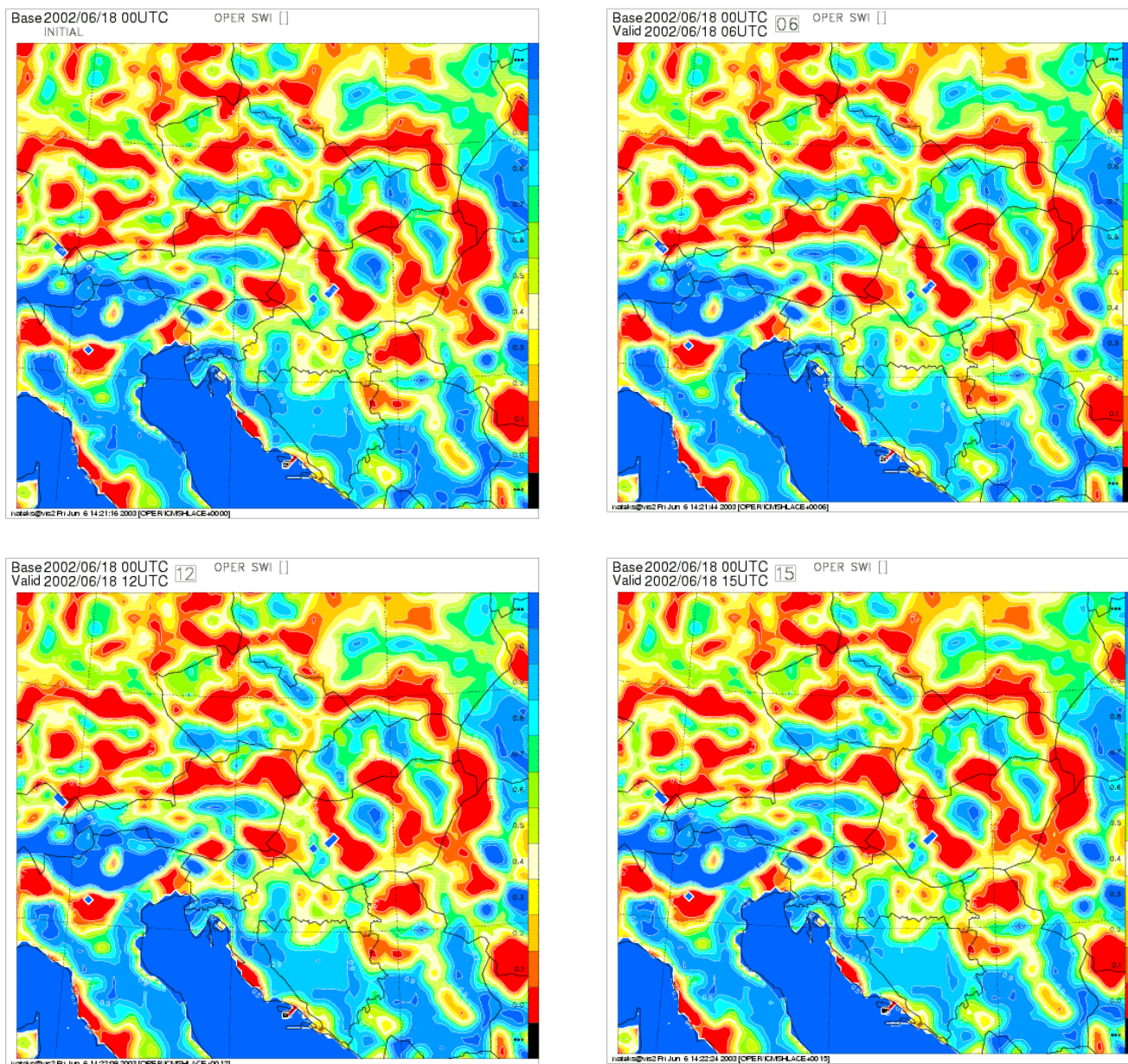


Figure 2 Smoothed Soil wetness index for operational run, start 18.06.2002. 00 UTC, analysis and forecasts for 6, 12 and 15 hours

4. Smoothing of SWI

With increasing of the radius of smoothing we increase area that is smoothed and amplitude of smoothing. After some value with increasing of the radius of smoothing results are the same like it is with lower radius. For LACE domain 12.2 km resolution results are the same for 8.1 and 6.1 km. In ALADIN smoothing is performed with data from just 5 nearest grid points and in ARPEGE it is with 7 grid points. Idea is just to smooth the SWI field over the land if there is no ice in a ground or snow cover. That means to high impact during the summer and low or no impact during the winter.

On Figures 3 and 4 results for smoothing of SWI for winter and summer are shown. For a summer period 00 UTC smoothing is performed for all domain, as it is shown on Figure 4. Radius of smoothing is 4.1 km (1/3 of grid size) or 6.1 km (1/2 of grid size), and numbers of smoothing are 10, 21 and 30. In legend XXSMRR, means that smoothing is performed XX times with radius of smoothing RR*0.1 km. 10SM61 means that 10 smoothings are performed with radius of 6.1 km. Smoothing is working quite well.

SWI-20030113_00

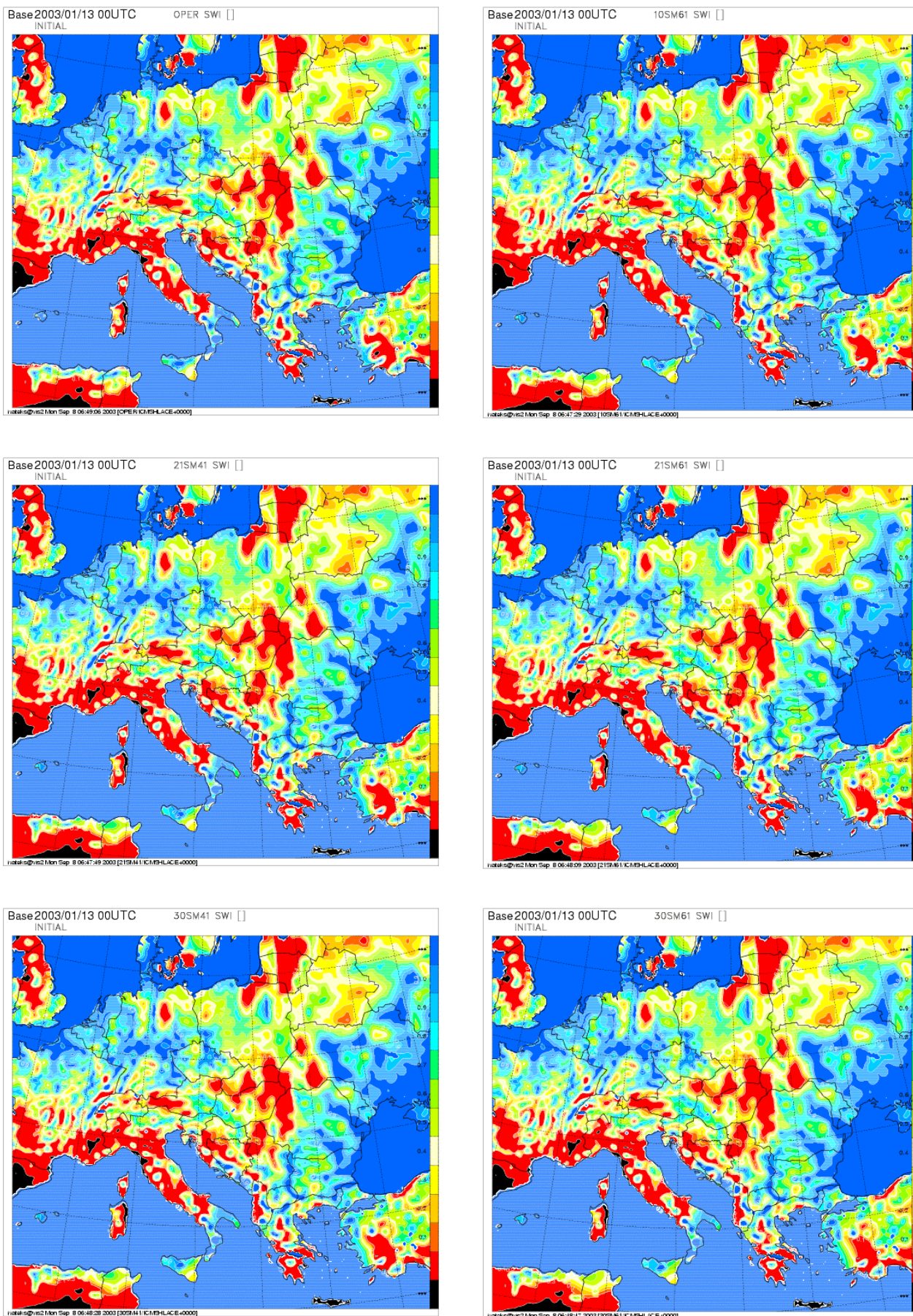


Figure 3 Smoothed Soil wetness index for operational run and for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km), for 13.01.2003. 00 UTC, winter example

SWI-20020619_00

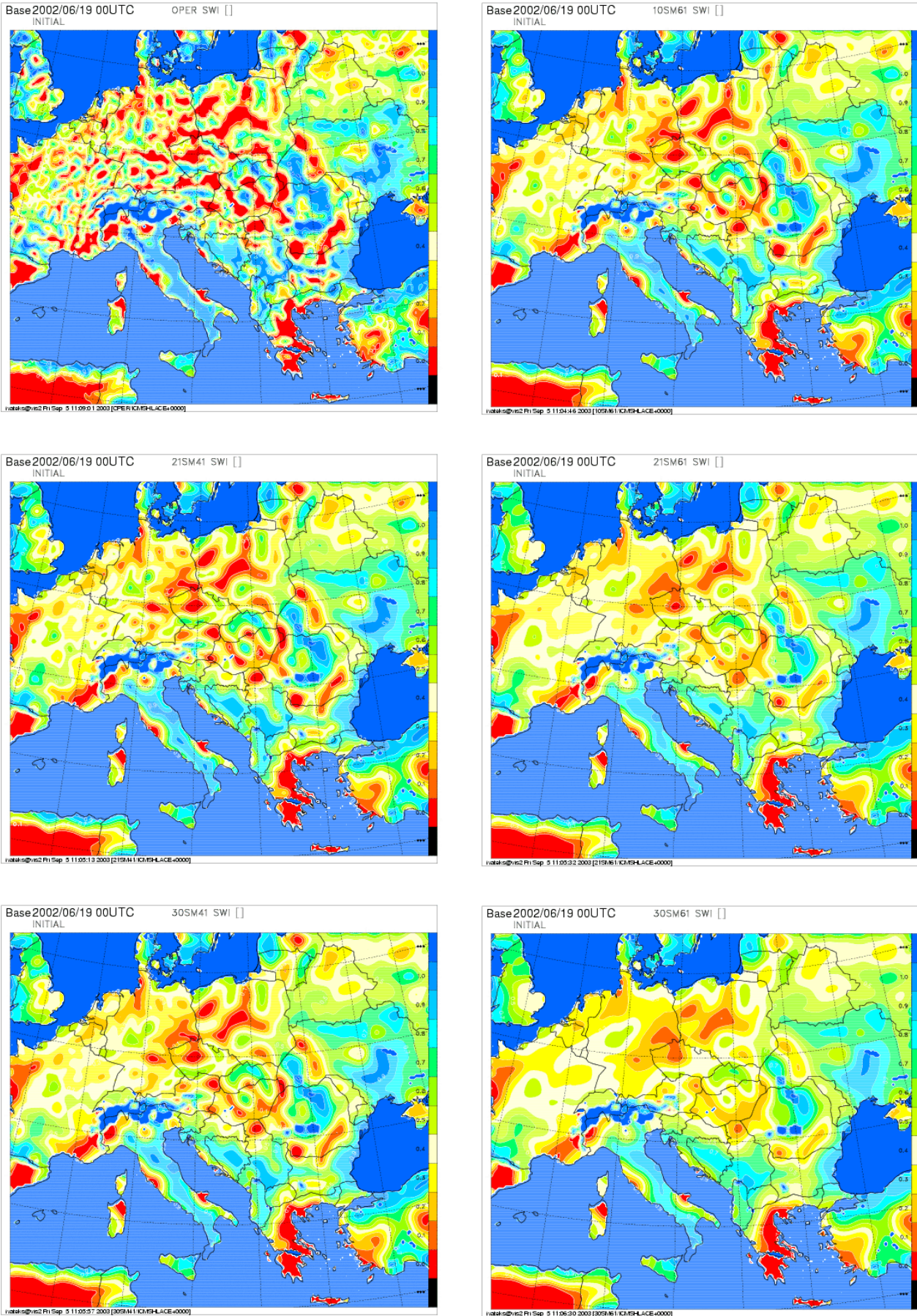


Figure 4 Smoothed Soil wetness index for operational run and for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km), for 19.06.2002. 00 UTC, summer example

As it is shown on Figure 3, there are some visible changes on Istria peninsula, Apennine peninsula Sicily and Africa, for other areas changes are too small, or there are no changes at all.

For SWI field during the summer smoothing for same number of smoothing with 6.1 km smooth SWI field more than with 4.1 km, like it was expected. Smoothed field for 21SM41 looks similar with 10SM61. For smoothing 21SM61 there is still some details in SWI field, what is not the case for 30SM61. For smoothing 30SM61 SWI field is really smooth, maybe to smooth?

5. Results

Forecasts with operational version of ALADIN AL25T1_op2 in Croatia were done. 12 days are chosen for testing, 6 days in June 2002 and 6 days in year 2003, 3 days in January, 2 days in April and 1 day in May.

5.1. Results for winter examples, January 2003

3 days in January 2003 were tested (07th, 13th and 16th).

7th was day with lot of snow in Croatia and with precipitation in South Europe. Highest daily temperatures for 7th and 8th were around 0°C for continental part of Europe.

13th and 14th were days with highest daily temperature around 0 with some sunny periods.

16th and 17th were days with lot of sunshine, and without rain for continental Europe. Highest daily temperatures were higher than 0°C for continental part of Europe.

For Analysis, there are no changes bigger than ± 0.5 °C for 2m Temperature or ± 2 % for Relative Humidity.

In winter examples there are less than 5, from more than 600 points, with difference between OPER and smoothed SWI in initial field in forecasted 2 m Temperature (T2m) for more than 0.5 °C for each forecast.

For 2 m Relative Humidity (H2m) there is some bigger impact, less than 50 points from more than 600 points with difference between OPER and smoothed SWI in initial field in forecasted H2m for more than 2 % for each forecast. Difference higher than 10 % was just for 13th January 2003 for 36 and 48 forecasts.

From that results we could conclude that impact on T2m for winter examples is really small, and same is for H2m.

5.2. Results for spring examples, April 2003

Two days in April 2003 were chosen 2nd and 5th.

During the 2nd and 3rd there were moving cyclone with frontal system over the Europe. First day was sunny in Central and East Europe. Amplitude of T2m in continental Croatia were around 20 °C, next day amplitude in west part of Croatia was less than 5 °C.

During the 5th and 6th West Europe was without precipitation. T2m amplitude was more than 10 °C in south part of Europe.

No important changes for analyses.

For T2m there is less than 5% of points with changes bigger than ± 0.5 °C. There is just one different between forecast for more than 2 °C.

For H2m maximum 20 % of points were changed for more than ± 2 %. Just few times H2m were changed for forecasts for more than 10 %.

That means that there are some changes, bigger than for winter, but not big one.

5.3. Results for 2nd spring example, 6th May 2003

6th and 7th May, front moving over West Europe it stop on Alps, other part of Europe with T2m amplitude around 20 °C with lot of sunshine. Hot spots over a Central Europe, smaller for 7th.

No changes for analyses.

For H2m maximum 45 % of points are changed for more than H2m ± 2 %, and 9 % for more than ± 10 %. For T2m maximum 22 % of points are changed for more than T2m ± 0.5 °C, and 2 % for more than ± 2 °C.

For this period impact of smoothing of SWI is relatively big.

5.4. Results for problematic period in June 2002.

Period from 15th to 21st of June 2002 were very hot period with temperatures in Central Europe more than 30 °C, even with extreme values from the beginning of measuring. Very hot period was same and for West Europe but not during the whole period.

No changes for analyses. For Analysis, there are no changes bigger than ± 0.5 °C for 2m Temperature or ± 2 % for Relative Humidity.

For forecasts, generally with increasing of the number of smoothing or radius of smoothing more and more points have changes bigger than ± 0.5 °C for 2m Temperature or ± 2 % for 2m Relative Humidity.

For H2m maximum 65 % of points are changed for more than ± 2 %, and 17 % for more than ± 10 %. For T2m during this period maximum numbers of changed point is 53 % for more than ± 0.5 °C, and 9 % for more than ± 2 °C.

In problematic period it was noticed maximum changes of H2m and T2m for all tested examples.

For a summer examples in areas where a very big gradients of surface temperature were noticed improvement in forecast of T2m is really big, in same points for more than 2 °C for radius of smoothing 6.1 km and for 21 and 30 times of smoothing for 12 and 36 hrs forecast.

On following Figures 5-14, 15 and 36 hours forecast for T2m and H2m are shown, star June 19th 2002 00 UTC.

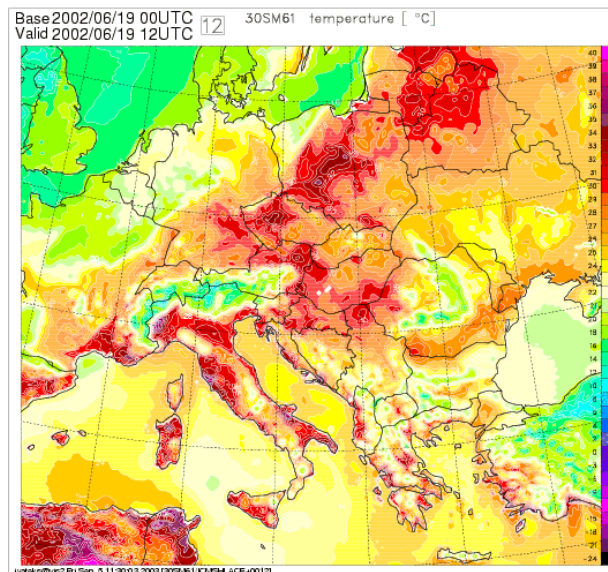
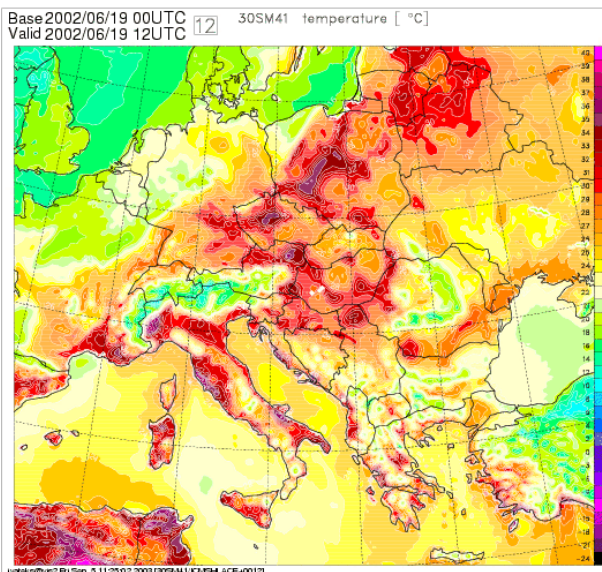
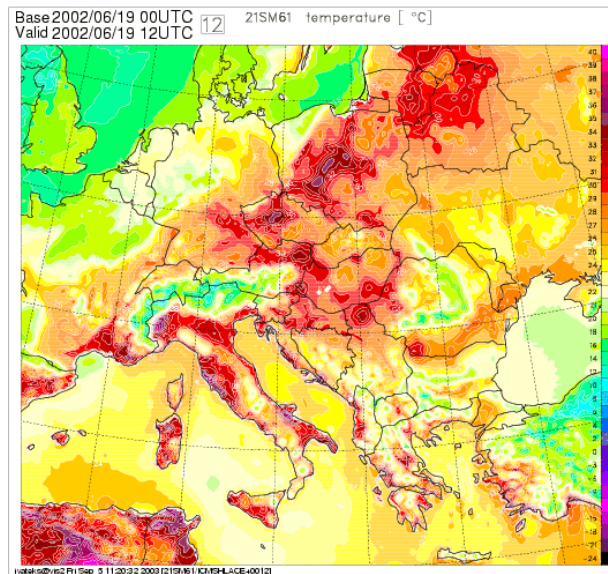
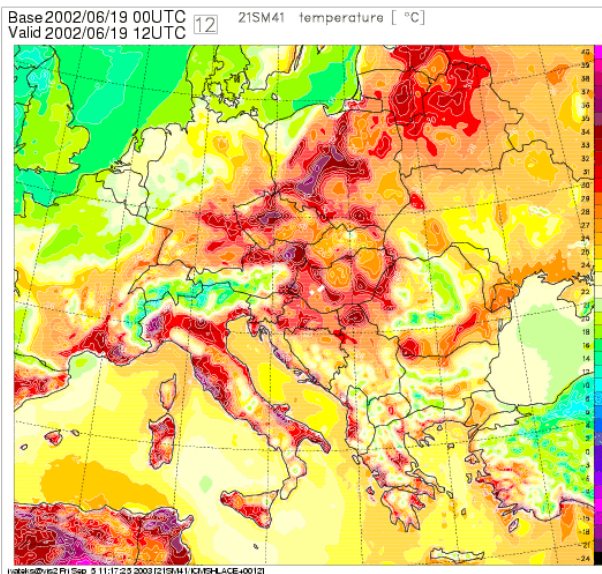
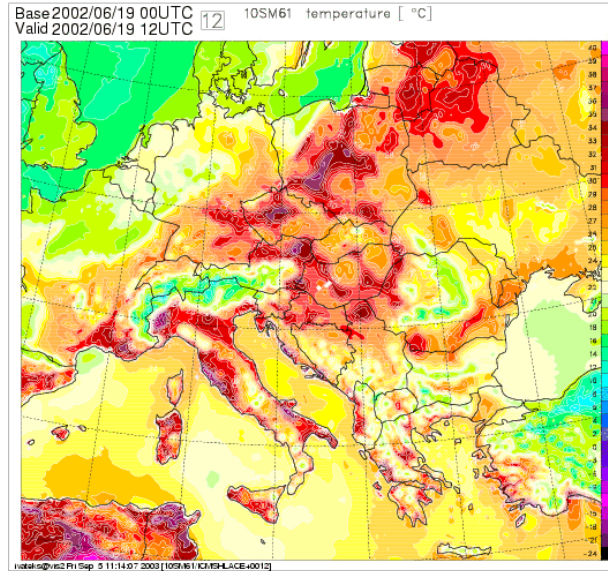
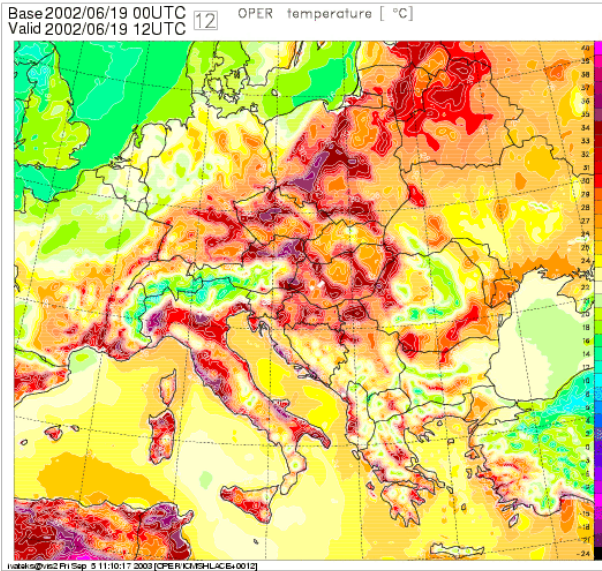


Figure 5 2 m Temperature 12 hrs forecast for operational run and for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km), start of the integration 19.06.2002. 00 UTC

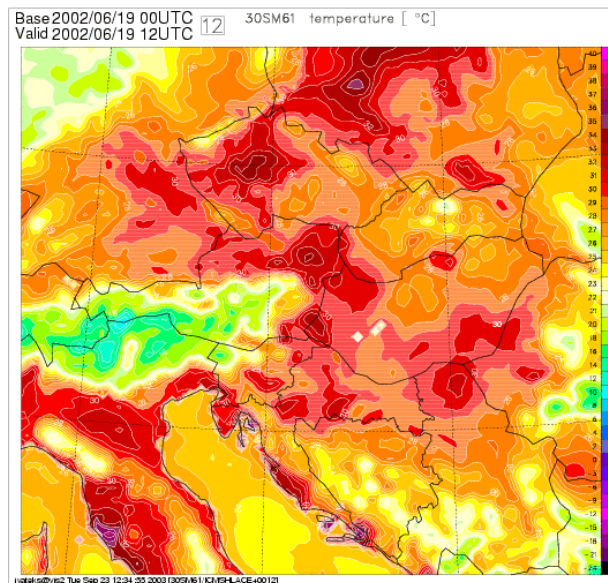
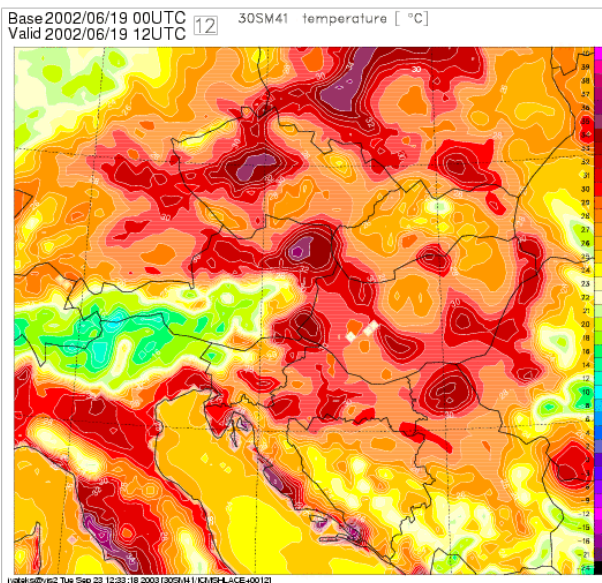
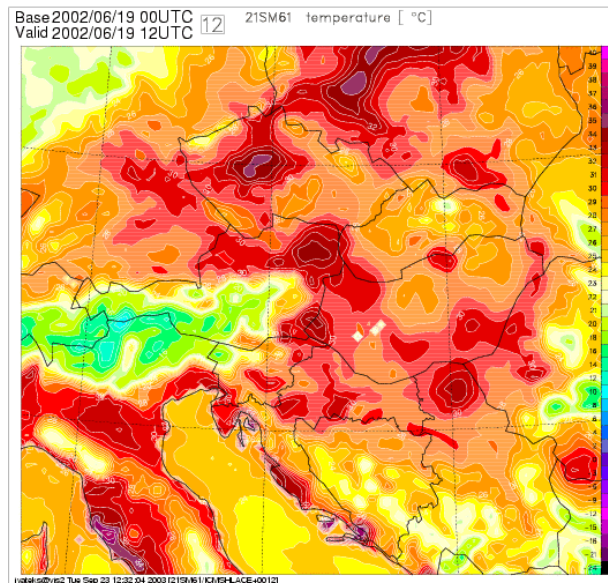
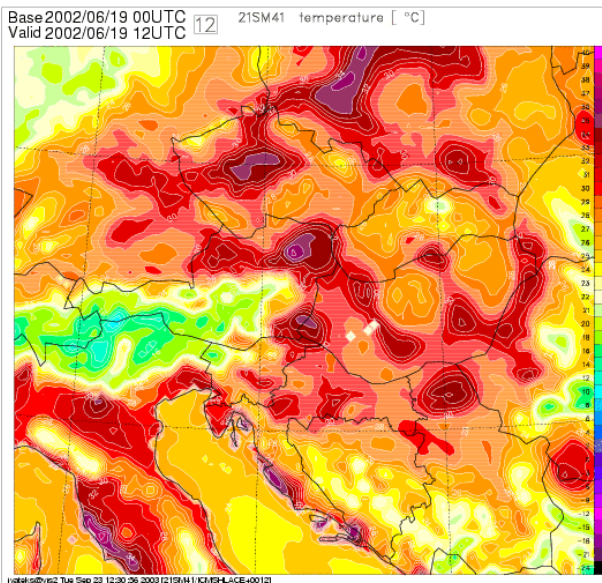
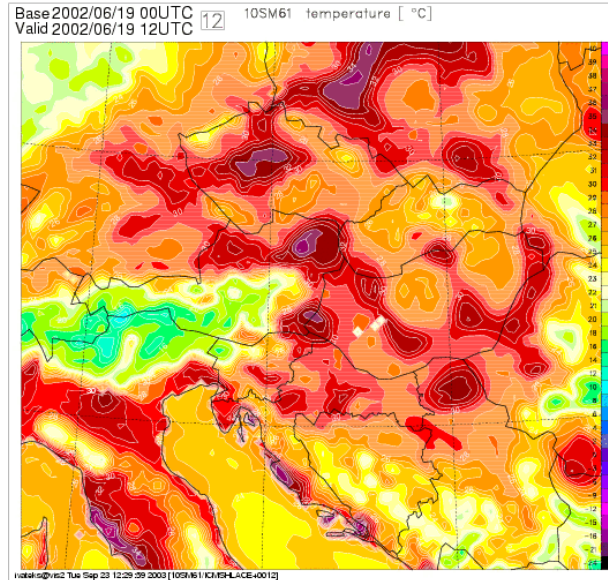
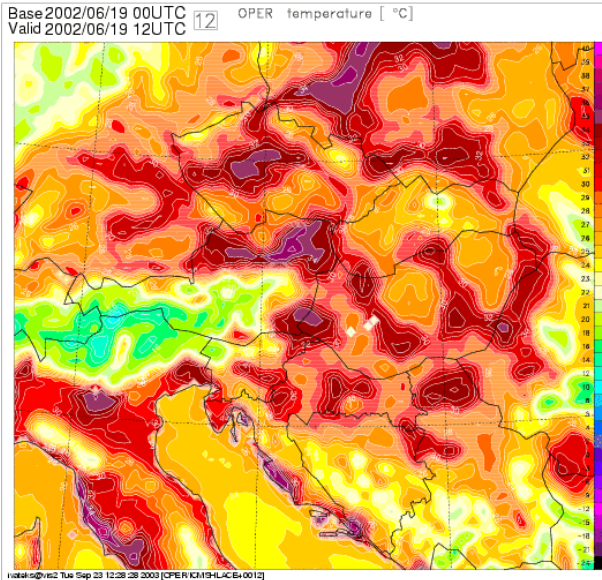


Figure 6 Zoom of T2 m 12 hrs forecast for operational run and for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km), start of the integration 19.06.2002. 00 UTC

There are no anymore-such big gradients in T2m field like it was in Operational run. For some points T2m is smaller for more than 2 °C if we compare operational run and smoothing with 21 and 30 smoothings with radius of smothing 6.1 km.

On Figure 8 and 11 comparison of absolute error are shown. If the value on Figure(s) is less than zero (blue or green color of point) that means that operational forecast is better, absolute error is smaller for operational run. If the value on Figure is higher than zero (yellow, orange and red points) one of the tested smoothed forecast is better, absolute error is greater for operational run. Model results are compared with SYNOP data.

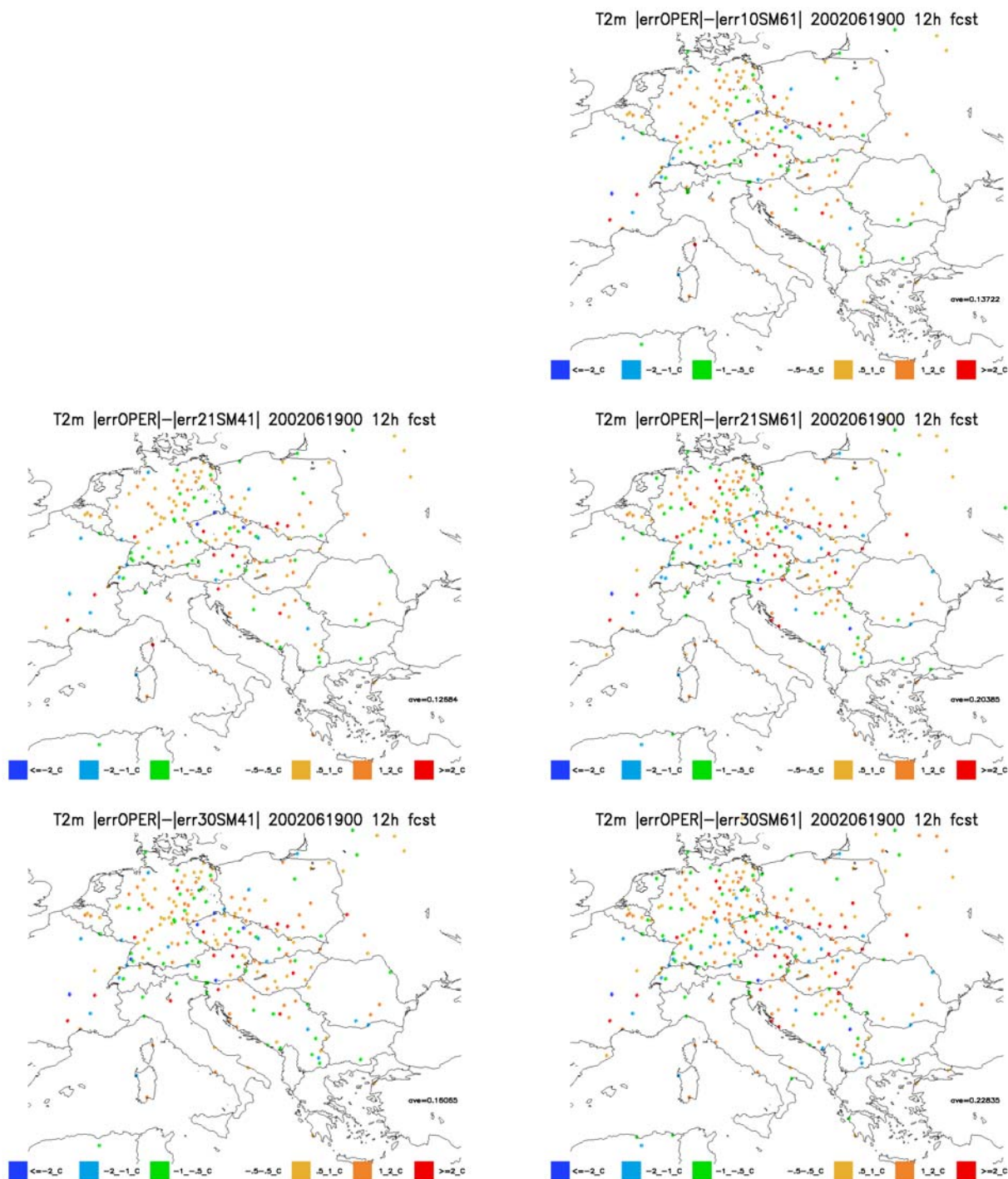


Figure 8 Comparison of absolute error for 12 hrs forecast of T2m for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km) with operational run forecast, start of the integration 19.06.2002. 00 UTC

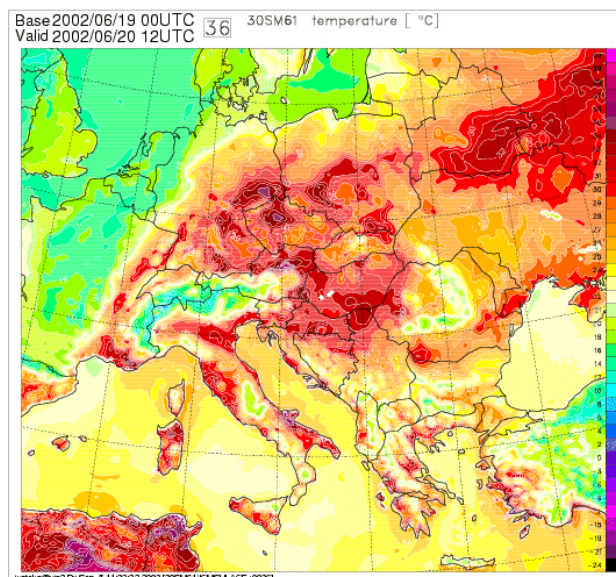
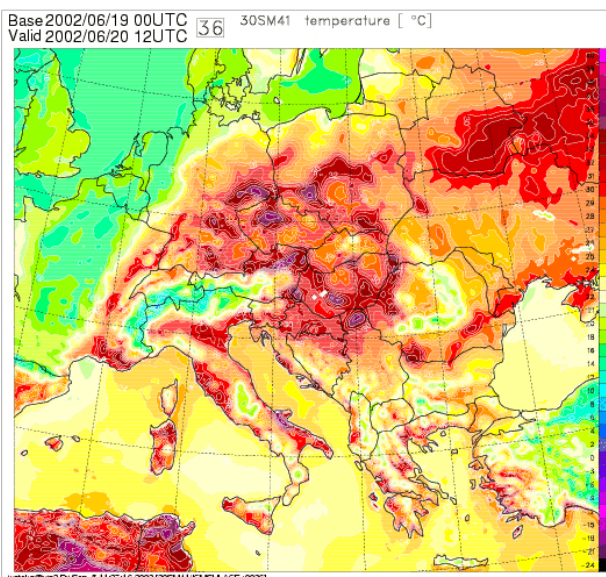
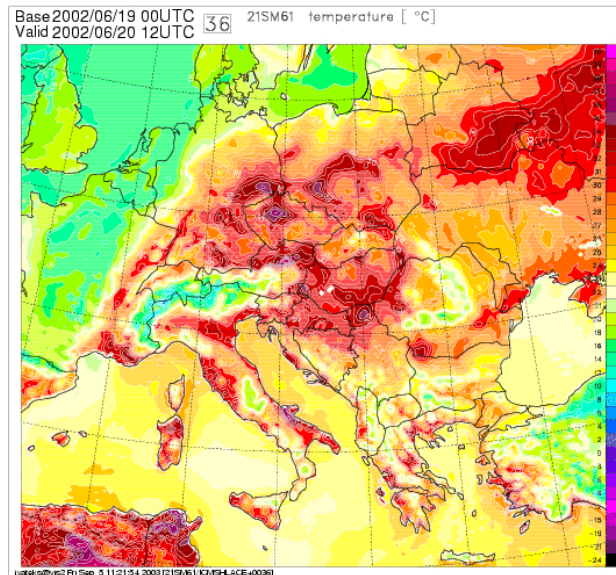
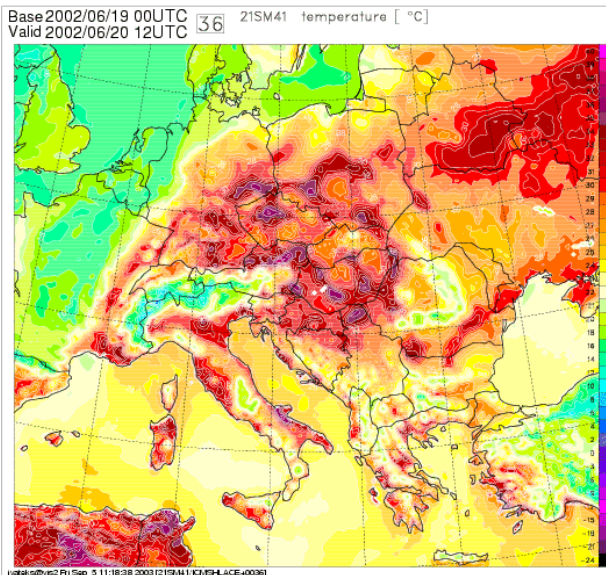
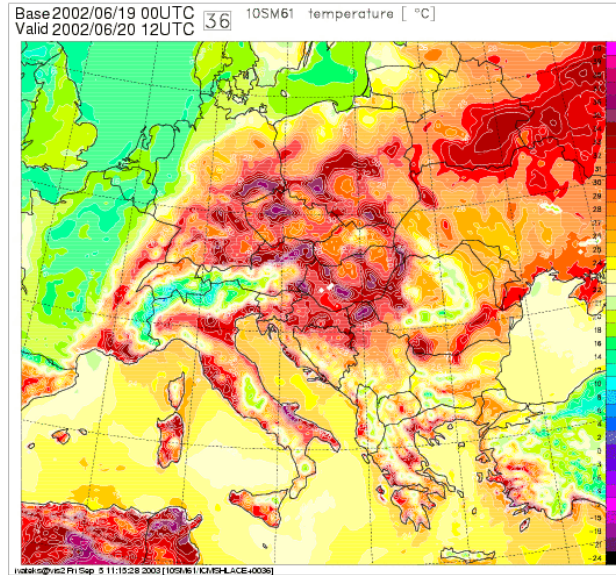
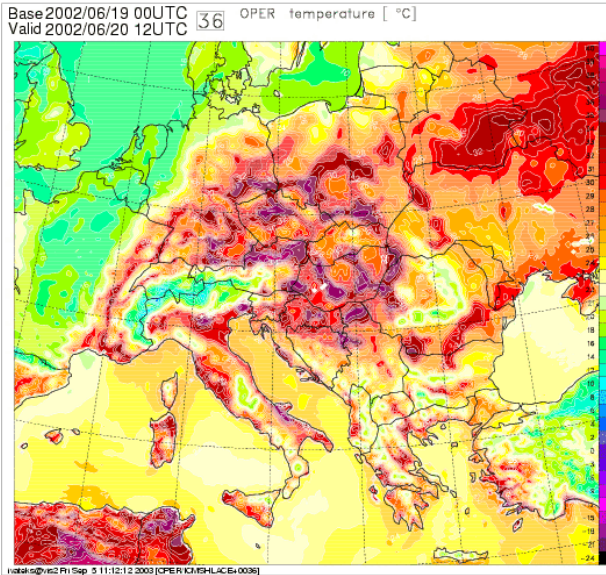


Figure 9 2 m Temperature 36 hrs forecast for operational run and for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km), start of the integration 19.06.2002. 00 UTC

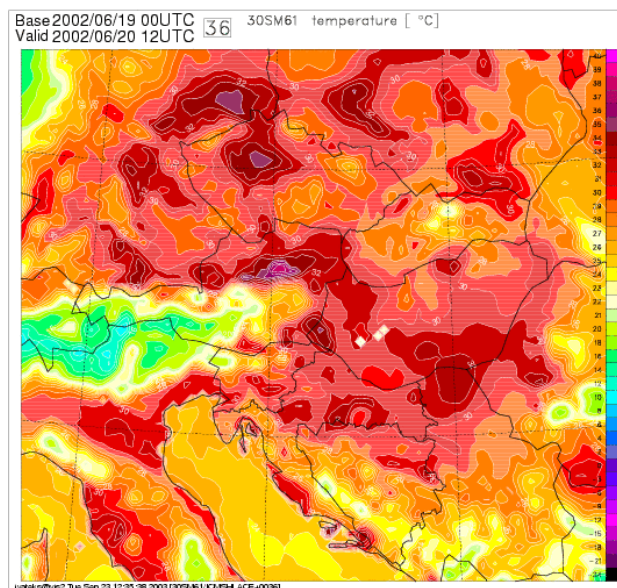
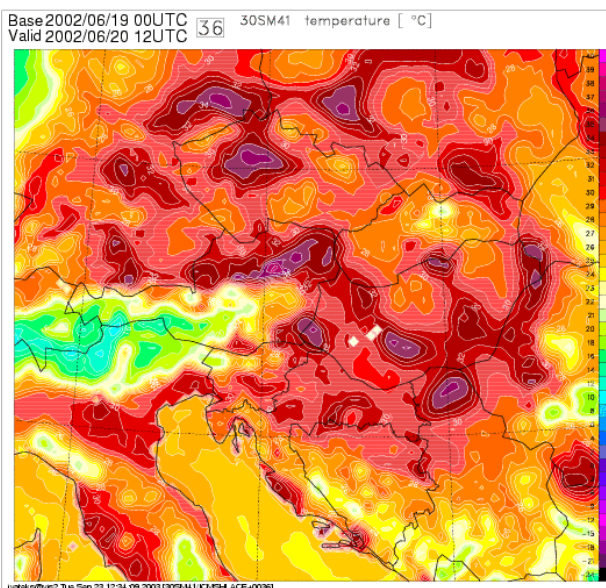
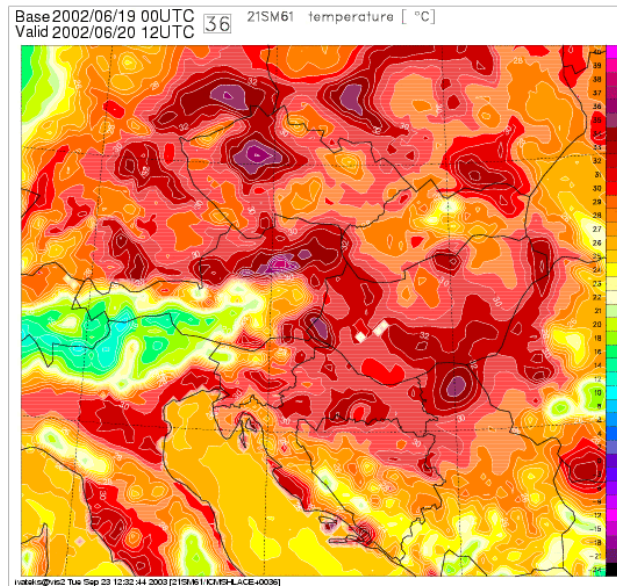
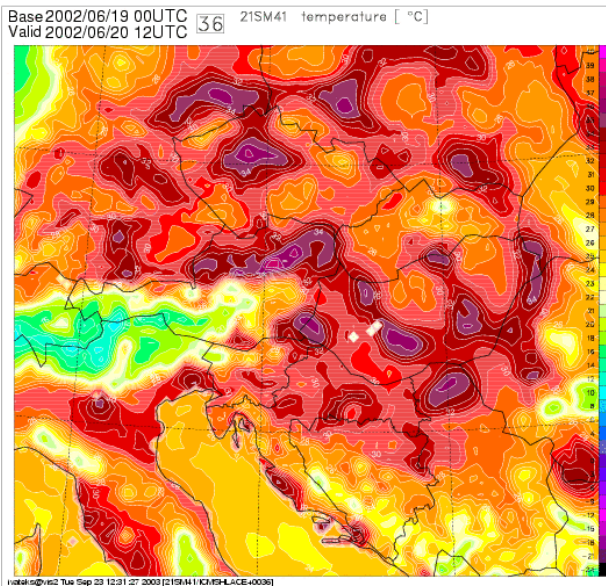
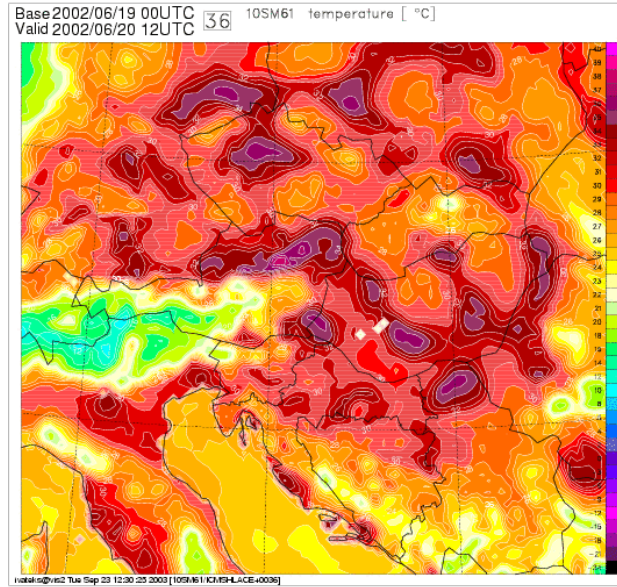
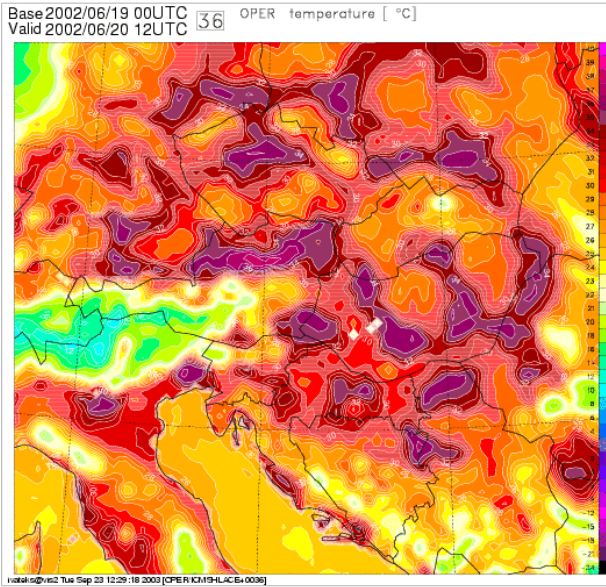


Figure 10 Zoom of T2 m 36 hrs forecast for operational run and for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km), start of the integration 19.06.2002. 00 UTC

It is not shown but it is obvious that in places where the maximum daily temperature is not too hot there is no change with smoothed SWI. For both days West France was with low maximum T2m and then there are no changes bigger than ± 0.5 °C for 2m Temperature.

At the end of the report Tables with numbers of points in classes, RMS and BIAS are placed.

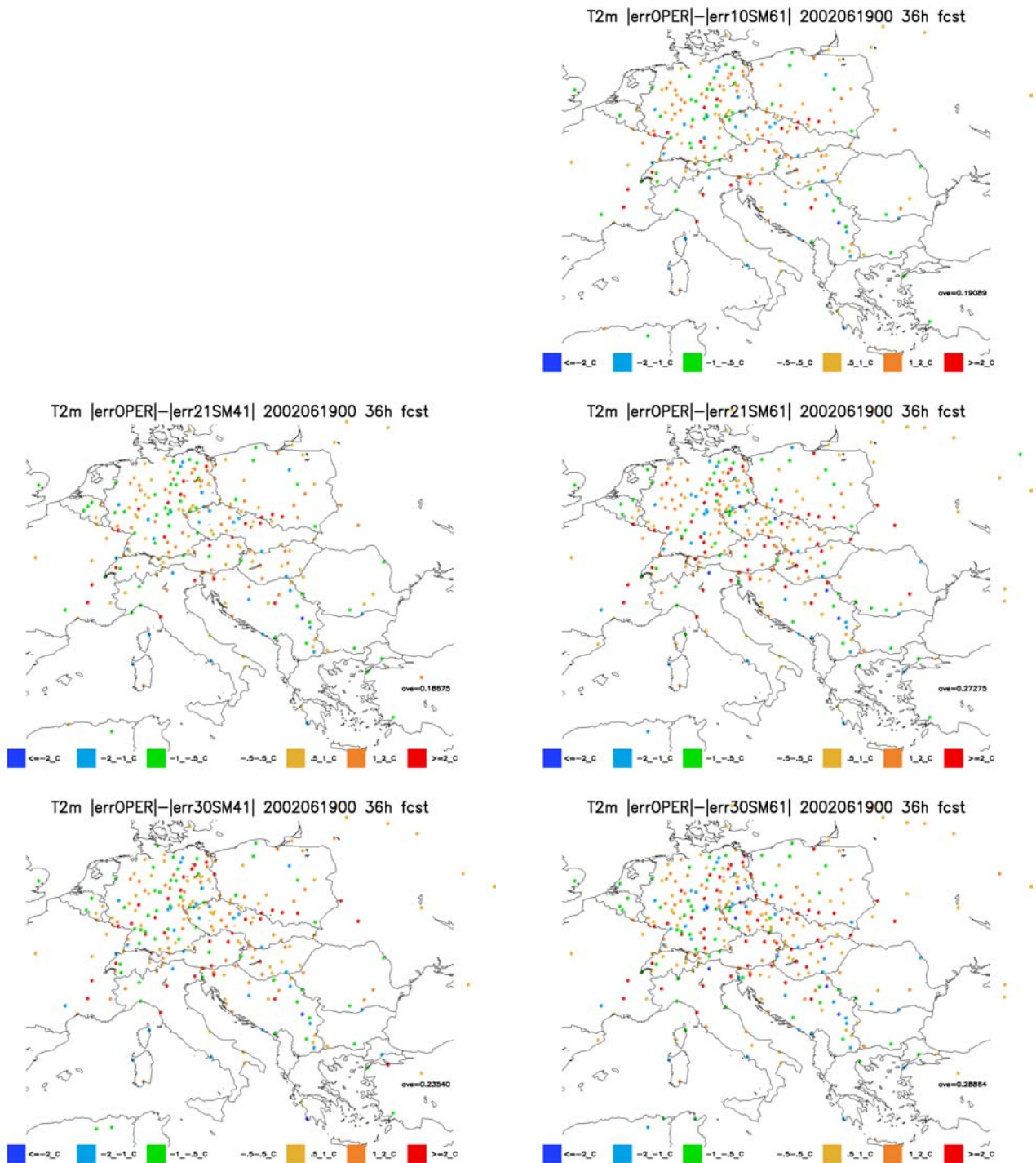


Figure 11 Comparison of absolute error for 36 hrs forecast of T2m for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km) with operational run forecast, start of the integration 19.06.2002. 00 UTC

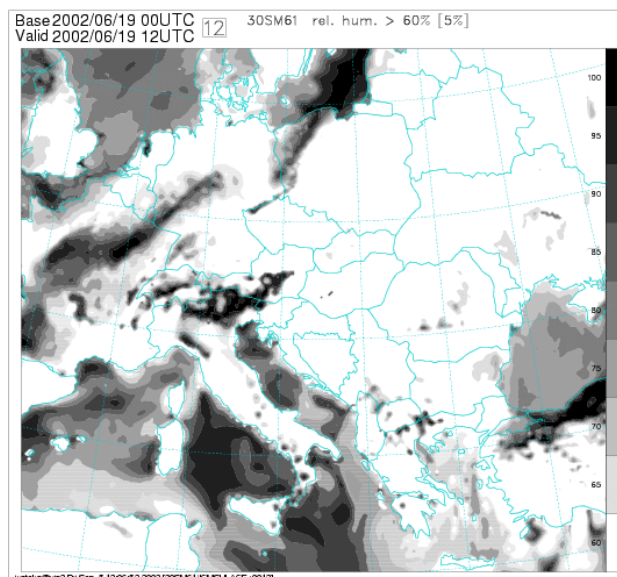
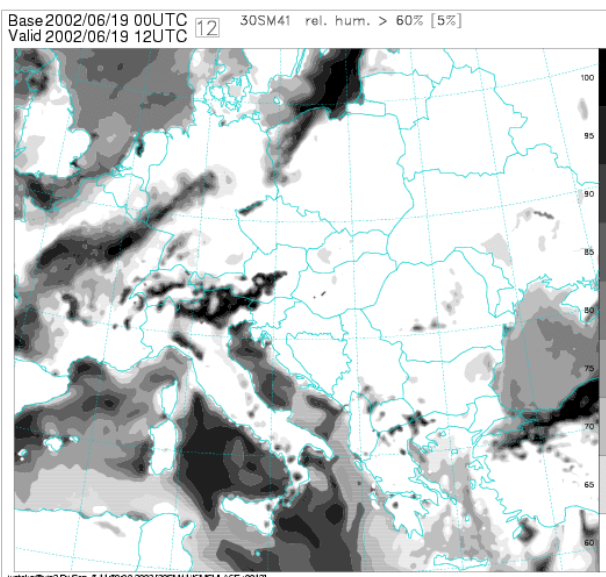
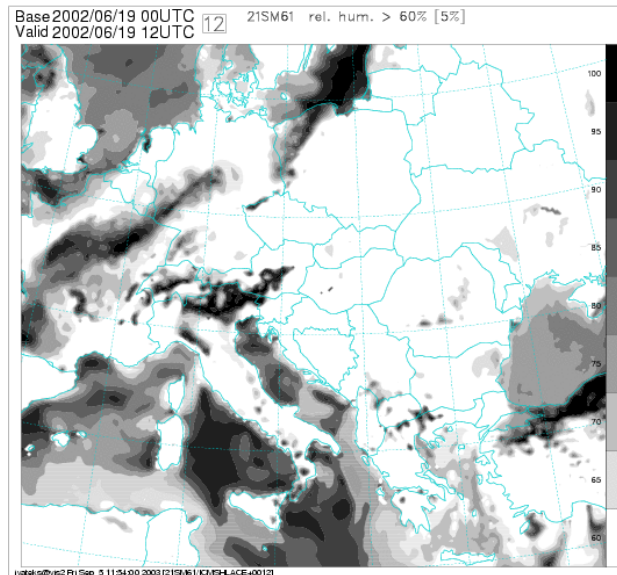
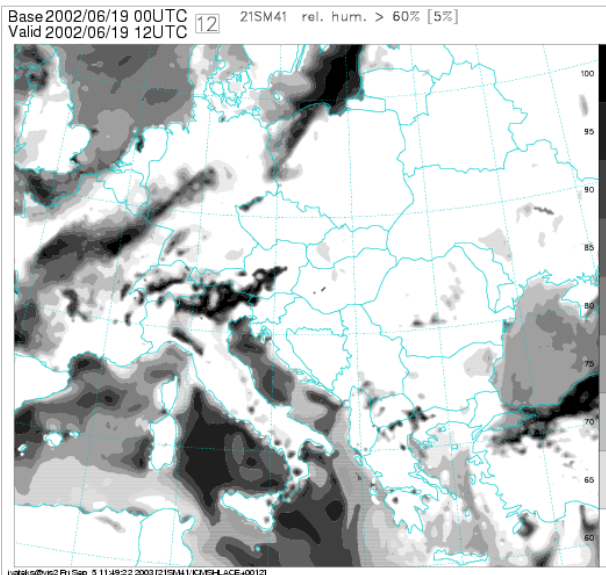
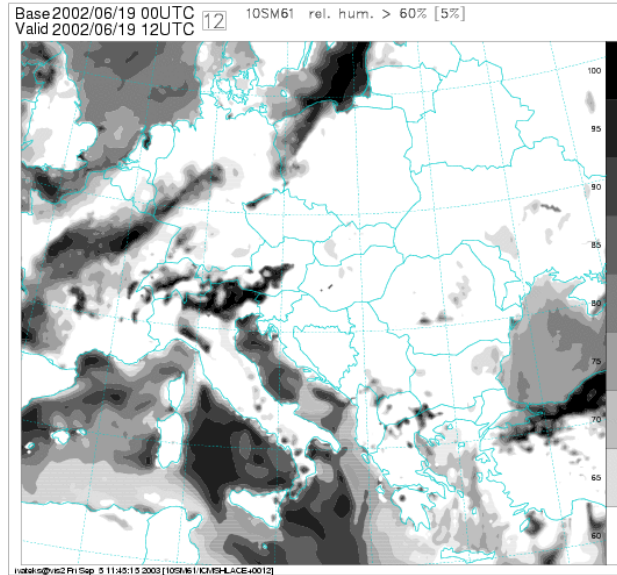
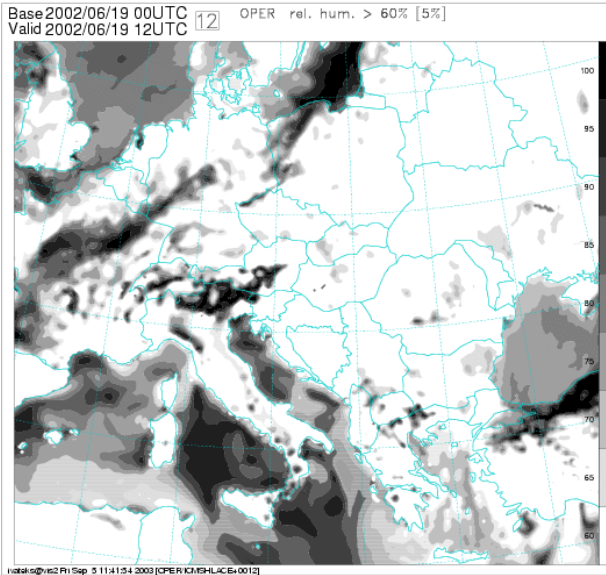


Figure 12 2 m Relative Humidity 12 hrs forecast for operational run and for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km), start of the integration 19.06.2002. 00 UTC

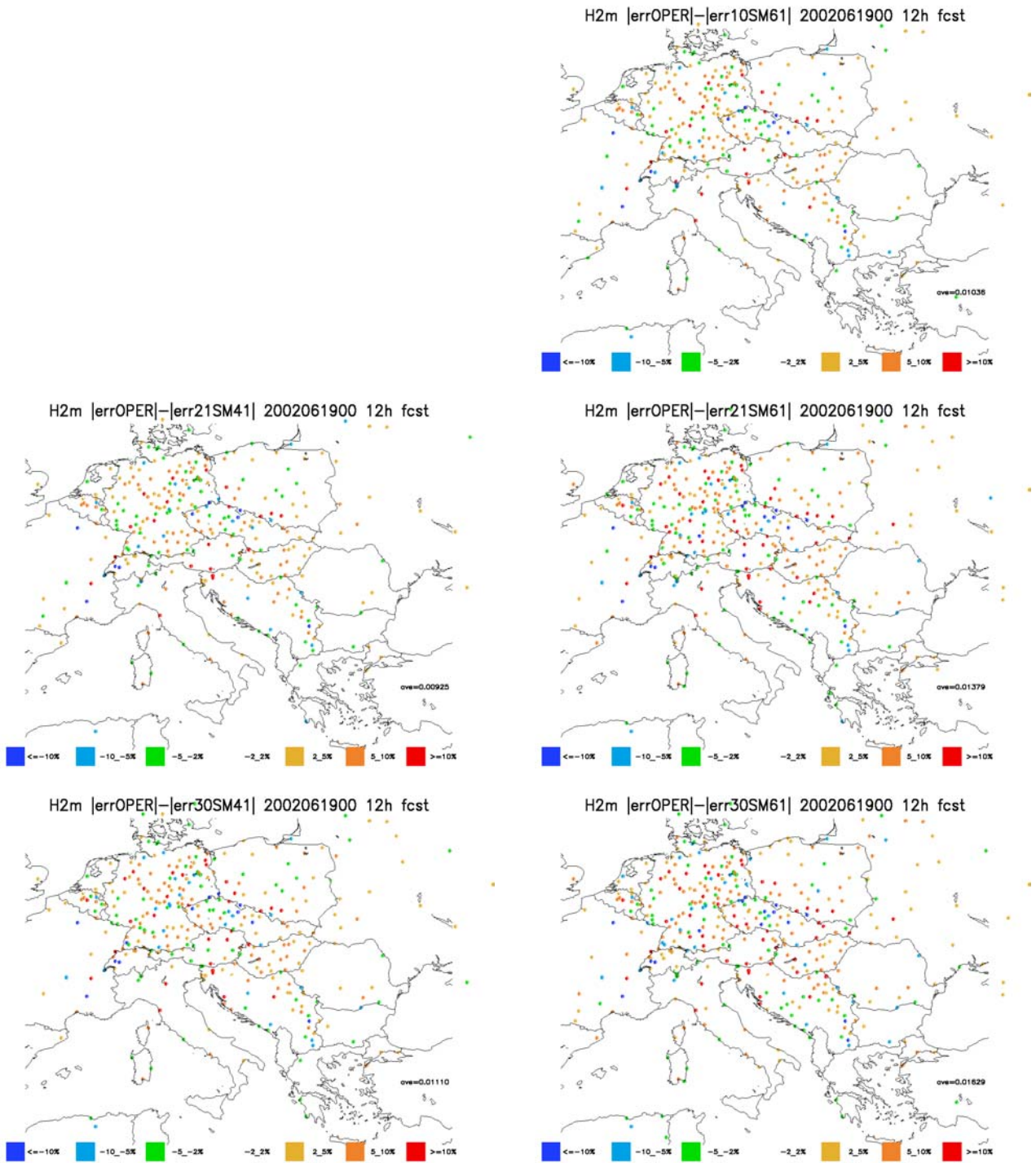


Figure 13 Comparison of absolute error for 12 hrs forecast of H2m for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km) with operational run forecast, start of the integration 19.06.2002. 00 UTC

As it was expected with increasing of smoothing 2m Relative Humidity be significantly changed more and more points be changed, same like it was for T2m. There is a lot of points where are improvement of both parameters T2m and H2m.

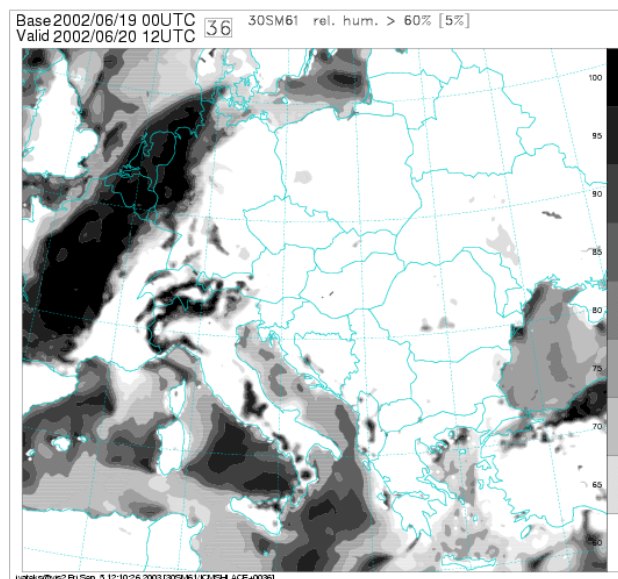
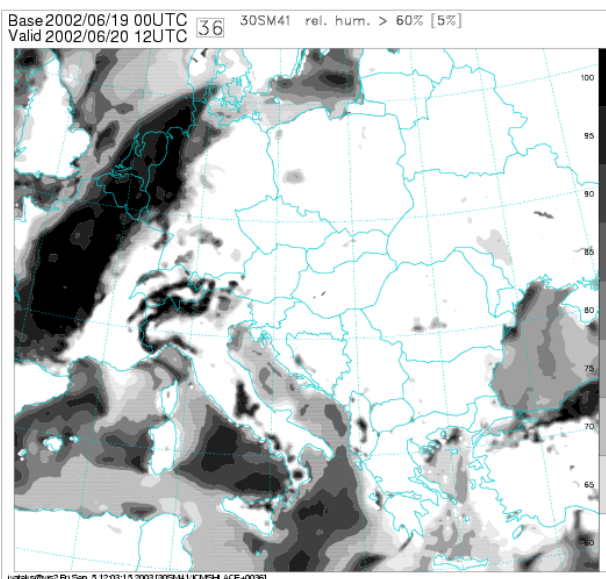
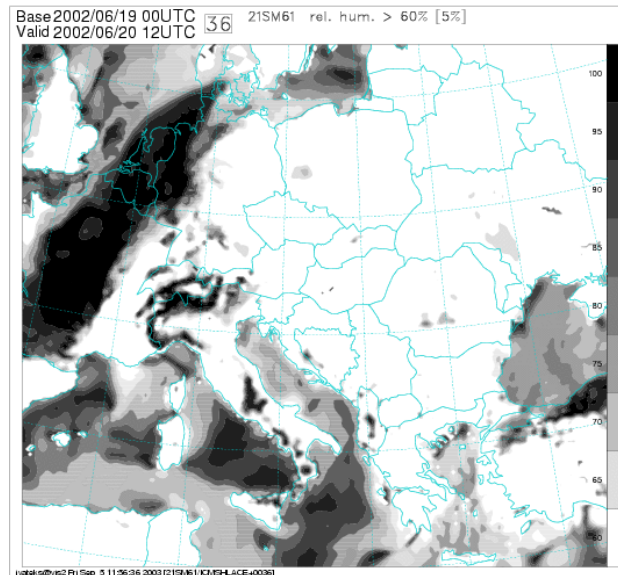
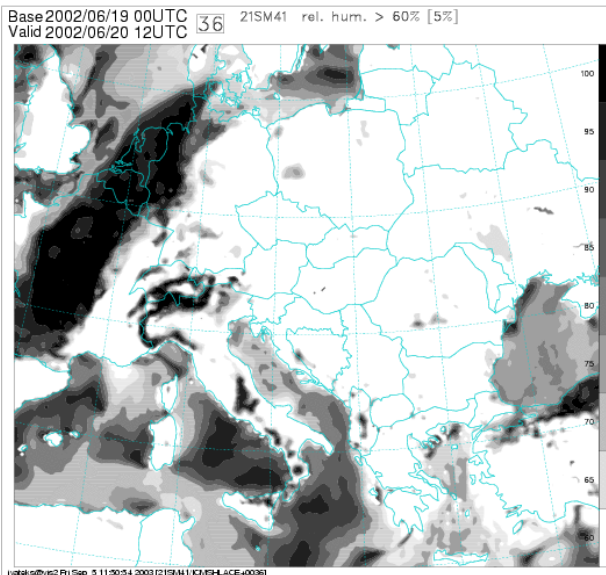
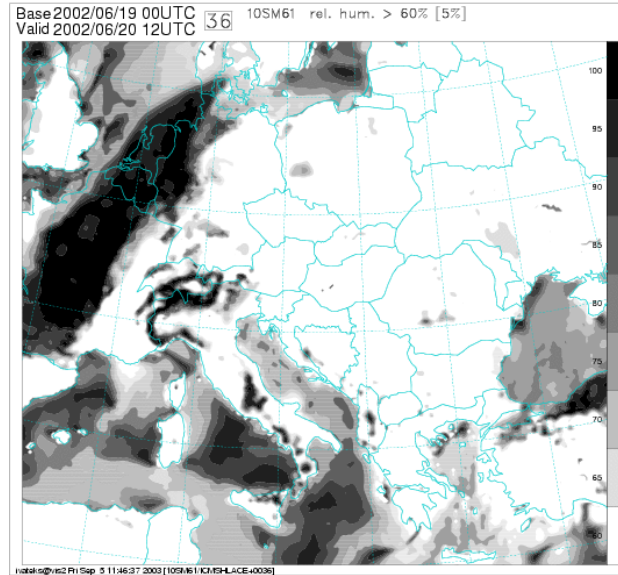
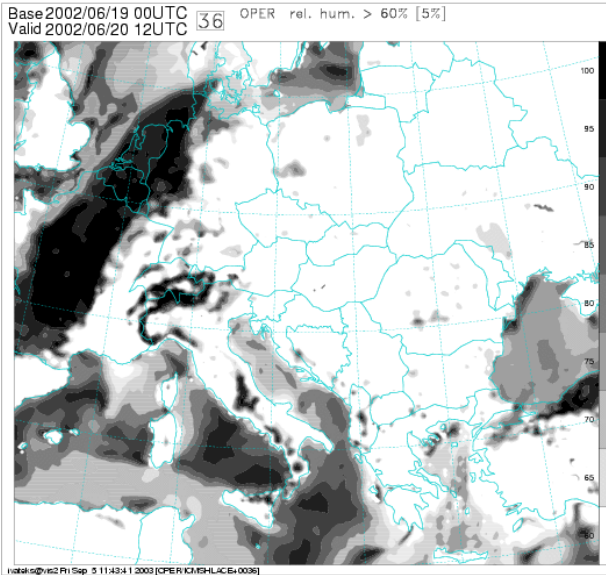


Figure 14 2 m Relative Humidity 36 hrs forecast for operational run and for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km), start of the integration 19.06.2002. 00 UTC

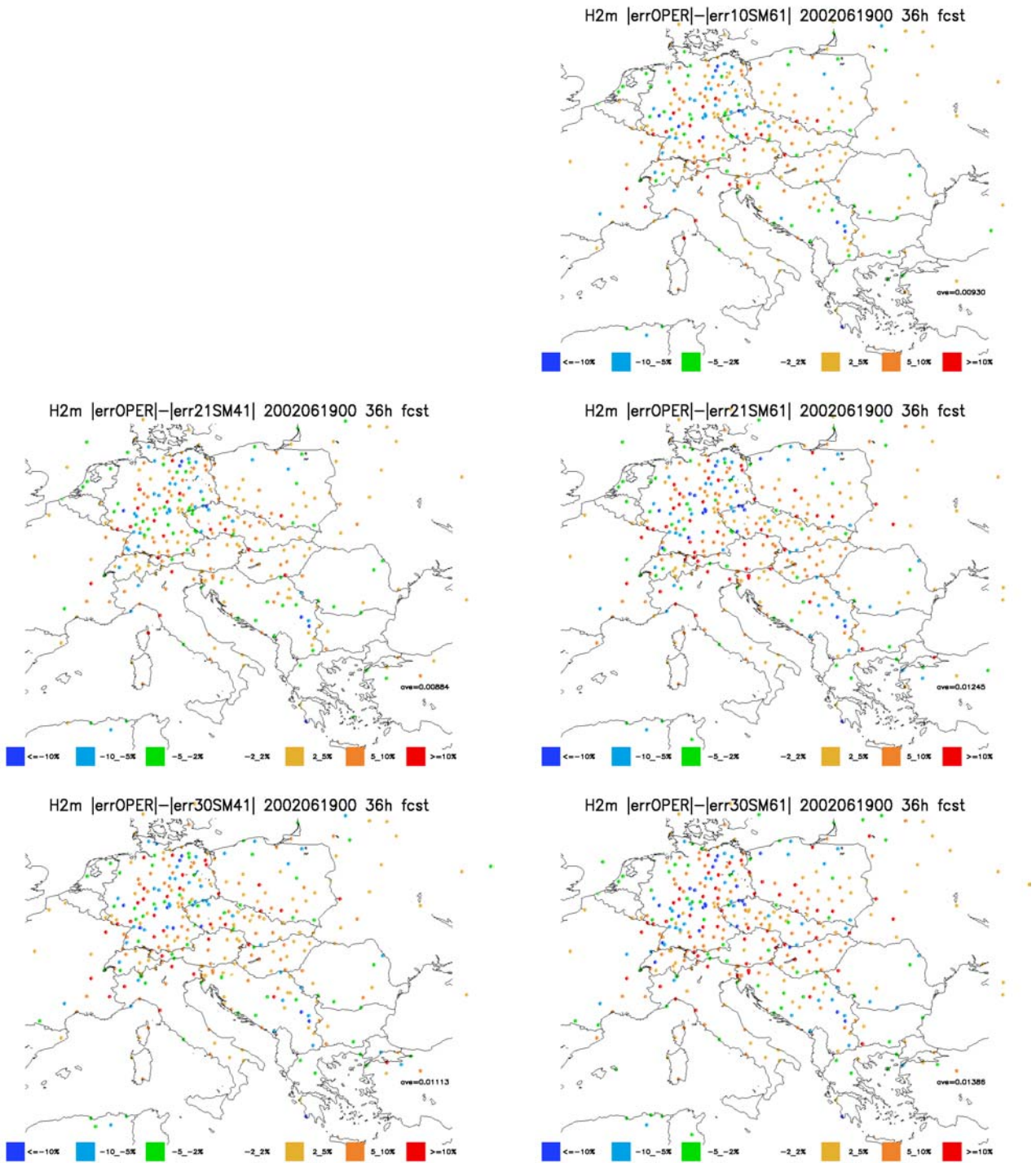


Figure 15 Comparison of absolute error for 36 hrs forecast of H2m for different numbers (10, 21, 30) and radius of smoothing (4.1, 6.1 km) with operational run forecast, start of the integration 19.06.2002. 00 UTC

6. Comparison of RMS and BIAS for H2m and T2m

Comparison of RMS and BIAS for H2m and T2m between operational run and runs with smoothed SWI. For winter days there is no important changes in RMS and BIAS. For examples in April 2003 there is some impact, but changes in RMS and BIAS are really small, smaller than 0.002 for H2m and smaller than 0.02 °C for T2m. For May example RMS is better sometimes for operational and sometime for smoothed SWI forecasts. Maximum differences for H2m are RMS=0.005 and for BIAS=0.013. For T2m maximum differences are RMS=0.05 BIAS=0.11.

For June 2002 with very high temperatures RMS is better for runs with smoothed SWI, maximum improvement of RMS for H2m is 0.022. For H2m and BIAS more times operational forecast is better than run with smoothed SWI, maximum difference for BIAS=0.024. For T2m RMS is usually better for smoothed SWI highest differences are for 12, 36 and 18 hrs forecast, maximum for RMS=0.33 °C. For all experiments BIAS is usually less than zero. Operational run is better for BIAS and difference is higher for 12, 18, 36 and 42 hrs forecasts. Maximal difference for BIAS=0.37 °C.

On next figures RMS and BIAS for all examples are shown.

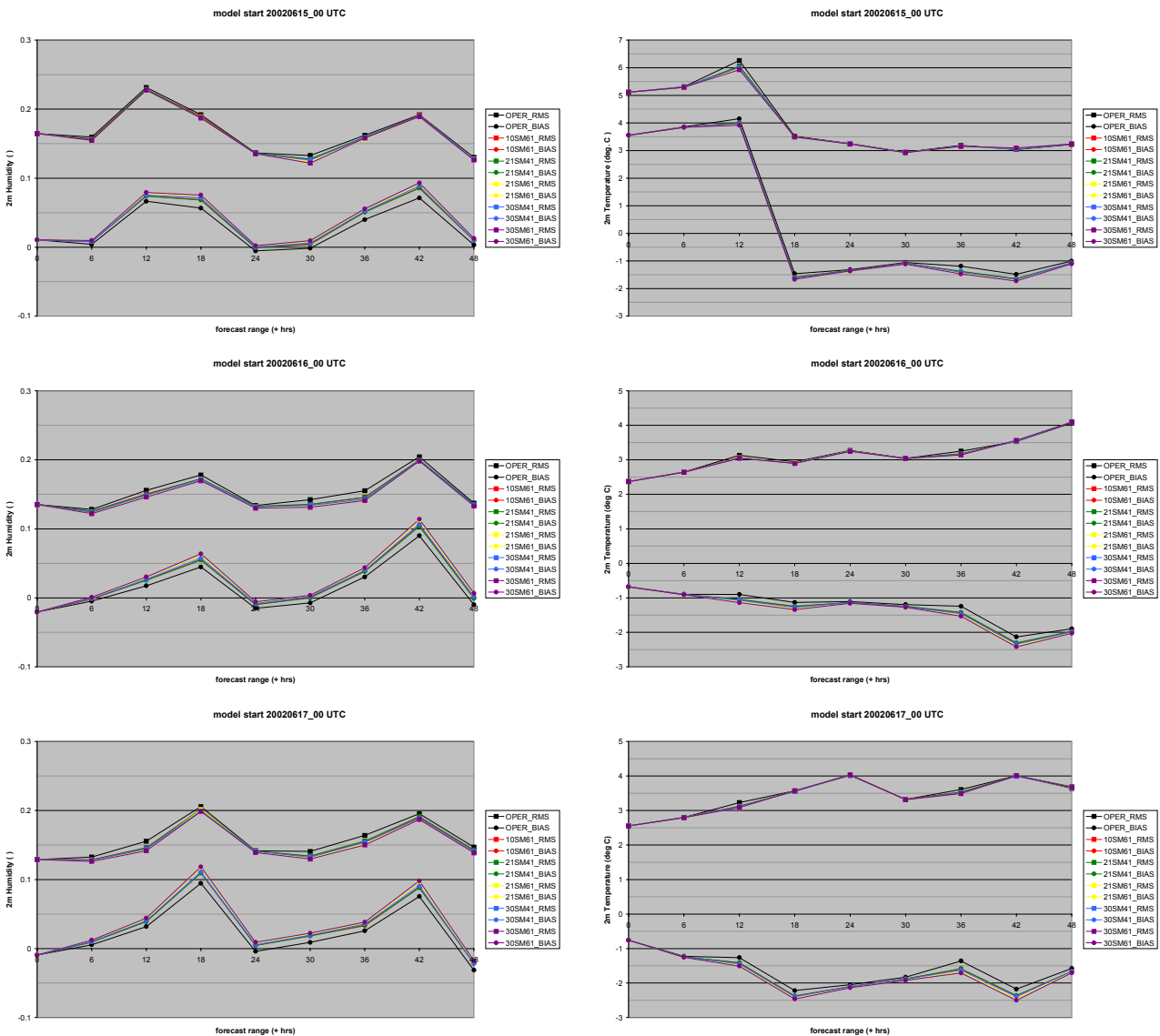


Figure 16 BIAS and RMS for T2m and H2m for period 15th-17th June 2002 00 UTC runs

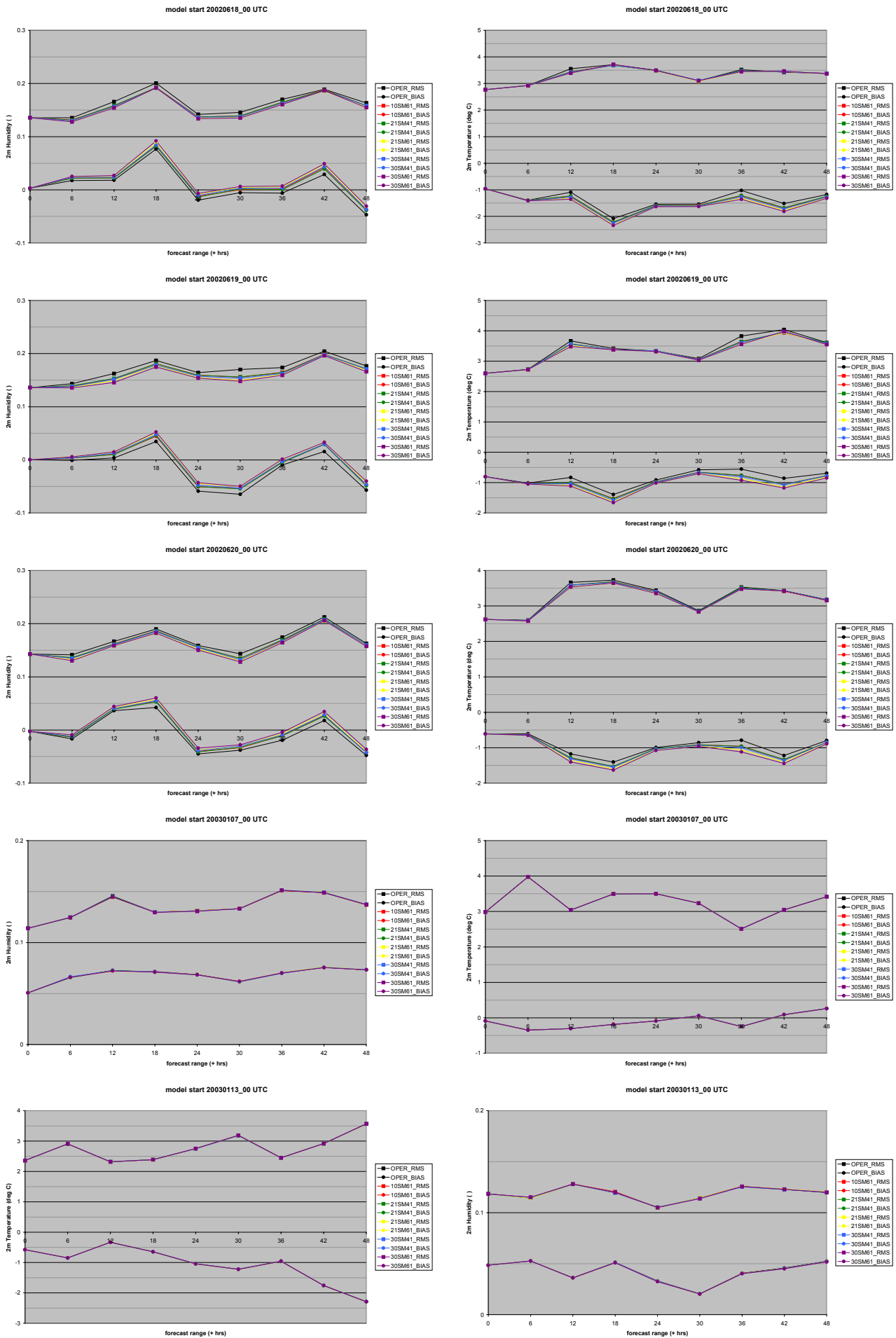


Figure 17 Same like on Figure 13 for period 18th-20th June 2002 and for 7th and 13th January 2003

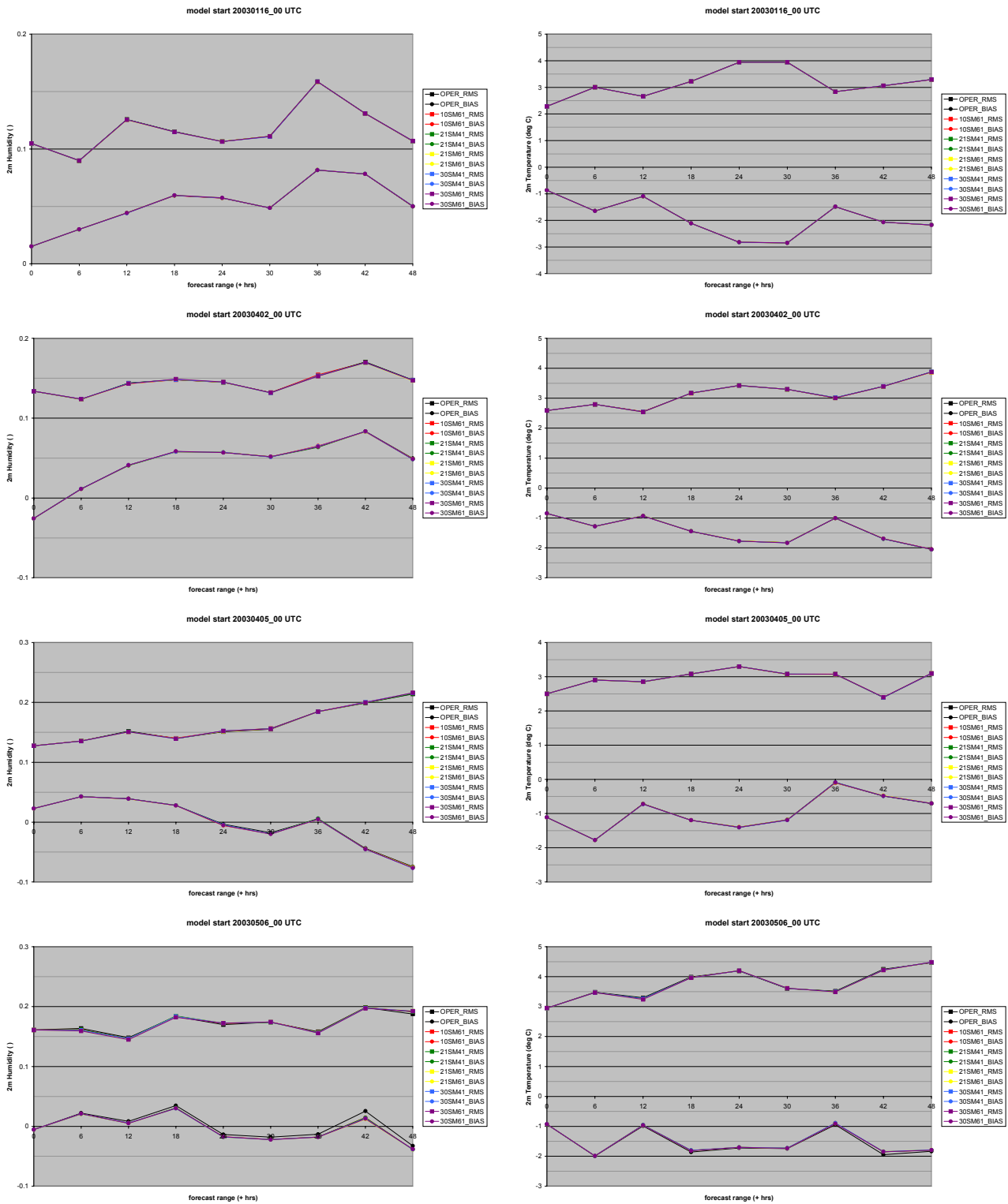


Figure 18 BIAS and RMS for H2m and T2m for 16th January, 2nd and 5th April and 6th May, 2003 00 UTC runs

During the January and beginning of April there is no some important changes in RMS and BIAS. During the worm period RMS is usually better for smoothed runs and BIAS for oper run. If there is some impact on BIAS for T2m than there is opposite impact on H2m (in term of sign of), same is for H2m and T2m. This is case for all warm situations.

7. Comparison for period in June 2002

First comparison against to the operational run is shown, than comparison against 21SM61 smoothing.

7.1. Comparison of oper run and smoothings for period in June 2002

In Table 1 statistics for 3 kinds of weight are calculated.

Class “+++” means that there is big improvement of forecast (greater than 2 °C or 5 %), “++” is for improvement (1-2 °C or 2-5 %) and class “+” means small improvement in forecast (0.5-1 °C or 0.5-2 %).

Same is for “-” classes, but for worse forecasts.

In Table 1 for 1st weight (explained below) and in Table 2 if the sign in table is great than zero than more points have better forecast.

1st weight “1*+++1*+++1*+1*-1*--1*---” that means same weight for all classes, it is possible to see how many points have better or worst for all run. For period 15th – 20th Jun 2002 just once forecast with smoothed initial SWI for T2m have negative sign, 21SM61 for 17th Jun. For all other, forecasts with smoothed SWI were better.

2nd weight is “2*+++1.5*+++1*+1*-2*--3*---” weight for worst forecast is little bit bigger than for better forecast.

Last (3rd) “2*+++1.5*+++1*+1*-3*--4*---” have even bigger weight for worst forecast. That means if we don’t want to risk too much but to have some small improvement these classes show us which one to choose.

Table 1 Comparison of number of better and worse points in comparison of oper run with smoothings runs, with different weights, for all days (15-20) and forecasts hours (00, 06,..., 48)

T2m 200206_15-20_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*+++1*+1*-3*--4*---	-448	-437	-830	-595	-1213
2*+++1.5*+++1*+1*-2*--3*---	344	308	416	398	275
1*+++1*+++1*+1*-1*--1*---	605	538	853	725	885
H2m 200206_15-20_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*+++1*+1*-3*--4*---	1051	1044	1072	1189	903
2*+++1.5*+++1*+1*-2*--3*---	2544	2457	3153	2894	3246
1*+++1*+++1*+1*-1*--1*---	2723	2608	3238	2943	3329

From Table 1 it look likes that there is no lot of data, which could help to find the best solutions of smoothing parameters. 21SM61 has the best results for 2nd weight in T2m and 2nd place in H2m. For 1st class the best are: 30SM61 for T2m and for H2m, 21SM61 are 2nd for both.

In 3rd class the best one are 21SM41 and 30SM41 for H2m.

Table 2 Comparison of number of better and worse points in comparison of oper run with smoothings runs, with different weights, for all forecast hours (00, 06,..., 48)

T2m 20020615_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*+++1*+1*-3*--4*---	-48	-48	-71	-77	-136
2*+++1.5*+++1*+1*-2*--3*---	38	36	74	37	38
1*+++1*+++1*+1*-1*--1*---	54	53	109	63	98
H2m 20020615_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*+++1*+1*-3*--4*---	-26	-9	-84	-65	-121
2*+++1.5*+++1*+1*-2*--3*---	192	206	212	197	229
1*+++1*+++1*+1*-1*--1*---	246	264	290	261	325

Table 2 Continuation of Table: Comparison of number of better and worse points in comparison of oper run with smoothings runs, with different weights, for all forecast hours (00, 06,..., 48)

T2m 20020616_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	-110	-100	-215	-152	-258
2*+++1.5*++1*+1*-2*--3*---	11	14	-30	-2	-46
1*+++1*++1*+1*-1*--1*---	56	53	47	53	56
H2m 20020616_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	192	173	234	285	219
2*+++1.5*++1*+1*-2*--3*---	415	378	528	524	551
1*+++1*++1*+1*-1*--1*---	407	371	502	488	525
T2m 20020617_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	-201	-232	-339	-247	-408
2*+++1.5*++1*+1*-2*--3*---	-44	-79	-92	-61	-129
1*+++1*++1*+1*-1*--1*---	27	-6	47	23	39
H2m 20020617_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	257	232	243	292	221
2*+++1.5*++1*+1*-2*--3*---	510	470	599	582	610
1*+++1*++1*+1*-1*--1*---	513	473	604	563	594
T2m 20020618_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	-84	-68	-191	-133	-306
2*+++1.5*++1*+1*-2*--3*---	78	83	52	76	3
1*+++1*++1*+1*-1*--1*---	145	147	150	169	153
H2m 20020618_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	158	168	64	146	5
2*+++1.5*++1*+1*-2*--3*---	455	448	495	485	480
1*+++1*++1*+1*-1*--1*---	523	506	551	523	558
T2m 20020619_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	53	66	91	112	32
2*+++1.5*++1*+1*-2*--3*---	196	202	307	281	294
1*+++1*++1*+1*-1*--1*---	216	210	324	287	327
H2m 20020619_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	362	404	446	415	461
2*+++1.5*++1*+1*-2*--3*---	613	634	808	715	855
1*+++1*++1*+1*-1*--1*---	614	615	750	679	766
T2m 20020620_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	-58	-56	-106	-98	-138
2*+++1.5*++1*+1*-2*--3*---	66	53	104	67	116
1*+++1*++1*+1*-1*--1*---	107	81	176	130	212
H2m 20020620_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	109	78	170	116	119
2*+++1.5*++1*+1*-2*--3*---	360	323	512	392	523
1*+++1*++1*+1*-1*--1*---	420	379	541	429	561
T2m 20030506_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	-11	2	-30	-24	-29
2*+++1.5*++1*+1*-2*--3*---	37	45	64	48	76
1*+++1*++1*+1*-1*--1*---	46	51	82	69	93
H2m 20030506_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
2*+++1.5*++1*+1*-3*--4*---	-335	-337	-413	-382	-447
2*+++1.5*++1*+1*-2*--3*---	-159	-150	-143	-153	-134
1*+++1*++1*+1*-1*--1*---	-50	-47	3	-30	39

Table 3 Comparison of numbers of worse points in comparison of oper run with smoothings runs, for all days (15-20) and forecasts hours (00, 06,..., 48) for T2m

T2m 200206_15-20_00	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
Just worse forecasts	-160	-180	-193	-180	-237

We are searching for smoothing with highest values in Tables 1, 2 and 3.

In Table 3 sum of just T2m forecasts worse than operational one during the period 15th – 20th June 2002.

Such table for H2m is not available because for all forecast hours smoothed forecasts have more betters than worse forecasts.

From Table 3 it is possible to conclude that just last one 21SM61 have more worse points than other one, if we take in account just worse points it is possible to eliminate 21SM61.

For problematic period smoothing 21SM61 have or the best one or second results for T2m and for 1st weight, same is for May example.

For H2m results for 21SM41 are usually in a middle or in a better part, same is for May example.

7.2. Comparison of 21SM61 smoothing with others for period in June 2002

In following tables comparison of 21SM61 smoothing with OPER run and other smoothings for period in June 2002 are shown. In the Table 4 if $D < 0$ (first 3 rows) means that absolute error for smoothing 21SM61 is lower than for other. 2161 is 21SM61, 3041 is 31SM41, etc. If the background is yellow means that more points have smaller than greater absolute error. If the background is yellow in first tree rows ($D < 0$), in Tables 4 and 5, 21SM61 smoothing have more points with better forecast. If the background is yellow in last tree rows ($D > 0$), in Tables 4 and 5, 21SM61 smoothing have more points with worst forecast.

Table 4 Number of better and worse points for T2m in comparison of 20SM61 with other runs (OPER and other smoothings: 10SM61, 21SM41, 30SM41 and 30SM61), sum for all forecasts hours: 00, 06, 12... 48 UTC, and for whole period, 15th-20th of June 2002

T2m 00,06,...,48	2161 - OPER	2161 - 1061	2161 - 2141	2161 - 3041	2161 - 3061
T2m_all_D <= -2 C	433	39	45	13	9
-2 C < D <= -1 C	1228	259	290	119	50
-1 C < D <= -.5 C	2287	857	916	532	400
-.5 C < D < .5 C	27179	32090	31920	33013	33318
.5 C <= D < 1 C	1849	743	798	440	374
1 C <= D < 2 C	1008	220	235	100	66
2 C <= D	238	14	18	5	5

Table 5 Number of better and worse points for H2m in comparison of 20SM61 with other runs (OPER and other smoothings: 10SM61, 21SM41, 30SM41 and 30SM61), sum for all forecasts hours: 00, 06, 12... 48 UTC, and for whole period, 15th-20th of June 2002

H2m 00,06,...,48	2161 - OPER	2161 - 1061	2161 - 2141	2161 - 3041	2161 - 3061
H2m_all_D <= -10 %	1269	159	179	78	57
-10 % < D <= -5 %	2755	792	884	407	303
-5 % < D <= -2 %	4522	3230	3288	2419	1624
-2 % < D < 2 %	20219	27102	26744	28992	29753
2 % <= D < 5 %	3227	2167	2328	1763	1974
5 % <= D < 10 %	1430	488	517	330	305
10 % <= D	651	135	133	84	57

If we compare all forecasts hour and whole period smoothing 21SM61 is better than others. Just smoothings 30SM41 and 30SM61 are better for some classes.

In tables 6 and 7 comparison are made separately for every forecast for whole period, 15th-20th of June 2002.

Table 6 Number of better and worse points for T2m in comparison of 20SM61 with other runs (OPER, 10SM61, 21SM41, 30SM41 and 30SM61), for 06, 12... 48 UTC, 15th-20th of June 2002

T2m 15-20.06.2002	2161 - OPER	2161 - 1061	2161 - 2141	2161 - 3041	2161 - 3061
06 D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	4	1	1	0	0
-1 C < D <= -.5 C	58	14	17	10	4
-.5 C < D < .5 C	3849	3927	3926	3937	3938
.5 C <= D < 1 C	35	7	5	2	7
1 C <= D < 2 C	3	0	0	0	0
2 C <= D	0	0	0	0	0
12 D <= -2 C	136	10	11	2	1
-2 C < D <= -1 C	311	75	80	30	8
-1 C < D <= -.5 C	377	173	192	135	57
-.5 C < D < .5 C	2681	3554	3523	3690	3762
.5 C <= D < 1 C	279	93	99	60	84
1 C <= D < 2 C	131	24	24	13	18
2 C <= D	15	1	1	0	0
18 D <= -2 C	59	6	7	2	1
-2 C < D <= -1 C	192	33	39	17	11
-1 C < D <= -.5 C	326	126	137	64	78
-.5 C < D < .5 C	2751	3463	3432	3617	3669
.5 C <= D < 1 C	247	141	148	99	56
1 C <= D < 2 C	185	56	60	29	13
2 C <= D	71	6	8	3	3
24 D <= -2 C	7	1	0	0	1
-2 C < D <= -1 C	75	12	16	5	3
-1 C < D <= -.5 C	218	71	71	45	25
-.5 C < D < .5 C	3033	3461	3448	3516	3546
.5 C <= D < 1 C	185	48	53	30	20
1 C <= D < 2 C	78	6	11	3	4
2 C <= D	3	0	0	0	0
30 D <= -2 C	3	0	0	0	0
-2 C < D <= -1 C	74	10	8	5	3
-1 C < D <= -.5 C	246	63	71	35	22
-.5 C < D < .5 C	3376	3809	3803	3879	3890
.5 C <= D < 1 C	196	55	53	22	23
1 C <= D < 2 C	44	4	6	0	3
2 C <= D	2	0	0	0	0
36 D <= -2 C	145	14	16	5	2
-2 C < D <= -1 C	274	73	86	37	6
-1 C < D <= -.5 C	440	190	192	112	82
-.5 C < D < .5 C	2508	3457	3420	3674	3727
.5 C <= D < 1 C	299	151	166	75	91
1 C <= D < 2 C	210	39	43	21	16
2 C <= D	49	1	2	1	1
42 D <= -2 C	66	6	9	4	4
-2 C < D <= -1 C	190	38	40	15	15
-1 C < D <= -.5 C	334	122	129	75	107
-.5 C < D < .5 C	2559	3419	3397	3603	3643
.5 C <= D < 1 C	362	174	181	111	59
1 C <= D < 2 C	245	72	75	28	8
2 C <= D	81	6	6	1	1
48 D <= -2 C	17	2	2	0	0
-2 C < D <= -1 C	108	17	20	10	4
-1 C < D <= -.5 C	288	98	107	56	25
-.5 C < D < .5 C	2813	3391	3362	3488	3534
.5 C <= D < 1 C	246	74	93	41	34
1 C <= D < 2 C	112	19	16	6	4
2 C <= D	17	0	1	0	0

Table 7 Number of better and worse points for H2m in comparison of 20SM61 with other runs (OPER, 10SM61, 21SM41, 30SM41 and 30SM61), for 06, 12... 48 UTC, 15th-20th of June 2002

H2m 15-20.06.2002	2161 - OPER	2161 - 1061	2161 - 2141	2161 - 3041	2161 - 3061
06 D <= -10 %	47	4	5	1	1
-10 % < D <= -5 %	187	41	44	19	8
-5 % < D <= -2 %	450	253	244	174	82
-2 % < D < 2 %	2918	3525	3512	3642	3708
2 % <= D < 5 %	281	113	129	96	134
5 % <= D < 10 %	47	5	6	9	8
10 % <= D	11	0	1	0	0
12 D <= -10 %	205	11	13	5	5
-10 % < D <= -5 %	435	100	120	47	35
-5 % < D <= -2 %	688	489	496	318	172
-2 % < D < 2 %	1911	2995	2932	3335	3450
2 % <= D < 5 %	414	255	290	171	227
5 % <= D < 10 %	193	58	61	32	25
10 % <= D	71	9	5	9	3
18 D <= -10 %	241	39	44	25	15
-10 % < D <= -5 %	404	148	165	62	72
-5 % < D <= -2 %	556	478	485	381	295
-2 % < D < 2 %	1766	2625	2567	2908	2977
2 % <= D < 5 %	418	358	374	309	354
5 % <= D < 10 %	254	106	120	88	73
10 % <= D	163	48	47	29	16
24 D <= -10 %	55	8	10	5	4
-10 % < D <= -5 %	223	58	68	30	21
-5 % < D <= -2 %	477	308	294	214	134
-2 % < D < 2 %	2303	2987	2956	3150	3218
2 % <= D < 5 %	387	171	211	148	164
5 % <= D < 10 %	108	42	32	27	32
10 % <= D	25	4	7	4	5
30 D <= -10 %	170	21	23	9	6
-10 % < D <= -5 %	309	99	107	55	25
-5 % < D <= -2 %	587	381	394	337	208
-2 % < D < 2 %	2290	3115	3084	3263	3377
2 % <= D < 5 %	389	263	277	237	277
5 % <= D < 10 %	160	51	49	31	37
10 % <= D	29	4	0	2	4
36 D <= -10 %	225	16	20	7	3
-10 % < D <= -5 %	507	124	141	50	27
-5 % < D <= -2 %	676	487	516	331	238
-2 % < D < 2 %	1697	2869	2827	3249	3379
2 % <= D < 5 %	452	353	327	239	228
5 % <= D < 10 %	253	54	74	32	36
10 % <= D	105	12	10	7	4
42 D <= -10 %	243	52	56	20	19
-10 % < D <= -5 %	418	162	159	101	86
-5 % < D <= -2 %	611	473	502	415	335
-2 % < D < 2 %	1578	2566	2469	2795	2937
2 % <= D < 5 %	485	389	444	364	353
5 % <= D < 10 %	260	122	129	88	65
10 % <= D	218	49	54	30	18
48 D <= -10 %	83	8	8	6	4
-10 % < D <= -5 %	272	60	80	43	29
-5 % < D <= -2 %	477	361	357	249	160
-2 % < D < 2 %	2166	2830	2807	3060	3117
2 % <= D < 5 %	401	265	276	199	237
5 % <= D < 10 %	155	50	46	23	29
10 % <= D	29	9	9	3	7

For all forecasts: 06, 12, 18, 24, 30, 36 and 48 21SM61 smoothing are usually better than other smoothing except for 31SM61 smoothing.

7.3. Comparison of 21SM61 and 30SM61 smoothings for period in June 2002

In following tables comparison of 21SM61 and 30SM61 smoothings are shown. If the number in tables is less than 0 21SM61 smoothing have better forecast.

Table 8 Comparison of number of better and worse points for T2m in comparison of 20SM61 with 30SM61 smoothings runs, with different weights, $|\text{err}(21\text{SM61})| - |\text{err}(30\text{SM61})|$, 15th-20th of June 2002

T2m 20020615-20_00	T2m +06	T2m +12	T2m +18	T2m +24	T2m +30	T2m +36	T2m +42	T2m +48
2*+++1.5*++1*+1*-3*--4*---	3	26	-33.5	-12	-3.5	9	-95	3
2*+++1.5*++1*+1*-2*--3*---	3	35	-21.5	-8	-0.5	17	-76	7
1*+++1*++1*+1*-1*--1*---	3	36	-18	-5	1	18	-58	9

Table 9 Comparison of number of better and worse points for H2m in comparison of 20SM61 with 30SM61 smoothings runs, with different weights, $|\text{err}(21\text{SM61})| - |\text{err}(30\text{SM61})|$ 15th-20th of June 2002

H2m 20020615-20_00	H2m +06	H2m +12	H2m +18	H2m +24	H2m +30	H2m +36	H2m +42	H2m +48
2*+++1.5*++1*+1*-3*--4*---	36	-26.5	-75.5	9	33.5	-41	-182.5	31.5
2*+++1.5*++1*+1*-2*--3*---	45	13.5	11.5	34	64.5	-11	-77.5	64.5
1*+++1*++1*+1*-1*--1*---	51	43	61	42	79	0	-4	80

With comparison of just two smoothing for T2m and H2m it is not clear which smoothing is better. If more weight is given to bigger improvement than results are better for 21SM61, especially it is case for H2m.

8. Conclusion

During the hot summer days, hot spots appear in 2m Temperature field, caused by small scales features in the soil moisture. They are the consequences of switching condition in the surface analysis and of connective precipitation which both have high degree of uncertainties. More over this smoothing is coherent with the soil moisture analysis which is not able to connect spatial scales lower than 100 km because of the Surface Observations network. Surface analysis is made in ARPEGE.

When the smoothing of SWI is applied, during the winter there is some visible changes of SWI on Istria peninsula, Apennine peninsula Sicily and Africa, for other areas changes are to small, or there are not changes at all. During the summer smoothing for the same number of smoothing with 6.1 km smooth SWI field more than with 4.1 km, like it was expected. Smoothed field for 21SM41 looks similar with 10SM61. For smoothing 21SM61 there is still some details in SWI field, what is not case for 30SM61, maybe 30SM61 is to smooth.

With smoothed SWI there are no anymore-such big gradients in T2m field like it was in Operational run. For some points T2m is smaller for more than 2 °C if we compare operational run and smoothing with 21 or 30 smoothings with radius of smoothing 6.1 km.

For winter days there is no important changes in RMS and BIAS. For examples in April 2003 there is some small impact. For May example RMS is better sometimes for operational and sometime for smoothed SWI forecasts. For June 2002 with very high temperatures RMS is better for runs with smoothed SWI, maximum improvement of RMS for H2m is 0.022. For H2m and BIAS more times

operational forecast is better than run with smoothed SWI, maximum difference for BIAS=0.024. For T2m RMS is usually better for smoothed SWI highest differences are for 12, 36 and 18 hrs forecast. Maximum for RMS=0.334 °C. For all experiments BIAS is usually less than zero. Operational run is better for BIAS and difference is higher for 12, 18, 36 and 42 hrs forecasts. Maximal difference for BIAS=0.369 °C.

If there is wish to smooth SWI proposal is to use 21SM61 smoothing, results for the period 15th – 20th June 2002 are the best. It is very important to make forecast worst in minimal number of points. If somebody like to use it 21 means 21 smoothings are apply and 61 is for radius of smoothing is 6.1 km (half of the horizontal grid).

Some longer parallel test during the late spring and summer is needed to conclude if the impact of smoothing SWI will improve or not the 2 m scores. The best solution is to improve assimilation in ARPEGE or to apply smoothing of SWI in ARPEGE than it is not needed in ALADIN.

T2m	2002061500+000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	609	609	609	609	609
	mean:	-0.00017	-0.00013	-0.00009	-0.00032	-0.00024
	D <= -2 C	0	0	0	0	0
	-2 C < D <= -1 C	0	0	0	0	0
	-1 C < D <= -0.5 C	0	0	0	0	0
	-0.5 C < D < 0.5 C	609	609	609	609	609
	0.5 C <= D < 1 C	0	0	0	0	0
	1 C <= D < 2 C	0	0	0	0	0
	2 C <= D	0	0	0	0	0
H2m	2002061500+000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	608	608	608	608	608
	mean:	-0.00002	-0.00001	-0.00001	-0.00003	0.00000
	D <= -10 %	0	0	0	0	0
	-10 % < D <= -5 %	0	0	0	0	0
	-5 % < D <= -2 %	0	0	0	0	0
	-2 % < D < 2 %	608	608	608	608	608
	2 % <= D < 5 %	0	0	0	0	0
	5 % <= D < 10 %	0	0	0	0	0
	10 % <= D	0	0	0	0	0
T2m	2002061500+006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	663	663	663	663	663
	mean:	0.01637	0.01490	0.01142	0.01252	0.01578
	D <= -2 C	0	0	0	0	0
	-2 C < D <= -1 C	0	0	0	0	0
	-1 C < D <= -0.5 C	2	3	3	4	2
	-0.5 C < D < 0.5 C	655	656	651	653	651
	0.5 C <= D < 1 C	5	4	8	6	9
	1 C <= D < 2 C	1	0	1	0	1
	2 C <= D	0	0	0	0	0
H2m	2002061500+006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	662	662	662	662	662
	mean:	0.00220	0.00261	0.00377	0.00330	0.00360
	D <= -10 %	1	0	2	1	2
	-10 % < D <= -5 %	5	6	6	5	10
	-5 % < D <= -2 %	39	33	50	45	51
	-2 % < D < 2 %	541	553	511	530	511
	2 % <= D < 5 %	57	56	60	57	50
	5 % <= D < 10 %	14	10	27	19	30
	10 % <= D	5	4	6	5	8
T2m	2002061500+012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	658	658	658	658	658
	mean:	0.15667	0.14375	0.22400	0.18054	0.23889
	D <= -2 C	0	0	1	0	2
	-2 C < D <= -1 C	3	3	2	2	16
	-1 C < D <= -0.5 C	33	48	43	47	39
	-0.5 C < D < 0.5 C	519	517	471	498	462
	0.5 C <= D < 1 C	39	45	50	49	45
	1 C <= D < 2 C	52	48	47	44	54
	2 C <= D	12	11	35	21	38
H2m	2002061500+012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	655	655	655	655	655
	mean:	0.00491	0.00471	0.00661	0.00520	0.00614
	D <= -10 %	7	9	16	8	20
	-10 % < D <= -5 %	29	27	38	42	50
	-5 % < D <= -2 %	70	76	71	68	68
	-2 % < D < 2 %	394	387	340	364	319
	2 % <= D < 5 %	84	93	104	100	103
	5 % <= D < 10 %	59	50	61	57	70
	10 % <= D	12	13	25	16	25
T2m	2002061500+018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	645	645	645	645	645
	mean:	0.00137	0.00687	0.01116	0.01730	-0.00175
	D <= -2 C	4	4	9	7	0
	-2 C < D <= -1 C	17	16	24	20	28
	-1 C < D <= -0.5 C	32	30	23	29	29
	-0.5 C < D < 0.5 C	535	534	517	524	505
	0.5 C <= D < 1 C	36	39	40	34	36
	1 C <= D < 2 C	17	18	22	22	27
	2 C <= D	4	4	10	8	10
H2m	2002061500+018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	636	636	636	636	636
	mean:	0.00278	0.00371	0.00508	0.00523	0.00632
	D <= -10 %	16	15	21	17	24
	-10 % < D <= -5 %	26	22	32	27	34
	-5 % < D <= -2 %	68	64	82	67	75
	-2 % < D < 2 %	378	392	337	372	319
	2 % <= D < 5 %	87	86	79	80	92
	5 % <= D < 10 %	42	39	56	46	50
	10 % <= D	19	18	29	27	42
T2m	2002061500+024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	598	598	598	598	598
	mean:	0.00465	0.00422	0.01497	0.00475	0.01948
	D <= -2 C	1	1	0	0	1
	-2 C < D <= -1 C	4	3	8	8	8
	-1 C < D <= -0.5 C	21	24	19	19	25
	-0.5 C < D < 0.5 C	554	554	537	549	524
	0.5 C <= D < 1 C	17	15	24	17	30
	1 C <= D < 2 C	1	1	7	5	10
	2 C <= D	0	0	0	0	0

H2m	2002061500+024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	594	594	594	594	594
	mean:	0.00068	0.00070	0.00056	0.00047	0.00071
	D <= -10 %	1	2	3	2	2
	-10 % < D <= -5 %	9	8	20	15	24
	-5 % < D <= -2 %	45	52	60	52	58
	-2 % < D < 2 %	477	465	417	448	417
	2 % <= D < 5 %	45	51	64	54	63
	5 % <= D < 10 %	15	14	27	19	26
	10 % <= D	2	2	3	4	4
T2m	2002061500+030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	652	652	652	652	652
	mean:	0.01129	0.00362	0.02126	0.01336	0.02036
	D <= -2 C	0	0	0	0	0
	-2 C < D <= -1 C	4	4	6	5	9
	-1 C < D <= -0.5 C	11	12	18	18	26
	-0.5 C < D < 0.5 C	617	618	591	603	578
	0.5 C <= D < 1 C	20	18	29	23	26
	1 C <= D < 2 C	0	0	8	3	12
	2 C <= D	0	0	0	0	1
H2m	2002061500+030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	651	651	651	651	651
	mean:	0.00435	0.00420	0.00664	0.00539	0.00837
	D <= -10 %	0	0	5	7	6
	-10 % < D <= -5 %	9	10	13	12	15
	-5 % < D <= -2 %	48	52	58	54	54
	-2 % < D < 2 %	485	469	441	457	434
	2 % <= D < 5 %	69	76	79	75	80
	5 % <= D < 10 %	27	29	36	33	40
	10 % <= D	8	10	18	13	23
T2m	2002061500+036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	659	659	659	659	659
	mean:	0.03170	0.03521	0.04510	0.04122	0.04107
	D <= -2 C	2	3	6	5	9
	-2 C < D <= -1 C	14	13	25	17	26
	-1 C < D <= -0.5 C	48	44	44	39	49
	-0.5 C < D < 0.5 C	526	530	487	521	463
	0.5 C <= D < 1 C	34	35	53	37	69
	1 C <= D < 2 C	31	30	31	31	32
	2 C <= D	4	4	13	9	11
H2m	2002061500+036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	658	658	658	658	658
	mean:	0.00473	0.00451	0.00694	0.00515	0.00650
	D <= -10 %	2	3	15	5	16
	-10 % < D <= -5 %	31	33	33	39	41
	-5 % < D <= -2 %	99	93	93	97	100
	-2 % < D < 2 %	359	368	322	337	292
	2 % <= D < 5 %	94	91	102	98	104
	5 % <= D < 10 %	56	58	69	59	72
	10 % <= D	17	15	24	23	33
T2m	2002061500+042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	628	628	628	628	628
	mean:	-0.05568	-0.05572	-0.07493	-0.06904	-0.10382
	D <= -2 C	4	4	9	4	14
	-2 C < D <= -1 C	23	23	34	32	37
	-1 C < D <= -0.5 C	47	44	49	48	52
	-0.5 C < D < 0.5 C	497	504	472	488	457
	0.5 C <= D < 1 C	41	38	41	35	44
	1 C <= D < 2 C	15	14	16	19	18
	2 C <= D	1	1	7	2	6
H2m	2002061500+042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	627	627	627	627	627
	mean:	-0.00017	0.00067	0.00227	0.00093	0.00271
	D <= -10 %	18	17	32	25	37
	-10 % < D <= -5 %	46	42	37	41	46
	-5 % < D <= -2 %	63	66	75	68	69
	-2 % < D < 2 %	344	340	299	328	278
	2 % <= D < 5 %	100	103	106	96	115
	5 % <= D < 10 %	42	45	48	51	50
	10 % <= D	14	14	30	18	34
T2m	2002061500+048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	593	593	593	593	593
	mean:	-0.00349	0.00617	0.01050	-0.00123	0.00990
	D <= -2 C	0	0	0	0	1
	-2 C < D <= -1 C	10	9	16	13	18

T2m	2002061600+000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061600+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	598	598	598	598	598		total nr.:	591	591	591	591	591
	mean:	-0.00001	-0.00003	-0.00004	-0.00002	0.00005		mean:	0.00136	0.00096	0.00233	0.00220	0.00333
	D <= -2 C	0	0	0	0	0		D <= -10 %	2	2	2	2	1
	-2 C < D <= -1 C	0	0	0	0	0		-10 % < D <= -5 %	7	6	14	6	13
	-1 C < D <= -0.5 C	0	0	0	0	0		-5 % < D <= -2 %	50	48	59	55	64
	-0.5 C < D < 0.5 C	598	598	598	598	598		-2 % < D < 2 %	452	463	419	434	411
	0.5 C <= D < 1 C	0	0	0	0	0		2 % <= D < 5 %	63	53	61	69	63
	1 C <= D < 2 C	0	0	0	0	0		5 % <= D < 10 %	15	18	32	20	31
	2 C <= D	0	0	0	0	0		10 % <= D	2	1	4	4	8
H2m	2002061600+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061600+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	594	594	594	594	594		total nr.:	658	658	658	658	658
	mean:	-0.00002	-0.00004	-0.00002	-0.00002	-0.00005		mean:	0.00948	0.00947	0.02008	0.00932	0.01657
	D <= -10 %	0	0	0	0	0		D <= -2 C	0	0	0	0	0
	-10 % < D <= -5 %	0	0	0	0	0		-2 C < D <= -1 C	3	2	6	4	4
	-5 % < D <= -2 %	0	0	0	0	0		-1 C < D <= -0.5 C	22	20	29	26	32
	-2 % < D < 2 %	594	594	594	594	594		-0.5 C < D < 0.5 C	609	614	580	596	576
	2 % <= D < 5 %	0	0	0	0	0		0.5 C <= D < 1 C	19	18	30	23	32
	5 % <= D < 10 %	0	0	0	0	0		1 C <= D < 2 C	5	4	13	9	14
	10 % <= D	0	0	0	0	0		2 C <= D	0	0	0	0	0
T2m	2002061600+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061600+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	652	652	652	652	652		total nr.:	657	657	657	657	657
	mean:	0.00246	0.00348	0.00927	0.00260	0.00662		mean:	0.00647	0.00589	0.00857	0.00717	0.00889
	D <= -2 C	0	0	0	0	0		D <= -10 %	0	1	0	0	0
	-2 C < D <= -1 C	1	1	1	1	1		-10 % < D <= -5 %	21	20	23	22	26
	-1 C < D <= -0.5 C	1	0	1	0	2		-5 % < D <= -2 %	44	50	50	51	59
	-0.5 C < D < 0.5 C	648	651	644	647	643		-2 % < D < 2 %	461	460	420	435	409
	0.5 C <= D < 1 C	2	0	6	4	5		2 % <= D < 5 %	81	84	94	92	87
	1 C <= D < 2 C	0	0	0	0	1		5 % <= D < 10 %	35	31	43	38	45
	2 C <= D	0	0	0	0	0		10 % <= D	14	11	24	17	28
H2m	2002061600+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061600+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	651	651	651	651	651		total nr.:	655	655	655	655	655
	mean:	0.00202	0.00181	0.00382	0.00276	0.00436		mean:	0.09627	0.08463	0.13078	0.11131	0.13420
	D <= -10 %	1	1	1	1	1		D <= -2 C	1	1	4	2	5
	-10 % < D <= -5 %	9	8	7	9	7		-2 C < D <= -1 C	22	23	33	30	37
	-5 % < D <= -2 %	24	28	36	30	38		-1 C < D <= -0.5 C	38	42	47	39	40
	-2 % < D < 2 %	551	553	522	546	515		-0.5 C < D < 0.5 C	489	491	441	467	437
	2 % <= D < 5 %	50	48	61	48	59		0.5 C <= D < 1 C	56	52	70	63	74
	5 % <= D < 10 %	12	10	15	12	22		1 C <= D < 2 C	41	38	37	37	36
	10 % <= D	4	3	9	5	9		2 C <= D	8	8	23	17	26
T2m	2002061600+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061600+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	659	659	659	659	659		total nr.:	655	655	655	655	655
	mean:	0.07035	0.07189	0.09285	0.08659	0.09351		mean:	0.01053	0.01061	0.01416	0.01279	0.01473
	D <= -2 C	2	3	4	3	4		D <= -10 %	6	5	9	8	9
	-2 C < D <= -1 C	11	11	19	13	23		-10 % < D <= -5 %	23	24	35	25	39
	-1 C < D <= -0.5 C	34	27	36	36	36		-5 % < D <= -2 %	76	68	61	62	64
	-0.5 C < D < 0.5 C	533	548	503	529	490		-2 % < D < 2 %	351	356	283	326	276
	0.5 C <= D < 1 C	46	41	47	41	54		2 % <= D < 5 %	105	112	114	113	110
	1 C <= D < 2 C	29	27	35	31	38		5 % <= D < 10 %	69	70	89	78	91
	2 C <= D	4	4	14	9	14		10 % <= D	25	20	43	36	46
H2m	2002061600+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061600+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	658	658	658	658	658		total nr.:	648	648	648	648	648
	mean:	0.00570	0.00610	0.00967	0.00783	0.01045		mean:	-0.02996	-0.02246	-0.05845	-0.04153	-0.08078
	D <= -10 %	7	5	13	9	13		D <= -2 C	3	2	11	6	14
	-10 % < D <= -5 %	19	18	22	24	28		-2 C < D <= -1 C	36	34	41	39	51
	-5 % < D <= -2 %	79	69	79	71	88		-1 C < D <= -0.5 C	46	46	61	50	60
	-2 % < D < 2 %	379	404	335	361	310		-0.5 C < D < 0.5 C	497	498	455	484	440
	2 % <= D < 5 %	105	101	117	118	114		0.5 C <= D < 1 C	44	47	49	44	47
	5 % <= D < 10 %	55	50	63	55	72		1 C <= D < 2 C	16	17	21	16	30
	10 % <= D	14	11	29	20	33		2 C <= D	6	4	10	9	6
T2m	2002061600+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061600+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	628	628	628	628	628		total nr.:	645	645	645	645	645
	mean:	0.02541	0.01667	0.00709	0.02771	0.00810		mean:	0.00530	0.00584	0.00616	0.00602	0.00553
	D <= -2 C	2	2	5	4	6		D <= -10 %	21	21	31	21	34
	-2 C < D <= -1 C	13	11	29	16	32		-10 % < D <= -5 %	39	34	44	42	54
	-1 C < D <= -0.5 C	39	42	46	44	48		-5 % < D <= -2 %	46	61	61	62	72
	-0.5 C < D < 0.5 C	512	515	476	501	457		-2 % < D < 2 %	336	332	270	301	266
	0.5 C <= D < 1 C	34	31	38	28	54		2 % <= D < 5 %	98	96	119	111	113
	1 C <= D < 2 C	23	22	27	30	20		5 % <= D < 10 %	43	46	56	49	57
	2 C <= D	5	5	7	5	11		10 % <= D	35	35	41	39	47
H2m	2002061600+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061600+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	627	627	627	627	627		total nr.:	608	608	608	608	608
	mean:	0.00634	0.00532	0.00772	0.00739	0.00939		mean:	-0.01693	-0.01454	-0.01743	-0.01814	-0.01975
	D <= -10 %	15	14	27	20	29		D <= -2 C	1	1	3	1	3
	-10 % < D <= -5 %	35	30	38	27	46		-2 C < D <= -1 C	19	19	20	24	23
	-5 % < D <= -2 %	74	85	77	84	64		-1 C < D <= -0.5 C	35	33	50	39	57
	-2 % < D < 2 %	331	336	292	311	273		-0.5 C < D < 0.5 C	522	519	480	500	466
	2 % <= D < 5 %	88	87	95	89	109		0.5 C <= D < 1 C	25	30	40	33	41
	5 % <= D < 10 %	59	53	53	63	51		1 C <= D < 2 C	6	6	13	11	17
	10 % <= D	25	22	45	33	55		2 C <= D	0	0	2	0	1
T2m	2002061600+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061600+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	593	593	593	593	593		total nr.:	606	606	606	606	606
	mean:	0.03132	0.03350	0.03991	0.04250	0.04459		mean:	0.00386	0.00370	0.00544	0.00499	0.00632
	D <= -2 C	1	0	0	0	0		D <= -10 %	1	1	2	2	4
	-2 C < D <= -1 C	5	5	8	7	9		-10 % < D <= -5 %	16	15	23	18	25
	-1 C < D <= -0.5 C	16	11	27	17	28		-5 % < D <= -2 %	60	62	81	63	75
	-0.5 C < D < 0.5 C	533	544	511	528	506		-2 % < D < 2 %	416				

T2m	2002061700+000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061700+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	593	593	593	593	593		total nr.:	606	606	606	606	606
	mean:	-0.00019	-0.00011	-0.00009	-0.00008	0.00006		mean:	0.00247	0.00174	0.00353	0.00294	0.00396
	D <= -2 C	0	0	0	0	0		D <= -10 %	1	0	2	1	3
	-2 C < D <= -1 C	0	0	0	0	0		-10 % < D <= -5 %	14	15	18	13	19
	-1 C < D <= -0.5 C	0	0	0	0	0		-5 % < D <= -2 %	68	63	82	66	79
	-0.5 C < D < 0.5 C	593	593	593	593	593		-2 % < D < 2 %	421	436	384	413	382
	0.5 C <= D < 1 C	0	0	0	0	0		2 % <= D < 5 %	70	61	76	80	72
	1 C <= D < 2 C	0	0	0	0	0		5 % <= D < 10 %	27	29	36	29	39
	2 C <= D	0	0	0	0	0		10 % <= D	5	2	8	4	12
H2m	2002061700+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061700+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	591	591	591	591	591		total nr.:	661	661	661	661	661
	mean:	-0.00002	-0.00003	-0.00003	-0.00003	-0.00002		mean:	0.00429	0.00574	0.00245	0.00597	-0.00132
	D <= -10 %	0	0	0	0	0		D <= -2 C	0	0	0	0	0
	-10 % < D <= -5 %	0	0	0	0	0		-2 C < D <= -1 C	6	6	10	6	12
	-5 % < D <= -2 %	0	0	0	0	0		-1 C < D <= -0.5 C	24	25	38	32	49
	-2 % < D < 2 %	591	591	591	591	591		-0.5 C < D < 0.5 C	601	604	572	594	552
	2 % <= D < 5 %	0	0	0	0	0		0.5 C <= D < 1 C	26	23	33	24	38
	5 % <= D < 10 %	0	0	0	0	0		1 C <= D < 2 C	4	3	8	5	10
	10 % <= D	0	0	0	0	0		2 C <= D	0	0	0	0	0
T2m	2002061700+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061700+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	658	658	658	658	658		total nr.:	659	659	659	659	659
	mean:	-0.00110	0.00113	0.00261	-0.00276	0.00033		mean:	0.00550	0.00552	0.00789	0.00620	0.00858
	D <= -2 C	0	0	0	0	0		D <= -10 %	0	5	9	6	11
	-2 C < D <= -1 C	0	0	0	0	0		-10 % < D <= -5 %	21	16	23	27	30
	-1 C < D <= -0.5 C	5	4	6	4	11		-5 % < D <= -2 %	75	79	79	69	85
	-0.5 C < D < 0.5 C	650	651	644	650	637		-2 % < D < 2 %	412	421	369	399	342
	0.5 C <= D < 1 C	3	3	7	4	8		2 % <= D < 5 %	93	86	106	98	111
	1 C <= D < 2 C	0	0	1	0	2		5 % <= D < 10 %	39	37	46	41	45
	2 C <= D	0	0	0	0	0		10 % <= D	14	16	27	19	35
H2m	2002061700+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061700+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	657	657	657	657	657		total nr.:	654	654	654	654	654
	mean:	0.00318	0.00347	0.00467	0.00394	0.00530		mean:	0.11062	0.10585	0.14824	0.13602	0.15084
	D <= -10 %	2	2	3	2	3		D <= -2 C	7	6	11	8	13
	-10 % < D <= -5 %	5	3	6	6	4		-2 C < D <= -1 C	24	22	33	26	37
	-5 % < D <= -2 %	27	30	38	33	43		-1 C < D <= -0.5 C	50	50	55	52	55
	-2 % < D < 2 %	552	553	522	534	507		-0.5 C < D < 0.5 C	460	471	407	435	381
	2 % <= D < 5 %	47	46	52	54	56		0.5 C <= D < 1 C	51	46	73	63	87
	5 % <= D < 10 %	19	18	27	24	31		1 C <= D < 2 C	47	44	52	52	52
	10 % <= D	5	5	9	4	13		2 C <= D	15	15	23	18	29
T2m	2002061700+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061700+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	655	655	655	655	655		total nr.:	652	652	652	652	652
	mean:	0.13818	0.13651	0.18242	0.15808	0.19152		mean:	0.01184	0.01065	0.01516	0.01288	0.01699
	D <= -2 C	1	1	1	1	1		D <= -10 %	3	3	12	8	11
	-2 C < D <= -1 C	7	7	15	7	18		-10 % < D <= -5 %	27	34	48	34	52
	-1 C < D <= -0.5 C	35	36	40	43	43		-5 % < D <= -2 %	78	77	68	68	70
	-0.5 C < D < 0.5 C	504	507	476	489	462		-2 % < D < 2 %	295	314	253	285	242
	0.5 C <= D < 1 C	66	62	65	57	65		2 % <= D < 5 %	138	131	131	123	119
	1 C <= D < 2 C	31	31	39	37	47		5 % <= D < 10 %	88	74	101	96	115
	2 C <= D	11	11	19	17	19		10 % <= D	18	19	39	26	43
H2m	2002061700+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061700+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	655	655	655	655	655		total nr.:	631	631	631	631	631
	mean:	0.01101	0.01103	0.01539	0.01335	0.01627		mean:	-0.05726	-0.05950	-0.09406	-0.05530	-0.12550
	D <= -10 %	5	3	7	5	8		D <= -2 C	10	11	23	12	28
	-10 % < D <= -5 %	14	11	27	19	38		-2 C < D <= -1 C	41	38	49	42	54
	-5 % < D <= -2 %	68	65	56	60	55		-1 C < D <= -0.5 C	59	59	66	68	73
	-2 % < D < 2 %	372	382	318	355	298		-0.5 C < D < 0.5 C	437	440	392	411	371
	2 % <= D < 5 %	116	116	134	119	138		0.5 C <= D < 1 C	57	59	58	65	59
	5 % <= D < 10 %	67	67	79	73	84		1 C <= D < 2 C	21	18	32	26	36
	10 % <= D	13	11	34	24	34		2 C <= D	6	6	11	7	10
T2m	2002061700+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061700+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	648	648	648	648	648		total nr.:	624	624	624	624	624
	mean:	-0.01443	-0.02532	-0.03826	-0.01467	-0.04214		mean:	0.00362	0.00332	0.00593	0.00522	0.00668
	D <= -2 C	4	3	11	7	14		D <= -10 %	22	24	32	23	37
	-2 C < D <= -1 C	29	32	43	33	46		-10 % < D <= -5 %	39	37	44	45	51
	-1 C < D <= -0.5 C	48	50	41	48	48		-5 % < D <= -2 %	80	79	62	82	77
	-0.5 C < D < 0.5 C	503	511	477	485	454		-2 % < D < 2 %	288	294	242	262	231
	0.5 C <= D < 1 C	35	27	40	45	44		2 % <= D < 5 %	113	105	106	109	94
	1 C <= D < 2 C	24	22	26	25	34		5 % <= D < 10 %	63	69	83	73	92
	2 C <= D	5	3	10	5	8		10 % <= D	19	16	38	30	42
H2m	2002061700+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061700+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	645	645	645	645	645		total nr.:	602	602	602	602	602
	mean:	0.00343	0.00311	0.00329	0.00500	0.00463		mean:	-0.01384	-0.01802	-0.00657	-0.00719	-0.00639
	D <= -10 %	15	17	37	21	35		D <= -2 C	3	2	7	4	9
	-10 % < D <= -5 %	53	46	50	55	48		-2 C < D <= -1 C	16	17	24	21	26
	-5 % < D <= -2 %	69	69	59	69	84		-1 C < D <= -0.5 C	28	27	35	39	39
	-2 % < D < 2 %	319	331	287	317	270		-0.5 C < D < 0.5 C	513	519	463	485	452
	2 % <= D < 5 %	106	100	98	88	91		0.5 C <= D < 1 C	32	28	49	35	51
	5 % <= D < 10 %	58	59	69	76	74		1 C <= D < 2 C	7	7	20	15	21
	10 % <= D	25	23	35	29	43		2 C <= D	3	2	4	3	4
T2m	2002061700+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061700+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	608	608	608	608	608		total nr.:	594	594	594	594	594
	mean:	-0.00405	-0.01116	-0.00490	-0.00502	0.00068		mean:	0.00592	0.00489	0.00791	0.00687	0.00872
	D <= -2 C	0	0	0	0	1		D <= -10 %	1	3	4	5	5
	-2 C < D <= -1 C	9	8	20	15	20		-10 % < D <= -5 %	21	19	34	20	34
	-1 C < D <= -0.5 C	36	33	33	36	37		-5 % < D <= -2 %	63	61	73	76	80
	-0.5 C < D < 0.5 C	538	546	517	529	501							

T2m	2002061800+0000	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61	H2m	2002061800+0024	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61
	total nr.:	608	608	608	608	608		total nr.:	594	594	594	594	594
	mean:	-0.00017	-0.00013	-0.00020	-0.00013	-0.00011		mean:	0.00386	0.00452	0.00638	0.00509	0.00766
	D <= -2 C	0	0	0	0	0		D <= -10 %	4	4	7	7	12
	-2 C < D <= -1 C	0	0	0	0	0		-10 % < D <= -5 %	12	9	20	13	18
	-1 C < D <= -0.5 C	0	0	0	0	0		-5 % < D <= -2 %	44	50	65	54	55
	-0.5 C < D <= 0.5 C	608	608	608	608	608		-2 % < D <= 2 %	419	407	358	385	355
	0.5 C <= D < 1 C	0	0	0	0	0		2 % <= D < 5 %	79	88	86	83	82
	1 C <= D < 2 C	0	0	0	0	0		5 % <= D < 10 %	35	34	42	46	55
	2 C <= D	0	0	0	0	0		10 % <= D	1	2	16	6	17
H2m	2002061800+0000	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61	T2m	2002061800+0030	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61
	total nr.:	606	606	606	606	606		total nr.:	656	656	656	656	656
	mean:	0.00000	-0.00002	-0.00001	-0.00001	-0.00001		mean:	0.01189	-0.00066	-0.00223	-0.01122	-0.01036
	D <= -10 %	0	0	0	0	0		D <= -2 C	0	0	0	0	0
	-10 % < D <= -5 %	0	0	0	0	0		-2 C < D <= -1 C	5	5	6	6	16
	-5 % < D <= -2 %	0	0	0	0	0		-1 C < D <= -0.5 C	25	25	52	36	54
	-2 % < D <= 2 %	606	606	606	606	606		-0.5 C < D <= 0.5 C	586	595	540	574	529
	2 % <= D < 5 %	0	0	0	0	0		0.5 C <= D < 1 C	33	26	53	38	43
	5 % <= D < 10 %	0	0	0	0	0		1 C <= D < 2 C	7	5	5	2	14
	10 % <= D	0	0	0	0	0		2 C <= D	0	0	0	0	0
T2m	2002061800+0006	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61	H2m	2002061800+0030	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61
	total nr.:	661	661	661	661	661		total nr.:	655	655	655	655	655
	mean:	-0.00364	-0.00113	-0.00141	-0.00346	-0.00043		mean:	0.00693	0.00676	0.00951	0.00804	0.01069
	D <= -2 C	0	0	0	0	0		D <= -10 %	3	3	4	2	5
	-2 C < D <= -1 C	0	1	0	2	0		-10 % < D <= -5 %	23	20	42	24	38
	-1 C < D <= -0.5 C	7	6	11	6	14		-5 % < D <= -2 %	68	76	73	83	81
	-0.5 C < D <= 0.5 C	652	652	642	650	637		-2 % < D <= 2 %	396	386	355	368	330
	0.5 C <= D < 1 C	2	2	8	3	9		2 % <= D < 5 %	106	115	93	103	109
	1 C <= D < 2 C	0	0	0	0	1		5 % <= D < 10 %	45	40	57	51	55
	2 C <= D	0	0	0	0	0		10 % <= D	14	15	33	22	37
H2m	2002061800+0006	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61	T2m	2002061800+0036	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61
	total nr.:	659	659	659	659	659		total nr.:	650	650	650	650	650
	mean:	0.00415	0.00461	0.00682	0.00574	0.00800		mean:	0.08803	0.07660	0.10857	0.09092	0.11232
	D <= -10 %	2	3	3	3	3		D <= -2 C	6	6	8	9	13
	-10 % < D <= -5 %	6	4	9	9	11		-2 C < D <= -1 C	33	30	42	32	49
	-5 % < D <= -2 %	50	46	55	48	55		-1 C < D <= -0.5 C	44	43	52	48	51
	-2 % < D <= 2 %	498	504	449	476	434		-0.5 C < D <= 0.5 C	442	456	400	426	378
	2 % <= D < 5 %	75	75	96	86	98		0.5 C <= D < 1 C	77	69	76	76	78
	5 % <= D < 10 %	25	24	39	33	47		1 C <= D < 2 C	35	35	46	43	56
	10 % <= D	3	3	8	4	11		2 C <= D	13	11	26	16	25
T2m	2002061800+0012	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61	H2m	2002061800+0036	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61
	total nr.:	654	654	654	654	654		total nr.:	646	646	646	646	646
	mean:	0.16785	0.16067	0.23246	0.19868	0.24322		mean:	0.00502	0.00499	0.00746	0.00665	0.00841
	D <= -2 C	0	0	1	1	5		D <= -10 %	18	20	27	32	38
	-2 C < D <= -1 C	21	20	30	25	35		-10 % < D <= -5 %	40	37	51	40	54
	-1 C < D <= -0.5 C	44	47	56	49	70		-5 % < D <= -2 %	55	69	70	84	81
	-0.5 C < D <= 0.5 C	444	443	389	405	377		-2 % < D <= 2 %	317	333	256	287	237
	0.5 C <= D < 1 C	82	84	83	88	88		2 % <= D < 5 %	126	117	115	112	97
	1 C <= D < 2 C	52	49	70	63	68		5 % <= D < 10 %	57	55	73	79	82
	2 C <= D	11	11	26	16	32		10 % <= D	18	17	40	25	53
H2m	2002061800+0012	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61	T2m	2002061800+0042	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61
	total nr.:	652	652	652	652	652		total nr.:	643	643	643	643	643
	mean:	0.01038	0.00976	0.01361	0.01193	0.01475		mean:	-0.00615	-0.00953	-0.04331	-0.01749	-0.05529
	D <= -10 %	8	11	11	10	16		D <= -2 C	8	8	15	10	21
	-10 % < D <= -5 %	26	27	33	45	48		-2 C < D <= -1 C	23	18	41	33	49
	-5 % < D <= -2 %	66	65	74	82	72		-1 C < D <= -0.5 C	53	55	68	56	57
	-2 % < D <= 2 %	342	345	273	300	252		-0.5 C < D <= 0.5 C	473	476	407	448	394
	2 % <= D < 5 %	116	111	117	110	124		0.5 C <= D < 1 C	60	60	63	59	59
	5 % <= D < 10 %	73	72	87	85	90		1 C <= D < 2 C	21	21	43	33	54
	10 % <= D	21	21	45	32	50		2 C <= D	5	5	6	4	9
T2m	2002061800+0018	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61	H2m	2002061800+0042	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61
	total nr.:	631	631	631	631	631		total nr.:	635	635	635	635	635
	mean:	0.01778	0.02391	-0.03045	0.00888	-0.04789		mean:	0.00148	0.00205	0.00291	0.00190	0.00134
	D <= -2 C	7	8	21	13	25		D <= -10 %	24	25	40	31	49
	-2 C < D <= -1 C	31	29	41	37	45		-10 % < D <= -5 %	54	45	55	53	54
	-1 C < D <= -0.5 C	53	49	57	45	57		-5 % < D <= -2 %	81	78	80	81	87
	-0.5 C < D <= 0.5 C	447	445	400	423	389		-2 % < D <= 2 %	285	305	237	254	219
	0.5 C <= D < 1 C	58	70	64	67	60		2 % <= D < 5 %	111	98	93	115	92
	1 C <= D < 2 C	28	24	37	35	44		5 % <= D < 10 %	57	63	92	77	96
	2 C <= D	7	6	11	11	11		10 % <= D	23	21	38	24	38
H2m	2002061800+0018	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61	T2m	2002061800+0048	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61
	total nr.:	624	624	624	624	624		total nr.:	599	599	599	599	599
	mean:	0.00847	0.00872	0.00959	0.00895	0.00863		mean:	0.02962	0.03418	0.05952	0.04831	0.06967
	D <= -10 %	22	22	33	25	41		D <= -2 C	1	1	3	1	3
	-10 % < D <= -5 %	33	33	54	38	59		-2 C < D <= -1 C	14	13	18	21	24
	-5 % < D <= -2 %	67	66	67	80	73		-1 C < D <= -0.5 C	25	22	24	39	40
	-2 % < D <= 2 %	291	298	247	266	222		-0.5 C < D <= 0.5 C	508	509	448	479	427
	2 % <= D < 5 %	111	100	94	93	95		0.5 C <= D < 1 C	39	45	67	56	69
	5 % <= D < 10 %	65	74	72	80	70		1 C <= D < 2 C	12	9	19	18	32
	10 % <= D	35	31	57	42	64		2 C <= D	0	0	5	0	4
T2m	2002061800+0024	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61	H2m	2002061800+0048	OP- 10SM61	OP- 21SM41	OP- 21SM61	OP- 30SM41	OP- 30SM61
	total nr.:	602	602	602	602	602		total nr.:	597	597	597	597	597
	mean:	0.01236	0.01109	0.01990	0.01914	0.01906		mean:	0.00415	0.00392	0.00623	0.00340	0.00652
	D <= -2 C	0	0	1	0	1		D <= -10 %	4	4	6	7	8
	-2 C < D <= -1 C	13	11	16	18	23		-10 % < D <= -5 %	18	15	26	22	27
	-1 C < D <= -0.5 C	26	24	42	31	46		-5 % < D <= -2 %	55	69	68	70	82
	-0.5 C < D <= 0.5 C	521	531	482	502	458		-2 % < D <= 2 %	395	380	342	362	331

T2m	2002061900+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061900+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	602	602	602	602	602		total nr.:	597	597	597	597	597
	mean:	-0.00005	0.00008	-0.00005	0.00003	-0.00017		mean:	0.00540	0.00555	0.00939	0.00724	0.00962
	D <= -2 C	0	0	0	0	0		D <= -10 %	2	2	4	3	7
	-2 C < D <= -1 C	0	0	0	0	0		-10 % < D <= -5 %	12	9	16	11	18
	-1 C < D <= -0.5 C	0	0	0	0	0		-5 % < D <= -2 %	69	55	71	69	65
	-0.5 C < D <= 0 C	602	602	602	602	602		-2 % < D <= 2 %	364	388	321	347	319
	0 C <= D < 1 C	0	0	0	0	0		2 % <= D < 5 %	122	114	118	121	113
	1 C <= D < 2 C	0	0	0	0	0		5 % <= D < 10 %	24	27	57	40	59
	2 C <= D	0	0	0	0	0		10 % <= D	4	2	10	6	16
H2m	2002061900+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061900+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	594	594	594	594	594		total nr.:	659	659	659	659	659
	mean:	0.00000	0.00000	-0.00001	-0.00002	-0.00002		mean:	0.04925	0.05091	0.07793	0.06200	0.08583
	D <= -10 %	0	0	0	0	0		D <= -2 C	0	0	0	0	0
	-10 % < D <= -5 %	0	0	0	0	0		-2 C < D <= -1 C	5	4	8	7	14
	-5 % < D <= -2 %	0	0	0	0	0		-1 C < D <= -0.5 C	22	15	31	26	30
	-2 % < D <= 2 %	594	594	594	594	594		-0.5 C < D <= 0 C	580	595	531	551	520
	2 % <= D < 5 %	0	0	0	0	0		0 C <= D < 1 C	46	38	65	60	61
	5 % <= D < 10 %	0	0	0	0	0		1 C <= D < 2 C	5	6	22	14	33
	10 % <= D	0	0	0	0	0		2 C <= D	1	1	2	1	1
T2m	2002061900+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061900+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	656	656	656	656	656		total nr.:	657	657	657	657	657
	mean:	0.00758	0.00378	0.01772	0.00807	0.01625		mean:	0.01078	0.01035	0.01588	0.01228	0.01675
	D <= -2 C	0	0	0	0	0		D <= -10 %	0	0	2	4	10
	-2 C < D <= -1 C	1	1	1	1	1		-10 % < D <= -5 %	27	13	28	29	33
	-1 C < D <= -0.5 C	4	3	6	3	10		-5 % < D <= -2 %	68	74	75	65	80
	-0.5 C < D <= 0 C	649	650	635	646	629		-2 % < D <= 2 %	366	382	320	351	297
	0 C <= D < 1 C	2	2	13	6	15		2 % <= D < 5 %	115	114	111	112	106
	1 C <= D < 2 C	0	0	1	0	1		5 % <= D < 10 %	52	42	73	61	82
	2 C <= D	0	0	0	0	0		10 % <= D	27	28	44	33	49
H2m	2002061900+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061900+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	655	655	655	655	655		total nr.:	654	654	654	654	654
	mean:	0.00358	0.00376	0.00697	0.00510	0.00783		mean:	0.19090	0.18676	0.27276	0.23541	0.28864
	D <= -10 %	1	1	1	1	2		D <= -2 C	1	1	6	2	7
	-10 % < D <= -5 %	6	7	10	9	8		-2 C < D <= -1 C	28	28	34	31	40
	-5 % < D <= -2 %	54	48	53	47	57		-1 C < D <= -0.5 C	51	52	52	54	55
	-2 % < D <= 2 %	498	499	448	478	438		-0.5 C < D <= 0 C	421	411	363	392	344
	2 % <= D < 5 %	81	81	92	90	94		0 C <= D < 1 C	72	86	97	82	91
	5 % <= D < 10 %	10	16	46	26	49		1 C <= D < 2 C	61	55	53	58	66
	10 % <= D	5	3	5	4	7		2 C <= D	20	21	49	35	51
T2m	2002061900+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061900+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	650	650	650	650	650		total nr.:	651	651	651	651	651
	mean:	0.13723	0.12684	0.20385	0.16065	0.22836		mean:	0.00931	0.00884	0.01246	0.01114	0.01386
	D <= -2 C	4	3	4	4	4		D <= -10 %	9	7	18	10	23
	-2 C < D <= -1 C	13	14	29	19	32		-10 % < D <= -5 %	36	34	46	45	45
	-1 C < D <= -0.5 C	47	48	61	60	59		-5 % < D <= -2 %	61	52	65	59	64
	-0.5 C < D <= 0 C	466	468	392	429	377		-2 % < D <= 2 %	343	339	291	315	281
	0 C <= D < 1 C	64	64	78	76	73		2 % <= D < 5 %	117	118	109	114	93
	1 C <= D < 2 C	43	40	62	52	79		5 % <= D < 10 %	66	69	86	74	89
	2 C <= D	13	13	24	16	25		10 % <= D	21	19	46	34	56
H2m	2002061900+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061900+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	646	646	646	646	646		total nr.:	636	636	636	636	636
	mean:	0.01037	0.00926	0.01380	0.01110	0.01630		mean:	0.08038	0.07695	0.08011	0.07809	0.03933
	D <= -10 %	9	9	14	12	15		D <= -2 C	5	5	14	7	20
	-10 % < D <= -5 %	23	22	33	28	40		-2 C < D <= -1 C	31	32	41	36	49
	-5 % < D <= -2 %	67	72	84	76	79		-1 C < D <= -0.5 C	47	43	61	49	55
	-2 % < D <= 2 %	346	342	276	315	252		-0.5 C < D <= 0 C	443	458	386	423	373
	2 % <= D < 5 %	109	115	107	106	108		0 C <= D < 1 C	67	51	68	65	67
	5 % <= D < 10 %	71	66	89	78	103		1 C <= D < 2 C	29	29	43	40	47
	10 % <= D	21	20	43	31	49		2 C <= D	14	18	23	16	25
T2m	2002061900+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061900+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	643	643	643	643	643		total nr.:	635	635	635	635	635
	mean:	0.05528	0.06416	0.05299	0.06746	0.04861		mean:	0.00584	0.00672	0.00765	0.00751	0.00874
	D <= -2 C	10	8	14	9	21		D <= -10 %	26	22	40	29	44
	-2 C < D <= -1 C	19	17	28	21	27		-10 % < D <= -5 %	33	28	32	32	34
	-1 C < D <= -0.5 C	42	46	43	48	46		-5 % < D <= -2 %	81	76	85	80	77
	-0.5 C < D <= 0 C	464	483	420	450	405		-2 % < D <= 2 %	299	325	262	287	257
	0 C <= D < 1 C	78	64	86	77	79		2 % <= D < 5 %	116	95	97	92	92
	1 C <= D < 2 C	27	32	44	38	53		5 % <= D < 10 %	52	59	80	77	81
	2 C <= D	3	3	5	5	10		10 % <= D	28	30	39	38	50
H2m	2002061900+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	T2m	2002061900+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	635	635	635	635	635		total nr.:	599	599	599	599	599
	mean:	0.00638	0.00651	0.00978	0.00881	0.01157		mean:	0.01990	0.01507	0.04065	0.02265	0.05470
	D <= -10 %	19	19	27	23	32		D <= -2 C	0	0	2	0	2
	-10 % < D <= -5 %	33	34	54	38	50		-2 C < D <= -1 C	11	12	19	16	26
	-5 % < D <= -2 %	67	73	60	71	66		-1 C < D <= -0.5 C	35	31	43	33	46
	-2 % < D <= 2 %	317	313	255	287	246		-0.5 C < D <= 0 C	501	508	455	484	433
	2 % <= D < 5 %	103	101	103	107	88		0 C <= D < 1 C	39	38	50	50	51
	5 % <= D < 10 %	76	76	92	75	86		1 C <= D < 2 C	12	9	25	14	33
	10 % <= D	20	19	44	34	67		2 C <= D	1	1	5	2	8
T2m	2002061900+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61	H2m	2002061900+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	599	599	599	599	599		total nr.:	596	596	596	596	596
	mean:	-0.00015	0.00154	0.01872	0.00356	0.02032		mean:	0.00557	0.00500	0.00744	0.00548	0.00978
	D <= -2 C	0	0	1	0	3		D <= -10 %	2	3	6	3	8
	-2 C < D <= -1 C	15	11	18	14	16		-10 % < D <= -5 %	11	16	27	21	25
	-1 C < D <= -0.5 C	24	28	38	31	46		-5 % < D <= -2 %	51	39	59	48	64
	-0.5 C < D <= 0 C	526	529	484	514	464							

T2m	2002062000+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	599	599	599	599	599
	mean:	-0.00013	-0.00006	-0.00011	0.00004	-0.00014
	D <= -2 C	0	0	0	0	0
	-2 C < D <= -1 C	0	0	0	0	0
	-1 C < D <= -0.5 C	0	0	0	0	0
	-0.5 C < D <= -0.2 C	599	599	599	599	599
	-0.2 C < D <= 0 C	0	0	0	0	0
	0 C < D <= 0.2 C	0	0	0	0	0
	0.2 C <= D	0	0	0	0	0
H2m	2002062000+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	597	597	597	597	597
	mean:	-0.00002	-0.00001	0.00001	-0.00001	0.00000
	D <= -10 %	0	0	0	0	0
	-10 % < D <= -5 %	0	0	0	0	0
	-5 % < D <= -2 %	0	0	0	0	0
	-2 % < D <= 2 %	597	597	597	597	597
	2 % <= D < 5 %	0	0	0	0	0
	5 % <= D < 10 %	0	0	0	0	0
	10 % <= D	0	0	0	0	0
T2m	2002062000+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	659	659	659	659	659
	mean:	0.01962	0.00996	0.02007	0.01062	0.02581
	D <= -2 C	0	0	0	0	0
	-2 C < D <= -1 C	0	0	1	0	1
	-1 C < D <= -0.5 C	7	8	8	8	11
	-0.5 C < D <= 0 C	644	642	633	640	628
	0 C < D <= 0.2 C	8	9	16	10	17
	0.2 C <= D	0	0	1	1	2
	2 C <= D	0	0	0	0	0
H2m	2002062000+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	657	657	657	657	657
	mean:	0.00462	0.00422	0.00690	0.00521	0.00886
	D <= -10 %	1	1	1	1	3
	-10 % < D <= -5 %	7	8	9	8	7
	-5 % < D <= -2 %	40	40	49	43	46
	-2 % < D <= 2 %	505	513	466	496	450
	2 % <= D < 5 %	77	71	89	79	97
	5 % <= D < 10 %	24	21	33	25	36
	10 % <= D	3	3	10	5	18
T2m	2002062000+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	654	654	654	654	654
	mean:	0.08500	0.09087	0.15572	0.09473	0.16492
	D <= -2 C	0	0	0	0	2
	-2 C < D <= -1 C	18	17	32	28	37
	-1 C < D <= -0.5 C	43	37	44	43	50
	-0.5 C < D <= 0 C	498	508	450	478	430
	0 C < D <= 0.2 C	57	55	54	56	63
	0.2 C <= D	32	30	58	37	57
	2 C <= D	6	7	18	11	22
H2m	2002062000+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	651	651	651	651	651
	mean:	0.00686	0.00689	0.01034	0.00792	0.01010
	D <= -10 %	4	3	10	4	11
	-10 % < D <= -5 %	20	19	27	23	35
	-5 % < D <= -2 %	52	54	50	54	65
	-2 % < D <= 2 %	416	426	369	406	345
	2 % <= D < 5 %	107	89	109	91	96
	5 % <= D < 10 %	42	51	56	54	64
	10 % <= D	10	9	29	15	35
T2m	2002062000+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	636	636	636	636	636
	mean:	0.05151	0.05143	0.08997	0.07955	0.08658
	D <= -2 C	6	5	11	7	11
	-2 C < D <= -1 C	16	13	20	18	27
	-1 C < D <= -0.5 C	28	28	35	31	35
	-0.5 C < D <= 0 C	514	520	461	482	452
	0 C < D <= 0.2 C	45	43	58	59	55
	0.2 C <= D	14	17	36	29	37
	2 C <= D	13	10	15	10	19
H2m	2002062000+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	635	635	635	635	635
	mean:	0.00417	0.00398	0.00828	0.00548	0.00799
	D <= -10 %	12	10	18	13	22
	-10 % < D <= -5 %	31	30	26	25	36
	-5 % < D <= -2 %	54	58	63	71	57
	-2 % < D <= 2 %	394	397	348	360	336
	2 % <= D < 5 %	87	86	87	93	75
	5 % <= D < 10 %	39	37	62	56	68
	10 % <= D	18	17	31	17	41
T2m	2002062000+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	599	599	599	599	599
	mean:	0.02422	0.02917	0.06103	0.02894	0.06370
	D <= -2 C	0	0	0	0	0
	-2 C < D <= -1 C	7	3	11	9	14
	-1 C < D <= -0.5 C	17	21	24	24	25
	-0.5 C < D <= 0 C	544	543	502	532	492
	0 C < D <= 0.2 C	21	21	42	33	38
	0.2 C <= D	9	10	16	9	27
	2 C <= D	1	1	4	2	3

H2m	2002062000+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	596	596	596	596	596
	mean:	0.00262	0.00238	0.00460	0.00249	0.00655
	D <= -10 %	3	3	7	2	8
	-10 % < D <= -5 %	16	12	20	20	25
	-5 % < D <= -2 %	37	43	50	43	44
	-2 % < D <= 2 %	457	454	404	443	381
	2 % <= D < 5 %	60	61	72	59	80
	5 % <= D < 10 %	18	18	29	22	38
	10 % <= D	5	5	14	7	20
T2m	2002062000+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	655	655	655	655	655
	mean:	0.02763	0.01921	0.04097	0.02714	0.04842
	D <= -2 C	1	1	2	2	2
	-2 C < D <= -1 C	7	5	8	4	12
	-1 C < D <= -0.5 C	22	26	28	27	26
	-0.5 C < D <= 0 C	581	585	562	569	541
	0 C < D <= 0.2 C	34	29	36	42	56
	0.2 C <= D	9	8	18	10	16
	2 C <= D	1	1	1	1	2
H2m	2002062000+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	655	655	655	655	655
	mean:	0.00707	0.00687	0.00961	0.00854	0.01078
	D <= -10 %	0	0	3	4	4
	-10 % < D <= -5 %	19	18	31	22	32
	-5 % < D <= -2 %	55	65	54	58	68
	-2 % < D <= 2 %	423	423	385	421	368
	2 % <= D < 5 %	99	86	104	88	93
	5 % <= D < 10 %	43	47	54	44	57
	10 % <= D	13	12	24	20	33
T2m	2002062000+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	653	653	653	653	653
	mean:	0.03194	0.02423	0.03985	0.03605	0.05869
	D <= -2 C	8	6	14	6	16
	-2 C < D <= -1 C	22	24	43	43	49
	-1 C < D <= -0.5 C	49	51	49	44	46
	-0.5 C < D <= 0 C	469	487	410	441	382
	0 C < D <= 0.2 C	71	53	71	73	85
	0.2 C <= D	30	28	55	41	58
	2 C <= D	4	4	11	5	17
H2m	2002062000+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	653	653	653	653	653
	mean:	0.00542	0.00459	0.00936	0.00706	0.01101
	D <= -10 %	15	15	29	19	28
	-10 % < D <= -5 %	27	33	40	31	44
	-5 % < D <= -2 %	67	72	70	74	63
	-2 % < D <= 2 %	356	364	292	323	273
	2 % <= D < 5 %	114	118	105	110	108
	5 % <= D < 10 %	55	56	89	76	97
	10 % <= D	14	10	33	20	40
T2m	2002062000+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	651	651	651	651	651
	mean:	0.01630	0.00772	-0.00728	0.00368	-0.02018
	D <= -2 C	2	2	9	4	17
	-2 C < D <= -1 C	28	23	39	32	39
	-1 C < D <= -0.5 C	45	45	57	48	59
	-0.5 C < D <= 0 C	503	508	447	488	427
	0 C < D <= 0.2 C	45	46	55	46	67
	0.2 C <= D	22	21	35	24	27
	2 C <= D	6	6	9	9	15
H2m	2002062000+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	647	647	647	647	647
	mean:	0.00360	0.00309	0.00568	0.00424	0.00482
	D <= -10 %	26	23	43	31	50
	-10 % < D <= -5 %	44	46	48	44	56
	-5 % < D <= -2 %	74	79	82	77	73
	-2 % < D <= 2 %	327	323	266	313	251
	2 % <= D < 5 %	95	95	90	95	100
	5 % <= D < 10 %	43	47	59	38	55
	10 % <= D	38	34	57	49	62
T2m	2002062000+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
	total nr.:	600	600	600	600	600
	mean:	0.03376	0.01934	0.02000	0.01553	0.02047
	D <= -2 C	0	0	2	1	2
	-2 C < D <= -1 C	8	10	15	11	24

T2m 2003011600+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	614	614	614	614	614
mean:	0.00016	0.00012	-0.00009	-0.00014	-0.00007
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	614	614	614	614	614
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003011600+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	620	620	620	620	620
mean:	-0.00001	0.00000	-0.00001	-0.00001	-0.00001
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	0	0	0	0	0
-2 % < D < 2 %	620	620	620	620	620
2 % <= D < 5 %	0	0	0	0	0
5 % <= D < 10 %	0	0	0	0	0
10 % <= D	0	0	0	0	0
T2m 2003011600+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	639	639	639	639	639
mean:	0.00056	0.00002	-0.00100	0.00049	-0.00039
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	639	639	639	639	639
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003011600+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	644	644	644	644	644
mean:	0.00003	0.00009	0.00004	0.00004	0.00009
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	0	0	0	0	0
-2 % < D < 2 %	643	641	642	644	642
2 % <= D < 5 %	0	3	2	0	2
5 % <= D < 10 %	1	0	0	0	0
10 % <= D	0	0	0	0	0
T2m 2003011600+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	666	666	666	666	666
mean:	0.00050	-0.00116	-0.00039	-0.00046	-0.00017
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	666	666	666	666	666
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003011600+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	668	668	668	668	668
mean:	0.00005	-0.00002	0.00030	-0.00005	0.00005
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	2	3	2	3	2
-2 % < D < 2 %	663	661	657	661	660
2 % <= D < 5 %	2	3	7	2	5
5 % <= D < 10 %	1	1	2	2	1
10 % <= D	0	0	0	0	0
T2m 2003011600+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	665	665	665	665	665
mean:	0.00115	0.00104	0.00006	-0.00006	-0.00122
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	1	1	2	1	2
-0.5 C < D < 0.5 C	663	663	663	664	661
0.5 C <= D < 1 C	1	1	0	0	2
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003011600+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	665	665	665	665	665
mean:	0.00023	0.00012	0.00029	0.00031	0.00031
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	1	0	0	0	2
-2 % < D < 2 %	659	662	661	661	656
2 % <= D < 5 %	5	3	4	4	7
5 % <= D < 10 %	0	0	0	0	0
10 % <= D	0	0	0	0	0
T2m 2003011600+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	607	607	607	607	607
mean:	0.00076	0.00198	0.00001	-0.00026	0.00015
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	1	0	1
-0.5 C < D < 0.5 C	606	607	606	607	605
0.5 C <= D < 1 C	1	0	0	0	1
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0

H2m 2003011600+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	602	602	602	602	602
mean:	-0.00006	0.00006	-0.00007	0.00000	0.00006
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	0	0	1	1	1
-2 % < D < 2 %	602	601	601	599	600
2 % <= D < 5 %	0	1	0	2	0
5 % <= D < 10 %	0	0	0	0	1
10 % <= D	0	0	0	0	0
T2m 2003011600+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	662	662	662	662	662
mean:	0.00008	0.00188	0.00129	0.00031	0.00013
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	1	0	0	1	0
-0.5 C < D < 0.5 C	661	660	662	661	661
0.5 C <= D < 1 C	0	2	0	0	1
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003011600+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	665	665	665	665	665
mean:	0.00007	-0.00002	-0.00008	0.00004	-0.00005
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	3	2	4	4	2
-2 % < D < 2 %	661	663	661	660	662
2 % <= D < 5 %	1	0	0	1	1
5 % <= D < 10 %	0	0	0	0	0
10 % <= D	0	0	0	0	0
T2m 2003011600+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	661	661	661	661	661
mean:	0.00109	-0.00159	-0.00086	0.00042	0.00036
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	661	661	661	661	661
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003011600+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	661	661	661	661	661
mean:	0.00023	0.00012	0.00018	0.00014	0.00003
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	2	2	2	1	4
-2 % < D < 2 %	654	657	656	657	652
2 % <= D < 5 %	5	2	2	2	4
5 % <= D < 10 %	0	0	1	1	1
10 % <= D	0	0	0	0	0
T2m 2003011600+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	651	651	651	651	651
mean:	-0.00099	-0.00143	-0.00180	-0.00534	-0.00122
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	1
-1 C < D <= -0.5 C	0	0	0	1	0
-0.5 C < D < 0.5 C	651	651	650	650	651
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003011600+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	654	654	654	654	654
mean:	0.00020	-0.00003	0.00003	0.00012	0.00013
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	0	0	1	0	0
-2 % < D < 2 %	651	652	652	652	652
2 % <= D < 5 %	3	1	1	2	2
5 % <= D < 10 %	0	0	0	0	0
10 % <= D	0	0	0	0	0
T2m 2003011600+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	620	620	620	620	620
mean:	0.00658	0.00148	-0.00023	0.00017	0.00478
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	619	620	620	620	619
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	1	0	0	0	1
H2m 2003011600+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	623	623	623	623	623
mean:	0.00007	-0.00001	-0.00019	-0.00011	-0.00016
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	0	0	0	3	4
-2 % < D < 2 %	622	619	617	618	618
2 % <= D < 5 %	1	2	1	2	1
5 % <= D < 10 %	0	0	0	0	0
10 % <= D	0	0	0	0	0

T2m 2003040200+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	625	625	625	625	625
mean:	0.00007	0.00010	0.00006	0.00000	0.00008
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	625	625	625	625	625
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040200+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	628	628	628	628	628
mean:	-0.00001	0.00000	0.00001	0.00000	0.00001
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	0	0	0	0	0
-2 % < D < 2 %	628	628	628	628	628
2 % <= D < 5 %	0	0	0	0	0
5 % <= D < 10 %	0	0	0	0	0
10 % <= D	0	0	0	0	0
T2m 2003040200+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	660	660	660	660	660
mean:	-0.00055	-0.00176	0.00012	0.00077	-0.00128
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	659	660	659	660	660
0.5 C <= D < 1 C	1	0	1	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040200+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	660	660	660	660	660
mean:	-0.00016	-0.00024	-0.00012	-0.00041	-0.00044
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	1	1	1	1	1
-5 % < D <= -2 %	5	2	3	5	5
-2 % < D < 2 %	652	656	650	652	650
2 % <= D < 5 %	2	1	5	2	4
5 % <= D < 10 %	0	0	1	0	0
10 % <= D	0	0	0	0	0
T2m 2003040200+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	694	694	694	694	694
mean:	-0.00748	-0.00163	0.00036	-0.00254	0.00011
D <= -2 C	0	0	0	0	1
-2 C < D <= -1 C	0	0	1	0	1
-1 C < D <= -0.5 C	4	2	2	2	3
-0.5 C < D < 0.5 C	689	692	689	690	685
0.5 C <= D < 1 C	1	0	1	1	4
1 C <= D < 2 C	0	0	1	1	1
2 C <= D	0	0	0	0	0
H2m 2003040200+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	694	694	694	694	694
mean:	0.00043	-0.00017	0.00049	-0.00013	0.00036
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	2	2	4	1	6
-5 % < D <= -2 %	17	22	24	26	25
-2 % < D < 2 %	647	643	635	641	626
2 % <= D < 5 %	27	27	28	25	32
5 % <= D < 10 %	1	0	3	1	5
10 % <= D	0	0	0	0	0
T2m 2003040200+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	668	668	668	668	668
mean:	0.00183	0.00013	0.00253	-0.00314	-0.00268
D <= -2 C	0	0	0	0	1
-2 C < D <= -1 C	0	0	1	0	1
-1 C < D <= -0.5 C	1	1	1	1	2
-0.5 C < D < 0.5 C	667	667	665	667	664
0.5 C <= D < 1 C	0	0	1	0	1
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040200+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	666	666	666	666	666
mean:	0.00002	-0.00015	-0.00003	-0.00021	-0.00054
D <= -10 %	0	0	1	0	1
-10 % < D <= -5 %	0	0	2	1	3
-5 % < D <= -2 %	11	25	17	17	17
-2 % < D < 2 %	640	619	628	629	627
2 % <= D < 5 %	14	21	18	17	15
5 % <= D < 10 %	1	1	0	2	3
10 % <= D	0	0	0	0	0
T2m 2003040200+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	613	613	613	613	613
mean:	-0.00267	-0.00711	-0.00013	-0.00438	-0.00203
D <= -2 C	0	0	0	0	1
-2 C < D <= -1 C	0	0	0	0	1
-1 C < D <= -0.5 C	2	3	1	2	1
-0.5 C < D < 0.5 C	611	610	612	611	610
0.5 C <= D < 1 C	0	0	0	0	1
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0

H2m 2003040200+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	611	611	611	611	611
mean:	-0.00003	-0.00004	0.00002	-0.00014	-0.00023
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	1	0	0
-5 % < D <= -2 %	5	3	5	9	6
-2 % < D < 2 %	598	601	600	599	601
2 % <= D < 5 %	8	7	4	3	3
5 % <= D < 10 %	0	0	1	0	1
10 % <= D	0	0	0	0	0
T2m 2003040200+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	668	668	668	668	668
mean:	-0.00031	0.00051	-0.00146	0.00127	-0.00504
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	1	0	0	1	2
-0.5 C < D < 0.5 C	667	668	668	667	666
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040200+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	666	666	666	666	666
mean:	-0.00015	-0.00017	0.00013	-0.00002	-0.00012
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	1	0	0	1
-5 % < D <= -2 %	9	11	6	11	11
-2 % < D < 2 %	648	646	649	645	646
2 % <= D < 5 %	9	8	11	8	6
5 % <= D < 10 %	0	0	0	2	2
10 % <= D	0	0	0	0	0
T2m 2003040200+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	670	670	670	670	670
mean:	-0.00030	-0.00025	0.00349	-0.00544	0.00533
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	6	6	9	5	7
-0.5 C < D < 0.5 C	662	658	654	661	652
0.5 C <= D < 1 C	1	6	3	3	10
1 C <= D < 2 C	1	0	1	1	1
2 C <= D	0	0	0	0	0
H2m 2003040200+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	668	668	668	668	668
mean:	-0.00141	-0.00001	0.00022	-0.00025	0.00085
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	7	7	11	8	11
-5 % < D <= -2 %	63	46	48	47	45
-2 % < D < 2 %	564	570	548	562	553
2 % <= D < 5 %	37	43	53	44	48
5 % <= D < 10 %	0	1	7	6	10
10 % <= D	1	1	1	1	1
T2m 2003040200+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	669	669	669	669	669
mean:	0.00383	0.00139	0.00511	0.00299	0.00049
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	1	1	2	2	3
-0.5 C < D < 0.5 C	666	666	663	666	664
0.5 C <= D < 1 C	2	2	4	1	2
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040200+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	666	666	666	666	666
mean:	0.00045	0.00041	0.00071	0.00078	0.00011
D <= -10 %	1	0	0	0	1
-10 % < D <= -5 %	3	2	4	3	4
-5 % < D <= -2 %	22	26	26	29	30
-2 % < D < 2 %	601	593	585	596	586
2 % <= D < 5 %	32	41	46	33	41
5 % <= D < 10 %	7	4	4	5	4
10 % <= D	0	0	1	0	0
T2m 2003040200+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	620	620	620	620	620
mean:	-0.00212	-0.00411	-0.00277	-0.00847	-0.00271
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	4	1	2	3	3
-0.5 C < D < 0.5 C	615	619	617	614	613
0.5 C <= D < 1 C	1	0	1	3	4
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040200+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	619	619	619	619	619
mean:	0.00082	0.00047	0.00069	0.00058	0.00058
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	1	1	0
-5 % < D <= -2 %	14	14	18	19	23
-2 % < D < 2 %	582	585	574	582	573
2 % <= D < 5 %	21	20	25	21	23
5 % <= D < 10 %	2	0	1	2	0
10 % <= D	0	0	0	0	0

T2m 2003040500+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	627	627	627	627	627
mean:	-0.00008	-0.00003	-0.00008	-0.00005	0.00007
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	627	627	627	627	627
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040500+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	626	626	626	626	626
mean:	-0.00001	-0.00001	0.00000	-0.00001	-0.00002
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	0	0	0	0	0
-2 % < D < 2 %	626	626	626	626	626
2 % <= D < 5 %	0	0	0	0	0
5 % <= D < 10 %	0	0	0	0	0
10 % <= D	0	0	0	0	0
T2m 2003040500+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	663	663	663	663	663
mean:	0.00078	-0.00014	0.00089	0.00134	0.00003
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	663	663	663	663	663
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040500+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	665	665	665	665	665
mean:	-0.00018	-0.00027	-0.00013	0.00002	-0.00015
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	1	1	1	1	1
-5 % < D <= -2 %	3	2	2	3	3
-2 % < D < 2 %	660	661	661	661	659
2 % <= D < 5 %	1	1	1	1	2
5 % <= D < 10 %	0	0	0	0	0
10 % <= D	0	0	0	0	0
T2m 2003040500+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	653	653	653	653	653
mean:	-0.00150	-0.00214	-0.00173	-0.00073	-0.00022
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	4	2	3	4	4
-0.5 C < D < 0.5 C	647	649	646	642	644
0.5 C <= D < 1 C	2	2	4	6	5
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040500+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	650	650	650	650	650
mean:	0.00114	0.00055	0.00157	0.00086	0.00121
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	3	3	3	4
-5 % < D <= -2 %	29	25	30	33	32
-2 % < D < 2 %	586	587	563	566	561
2 % <= D < 5 %	34	34	49	47	49
5 % <= D < 10 %	1	1	5	1	4
10 % <= D	0	0	0	0	0
T2m 2003040500+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	664	664	664	664	664
mean:	0.00236	0.00259	0.00148	-0.00136	0.00060
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	1	1	1	1	1
-1 C < D <= -0.5 C	1	1	2	1	3
-0.5 C < D < 0.5 C	658	659	656	659	655
0.5 C <= D < 1 C	3	3	3	1	2
1 C <= D < 2 C	1	0	2	2	3
2 C <= D	0	0	0	0	0
H2m 2003040500+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	661	661	661	661	661
mean:	-0.00021	0.00061	0.00002	0.00036	0.00029
D <= -10 %	1	0	1	1	2
-10 % < D <= -5 %	4	2	4	2	2
-5 % < D <= -2 %	31	25	30	24	40
-2 % < D < 2 %	598	605	588	603	572
2 % <= D < 5 %	22	26	35	27	40
5 % <= D < 10 %	5	3	3	4	5
10 % <= D	0	0	0	0	0
T2m 2003040500+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	629	629	629	629	629
mean:	0.00140	-0.00279	-0.00003	-0.00406	-0.00249
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	1	0	0	0
-1 C < D <= -0.5 C	0	1	0	0	1
-0.5 C < D < 0.5 C	629	626	628	629	626
0.5 C <= D < 1 C	0	1	1	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0

H2m 2003040500+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	623	623	623	623	623
mean:	-0.00086	-0.00035	-0.00032	-0.00081	-0.00093
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	2	2	1	4	3
-5 % < D <= -2 %	30	28	33	26	32
-2 % < D < 2 %	581	568	561	575	562
2 % <= D < 5 %	8	23	25	17	25
5 % <= D < 10 %	2	2	2	0	0
10 % <= D	0	0	1	1	1
T2m 2003040500+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	665	665	665	665	665
mean:	-0.00239	-0.00061	-0.00283	-0.00403	-0.00097
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	1	1	1	0	1
-0.5 C < D < 0.5 C	664	663	663	665	662
0.5 C <= D < 1 C	0	0	1	0	2
1 C <= D < 2 C	0	1	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040500+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	664	664	664	664	664
mean:	-0.00133	-0.00121	-0.00088	-0.00129	-0.00119
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	1	2	2	2	7
-5 % < D <= -2 %	32	37	34	34	40
-2 % < D < 2 %	619	599	605	607	589
2 % <= D < 5 %	12	25	20	21	26
5 % <= D < 10 %	0	1	3	0	2
10 % <= D	0	0	0	0	0
T2m 2003040500+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	656	656	656	656	656
mean:	-0.00321	-0.00353	0.00547	0.00192	-0.00222
D <= -2 C	0	0	0	0	1
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	18	17	15	11	12
-0.5 C < D < 0.5 C	620	625	623	633	628
0.5 C <= D < 1 C	18	14	16	12	13
1 C <= D < 2 C	0	0	2	0	2
2 C <= D	0	0	0	0	0
H2m 2003040500+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	646	646	646	646	646
mean:	0.00001	-0.00015	0.00065	0.00010	0.00008
D <= -10 %	0	0	0	0	2
-10 % < D <= -5 %	11	11	11	4	10
-5 % < D <= -2 %	49	55	45	59	65
-2 % < D < 2 %	520	510	517	524	495
2 % <= D < 5 %	62	64	67	50	65
5 % <= D < 10 %	3	5	5	9	9
10 % <= D	1	1	0	0	0
T2m 2003040500+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	641	641	641	641	641
mean:	-0.00010	0.00436	-0.00589	0.00481	-0.00483
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	2	0	2	1	1
-1 C < D <= -0.5 C	1	3	2	2	5
-0.5 C < D < 0.5 C	635	635	634	636	632
0.5 C <= D < 1 C	2	3	2	1	2
1 C <= D < 2 C	1	0	1	1	1
2 C <= D	0	0	0	0	0
H2m 2003040500+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	635	635	635	635	635
mean:	-0.00079	0.00093	0.00017	-0.00026	0.00025
D <= -10 %	0	0	1	0	0
-10 % < D <= -5 %	8	5	2	7	8
-5 % < D <= -2 %	44	39	46	46	46
-2 % < D < 2 %	546	540	534	541	525
2 % <= D < 5 %	30	42	43	41	49
5 % <= D < 10 %	6	9	7	5	6
10 % <= D	1	0	2	1	1
T2m 2003040500+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	611	611	611	611	611
mean:	-0.00524	-0.00261	-0.00906	0.00060	-0.00108
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	1	0	0	1	0
-1 C < D <= -0.5 C	1	2	4	3	2
-0.5 C < D < 0.5 C	609	608	607	607	607
0.5 C <= D < 1 C	0	1	0	0	2
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003040500+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	608	608	608	608	608
mean:	-0.00145	-0.00052	-0.00171	-0.00157	-0.00188
D <= -10 %	0	0	1	1	2
-10 % < D <= -5 %	8	3	7	3	5
-5 % < D <= -2 %	30	33	33	36	41
-2 % < D < 2 %	547	538	542	540	537
2 % <= D < 5 %	2	2	2	2	21
5 % <= D < 10 %	2	3	5	2	1
10 % <= D	1	2	0	2	1

T2m 2003050600+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	611	611	611	611	611
mean:	-0.00008	-0.00015	0.00003	-0.00003	0.00008
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	0	0	0	0
-0.5 C < D < 0.5 C	611	611	611	611	611
0.5 C <= D < 1 C	0	0	0	0	0
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003050600+0000	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	614	614	614	614	614
mean:	-0.00002	-0.00001	0.00000	-0.00001	-0.00001
D <= -10 %	0	0	0	0	0
-10 % < D <= -5 %	0	0	0	0	0
-5 % < D <= -2 %	0	0	0	0	0
-2 % < D < 2 %	614	614	614	614	614
2 % <= D < 5 %	0	0	0	0	0
5 % <= D < 10 %	0	0	0	0	0
10 % <= D	0	0	0	0	0
T2m 2003050600+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	660	660	660	660	660
mean:	0.01440	0.01314	0.01679	0.01404	0.01754
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	0	0	0
-1 C < D <= -0.5 C	0	1	0	1	0
-0.5 C < D < 0.5 C	655	656	651	655	653
0.5 C <= D < 1 C	5	3	9	4	7
1 C <= D < 2 C	0	0	0	0	0
2 C <= D	0	0	0	0	0
H2m 2003050600+0006	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	660	660	660	660	660
mean:	0.00218	0.00206	0.00398	0.00302	0.00423
D <= -10 %	2	2	3	2	4
-10 % < D <= -5 %	11	12	12	13	10
-5 % < D <= -2 %	30	29	27	32	32
-2 % < D < 2 %	559	559	534	549	531
2 % <= D < 5 %	41	43	51	47	50
5 % <= D < 10 %	12	10	22	14	24
10 % <= D	5	5	9	8	9
T2m 2003050600+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	659	659	659	659	659
mean:	0.03496	0.03186	0.05978	0.04252	0.07849
D <= -2 C	1	0	0	0	0
-2 C < D <= -1 C	6	4	7	8	7
-1 C < D <= -0.5 C	32	33	43	35	50
-0.5 C < D < 0.5 C	560	568	528	547	512
0.5 C <= D < 1 C	48	43	49	53	48
1 C <= D < 2 C	12	11	31	15	37
2 C <= D	0	0	1	2	4
H2m 2003050600+0012	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	655	655	655	655	655
mean:	0.00235	0.00211	0.00353	0.00284	0.00444
D <= -10 %	1	0	3	2	4
-10 % < D <= -5 %	17	17	22	18	30
-5 % < D <= -2 %	49	59	68	57	63
-2 % < D < 2 %	485	475	428	459	411
2 % <= D < 5 %	73	76	90	87	90
5 % <= D < 10 %	28	26	38	28	47
10 % <= D	2	2	6	4	10
T2m 2003050600+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	670	670	670	670	670
mean:	0.03318	0.03058	0.04049	0.03604	0.04493
D <= -2 C	0	0	3	0	2
-2 C < D <= -1 C	7	7	14	7	17
-1 C < D <= -0.5 C	24	25	32	33	35
-0.5 C < D < 0.5 C	593	593	555	574	545
0.5 C <= D < 1 C	28	28	38	33	39
1 C <= D < 2 C	17	16	21	16	23
2 C <= D	1	1	4	1	9
H2m 2003050600+0018	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	665	665	665	665	665
mean:	-0.00118	-0.00196	-0.00069	-0.00114	-0.00024
D <= -10 %	3	3	12	7	14
-10 % < D <= -5 %	25	25	29	30	37
-5 % < D <= -2 %	92	101	100	89	89
-2 % < D < 2 %	456	457	407	426	411
2 % <= D < 5 %	58	52	73	69	65
5 % <= D < 10 %	24	23	28	20	28
10 % <= D	7	4	16	10	21
T2m 2003050600+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	588	588	588	588	588
mean:	-0.01084	-0.00966	-0.01361	-0.01287	-0.01515
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	0	0	2	1	4
-1 C < D <= -0.5 C	12	12	13	16	16
-0.5 C < D < 0.5 C	566	567	555	562	553
0.5 C <= D < 1 C	9	7	10	11	8
1 C <= D < 2 C	1	2	5	1	7
2 C <= D	0	0	0	0	0

H2m 2003050600+0024	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	586	586	586	586	586
mean:	-0.00216	-0.00238	-0.00295	-0.00255	-0.00269
D <= -10 %	0	0	1	1	2
-10 % < D <= -5 %	3	3	6	4	9
-5 % < D <= -2 %	58	57	74	68	74
-2 % < D < 2 %	495	495	469	480	453
2 % <= D < 5 %	26	26	28	26	40
5 % <= D < 10 %	3	3	6	6	7
10 % <= D	1	2	2	1	1
T2m 2003050600+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	665	665	665	665	665
mean:	0.00196	0.00215	-0.00441	0.00009	-0.00311
D <= -2 C	0	0	0	0	0
-2 C < D <= -1 C	1	0	2	2	2
-1 C < D <= -0.5 C	11	10	14	13	16
-0.5 C < D < 0.5 C	640	641	631	634	628
0.5 C <= D < 1 C	10	12	14	13	15
1 C <= D < 2 C	3	2	4	3	4
2 C <= D	0	0	0	0	0
H2m 2003050600+0030	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	660	660	660	660	660
mean:	0.00067	0.00082	0.00025	0.00061	0.00001
D <= -10 %	0	0	4	4	6
-10 % < D <= -5 %	7	6	14	13	17
-5 % < D <= -2 %	49	53	59	52	68
-2 % < D < 2 %	536	530	507	522	475
2 % <= D < 5 %	48	49	52	49	68
5 % <= D < 10 %	12	14	17	16	19
10 % <= D	4	4	7	4	7
T2m 2003050600+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	658	658	658	658	658
mean:	0.02415	0.01972	0.04342	0.02992	0.03947
D <= -2 C	2	2	3	3	3
-2 C < D <= -1 C	13	15	26	21	26
-1 C < D <= -0.5 C	43	35	43	39	50
-0.5 C < D < 0.5 C	538	545	498	518	476
0.5 C <= D < 1 C	45	46	57	54	70
1 C <= D < 2 C	16	14	26	20	26
2 C <= D	1	1	5	3	7
H2m 2003050600+0036	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	658	658	658	658	658
mean:	0.00156	0.00171	0.00302	0.00303	0.00368
D <= -10 %	4	4	5	5	11
-10 % < D <= -5 %	33	28	36	33	47
-5 % < D <= -2 %	67	67	66	66	63
-2 % < D < 2 %	431	430	394	418	377
2 % <= D < 5 %	84	87	89	86	91
5 % <= D < 10 %	33	36	44	40	54
10 % <= D	6	6	18	10	15
T2m 2003050600+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	658	658	658	658	658
mean:	0.05080	0.05025	0.06201	0.04978	0.07108
D <= -2 C	1	1	3	2	5
-2 C < D <= -1 C	11	8	25	20	26
-1 C < D <= -0.5 C	42	41	43	38	47
-0.5 C < D < 0.5 C	538	545	494	518	474
0.5 C <= D < 1 C	40	39	53	53	62
1 C <= D < 2 C	23	21	32	22	38
2 C <= D	3	3	8	5	6
H2m 2003050600+0042	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	656	656	656	656	656
mean:	-0.00063	-0.00076	0.00081	0.00018	0.00123
D <= -10 %	15	15	26	17	27
-10 % < D <= -5 %	45	43	50	50	55
-5 % < D <= -2 %	71	67	66	70	62
-2 % < D < 2 %	404	412	367	374	355
2 % <= D < 5 %	73	76	77	84	77
5 % <= D < 10 %	33	30	44	41	51
10 % <= D	15	15	26	20	29
T2m 2003050600+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	600	600	600	600	600
mean:	-0.01649	-0.01285	-0.02200	-0.01904	-0.01638
D <= -2 C	0	0	1	1	2
-2 C < D <= -1 C	6	6	7	4	9
-1 C < D <= -0.5 C	28	24	42	34	43
-0.5 C < D < 0.5 C	542	544	512	527	502
0.5 C <= D < 1 C	20	23	31	28	36
1 C <= D < 2 C	4	3	6	6	6
2 C <= D	0	0	1	0	2
H2m 2003050600+0048	OP - 10SM61	OP - 21SM41	OP - 21SM61	OP - 30SM41	OP - 30SM61
total nr.:	606	606	606	606	606
mean:	-0.00394	-0.00393	-0.00478	-0.00469	-0.00450
D <= -10 %	1	1	9	2	11
-10 % < D <= -5 %	25	24	31	28	29
-5 % < D <= -2 %	80	75	86	83	85
-2 % < D < 2 %	446	449	403	438	396
2 % <= D < 5 %	45	46			

