

TOUCANS

- internal architecture of turbulence part

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Introduction

Vertical turbulent flux:

$$\overline{w' \psi'} = -K_\psi \frac{\partial \bar{\psi}}{\partial z} \Rightarrow \frac{\partial \psi}{\partial t} = \frac{\partial}{\partial z} \left(K_\psi \frac{\partial \psi}{\partial z} \right)$$

$$z \rightarrow 0 : \quad \overline{w' \psi'} = C_\psi \cdot \sqrt{\bar{u}^2 + \bar{v}^2} (\psi(z) - \psi_s)$$

K_ψ - exchange coefficient for ψ

C_ψ - drag coefficient for ψ , ψ_s - ψ at surface

Introduction

Exchange coefficients $K_{m/h}$ and
drag coefficients $C_{M/H}$ in Louis scheme:

$$K_{m/h} = I_{m/h} I_m \left[\left(\frac{\partial \bar{u}}{\partial z} \right)^2 + \left(\frac{\partial \bar{v}}{\partial z} \right)^2 \right]^{\frac{1}{2}} F_{m/h}(Ri)$$

$$C_{M/H} = C_{M/H}^N(z, z_0, \kappa) \cdot F_{m/h}(Ri)$$

$I_{m/h}$ - Prandtl mixing length for momentum and pot. temperature

$F_{m/h}(Ri)$ - stability functions, Ri - Richardson gradient number

u , v , w - wind components , z - height, z_0 - roughness

$C_{M/H}^N$ - drag coefficient at neutrality($Ri = 0$)

κ - von Karman constant

Introduction

Louis stability functions F_m and F_h :
stable case:

$$F_m(Ri) = \frac{1}{1 + \frac{2bRi}{\sqrt{1 + \frac{d}{k} Ri}}}$$

$$F_h(Ri) = \frac{1}{1 + 3bRi\sqrt{1 + dkRi}}$$

unstable case:

$$F_m(Ri) = 1 - \frac{2bRi}{1 + 3bc\sqrt{\frac{|Ri|}{27}} \left(\frac{I_m}{z+z_0} \right)^2}$$

$$F_h(Ri) = 1 - \frac{3bRi}{1 + 3bc\sqrt{\frac{|Ri|}{27}} \left(\frac{I_h}{z+z_{0h}} \right) \left(\frac{I_m}{z+z_0} \right)}$$

b, c, d, k - constants,

z_0, z_{0H} - roughness

Introduction

TKE equation:

$$\frac{dE}{dt} = \underbrace{-\overline{u' \cdot w'} \frac{\partial \bar{u}}{\partial z} - \overline{v' \cdot w'} \frac{\partial \bar{v}}{\partial z}}_{\text{shear (I)}} + \frac{g}{\bar{\rho}} (\overline{w' \cdot \theta'}) \text{ buoyancy(II)}$$
$$-\frac{\partial(\overline{w' \cdot E})}{\partial z} - \frac{1}{\bar{\rho}} \frac{\partial(\overline{w' \cdot p'})}{\partial z} - C_\epsilon \frac{(E)^{\frac{3}{2}}}{L_\epsilon}$$

turb. trans. of TKE pressure cor. dissipation(ϵ)

$E = \frac{1}{2}(\overline{u' \cdot u' + v' \cdot v' + w' \cdot w'})$ - TKE (Turbulence Kinetic Energy)

L_ϵ - mixing length, C_ϵ - closure constant

θ - potential temperature, ρ - density, p - atm. pressure

Introduction

extended CBR scheme:

$$I = -\overline{u'w'} \frac{\partial \bar{u}}{\partial z} - \overline{v'w'} \frac{\partial \bar{v}}{z} = L_K C_K \sqrt{E} \left[\left(\frac{\partial \bar{u}}{\partial z} \right)^2 + \left(\frac{\partial \bar{v}}{\partial z} \right)^2 \right] \chi_3(Ri)$$

$$II = \frac{g}{\theta} \overline{\theta' w'} = -\frac{g}{\theta} L_K C_K C_3 \sqrt{E} \frac{\partial \bar{\theta}}{\partial z} \phi_3(Ri)$$

$$III = -\epsilon = -C_\epsilon \frac{(E)^{\frac{3}{2}}}{L_\epsilon}$$

$$\Rightarrow K_m = L_K C_K \sqrt{E} \chi_3(Ri)$$

$$K_h = L_K C_K C_3 \sqrt{E} \phi_3(Ri)$$

$\chi_3(Ri)$, $\phi_3(Ri)$ - stability functions, L_K - mixing length

C_K - closure constant, C_3 - inverse Prandtl number at neutrality ($Ri = 0$)

Introduction

The full TKE equation:

$$\frac{dE}{dt} = -\frac{\partial}{\partial z} \left(\overline{E'w'} + \frac{\overline{p'w'}}{\rho} \right) + I + II + III$$

TKE eqation in pTKE:

$$\frac{dE}{dt} = -\frac{\partial}{\partial z} \left(-K_E \frac{\partial E}{\partial z} \right) + \frac{1}{\tau_\epsilon} (\tilde{E} - E)$$

\tilde{E} - TKE at stationary equilibrium

$\tau_\epsilon = \frac{E}{\epsilon}$ - dissipation time scale

$K_E = -\frac{\overline{E'w'} + \frac{\overline{p'w'}}{\rho}}{\frac{\partial E}{\partial z}}$ - auto-diffusion vertical coefficient for the TKE

Introduction

pTKE scheme:

$$\tilde{E} = \left(\frac{K^*}{\nu l_m} \right)^2$$

$$\tau_\epsilon = \frac{\nu^3 \sqrt{E}}{l_m} = \frac{l_m^2}{\nu^2 K^*}$$

$$K_E = \frac{l_m \sqrt{E}}{\nu} = \underbrace{\frac{K^*}{\nu^2}}$$

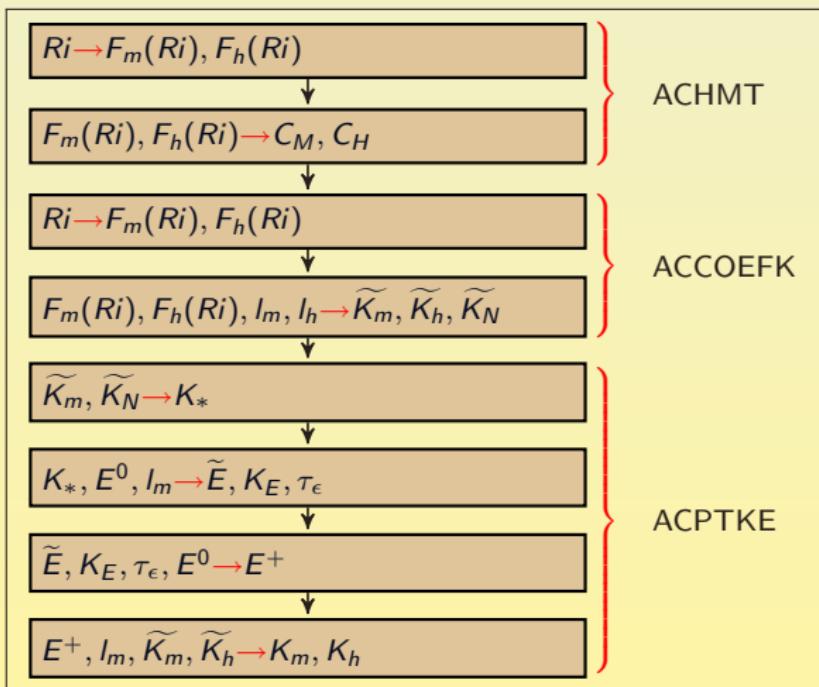
first time step

$$\nu = (C_K C_\epsilon)^{\frac{1}{4}}, K^* = \sqrt{K_m K_N}$$

$K_N - K_m$ for neutral stratification ($Ri = 0$)

Introduction

pTKE scheme - draft:



Stability functions F_m and F_h

Condition of equivalence with full TKE:

$$\tilde{E}(L_K) = \frac{E}{\epsilon(L_\epsilon)} [I(L_K) + II(L_K)]$$

Mixing lengths relation:

$$L_K C_K = \nu l_m \frac{f(Ri)^{\frac{1}{4}}}{\chi_3^{\frac{1}{2}}} ,$$

$$\frac{L_\epsilon}{C_\epsilon} = \frac{l_m}{\nu^3} \frac{\chi_3^{\frac{3}{2}}}{f(Ri)^{\frac{3}{4}}} ,$$

$$f(Ri) = \chi_3(Ri) - Ri C_3 \phi_3(Ri)$$

Stability functions F_m and F_h

From definition of $F_m(Ri)$ and $F_h(Ri)$:

$$F_{m/h}(Ri) = \frac{\tilde{K}_{m/h}}{l_m l_{m/h} \sqrt{\left[\left(\frac{\partial \bar{u}}{\partial z} \right)^2 + \left(\frac{\partial \bar{v}}{\partial z} \right)^2 \right]}}$$

we get resulting :

$$F_m(Ri) = \chi_3(Ri) \sqrt{f(Ri)} = \chi_3(Ri) \sqrt{\chi_3(Ri)(1 - Ri_f)}$$

$$F_h(Ri) = \frac{\phi_3(Ri)}{\chi_3(Ri)} F_m(Ri)$$

$Ri_f = Ri \frac{K_h}{K_m}$ - flux Richardson number

Stability functions χ_3 , ϕ_3

Modified CCH02 scheme (no critical Ri):

$$\begin{aligned}\chi_3(Ri) &= \frac{1 - \frac{Ri_f}{R}}{1 - Ri_f} = \\ &= \frac{f(Ri)}{f(Ri).R + 1 - R} ,\end{aligned}$$

$$\begin{aligned}\phi_3(Ri) &= \frac{1 - \frac{Ri_f}{Ri_{fc}}}{1 - Ri_f} = \\ &= \left(1 - \frac{1 - Q}{f(Ri).R + 1 - R}\right) \frac{f(Ri)}{f(Ri).Q + 3\lambda_0 Ri} ,\end{aligned}$$

$$Ri_f = \frac{C_3 Ri \phi_3(Ri)}{\chi_3(Ri)}, \quad Ri_{fc} = \lim_{Ri \rightarrow \infty} Ri_f$$

R , Q , λ_0 - constants

Stability functions χ_3 , ϕ_3

Fitted QNSE scheme:

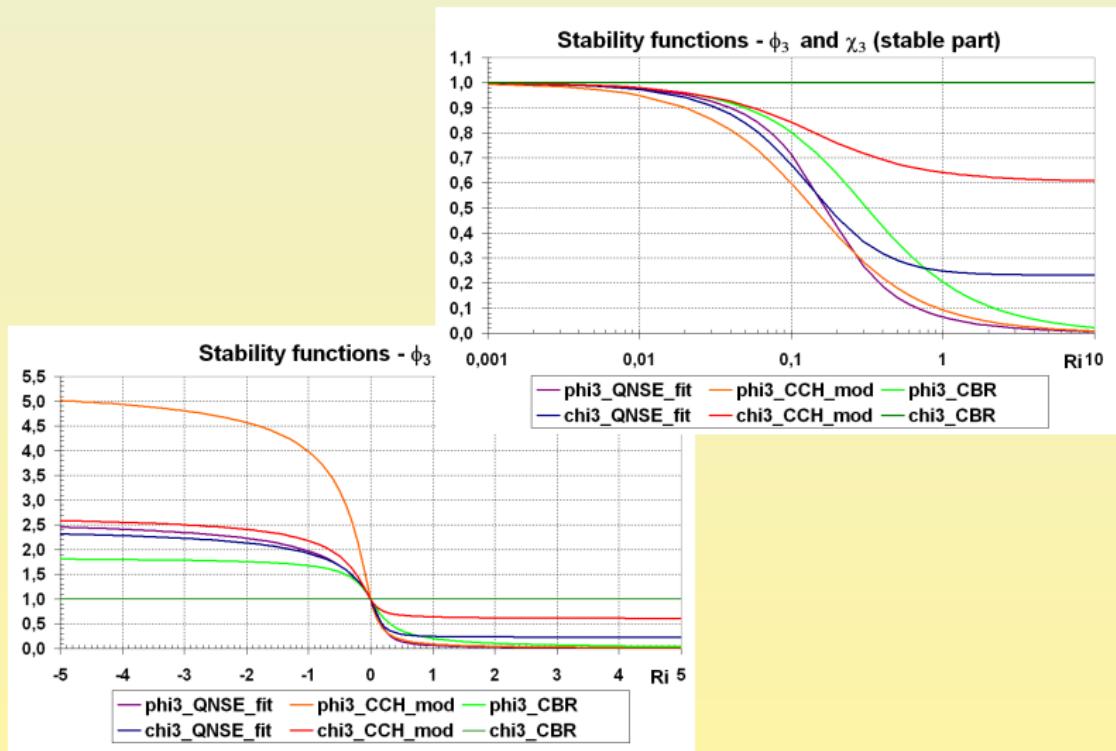
$$\text{for } Ri \geq 0 \quad \chi_3(Ri) = \frac{1 + 0.75Ri(1 + a.Ri)}{1 + 3.23Ri(1 + a.Ri)} ,$$
$$\text{for } Ri < 0 \quad \chi_3(Ri) = \frac{1 - b.Ri}{1 - (b - 2.48).Ri} ,$$

$a = 13.0$, $b = 4.16$ - tuning constants

Stability function $\phi_3(Ri)$ is computed from quadratic equation derived in modified CCH02:

$$C_3 Ri \phi_3(Ri)^2 - \left[\chi_3(Ri) + \frac{C_3 Ri}{Ri_{fc}} \right] \phi_3(Ri) + \chi_3(Ri) = 0$$

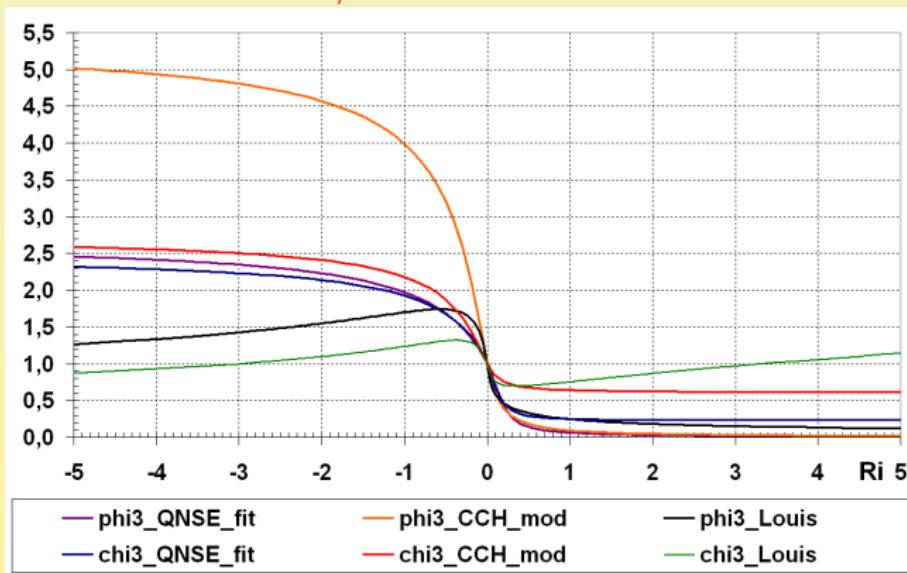
Stability functions χ_3 , ϕ_3



Modification in K_E , τ_ϵ

pTKE scheme:

- simplified assumptions
- derived for CBR scheme ($\chi_3 = 1$)
- from Louis $F_{m/h}$:



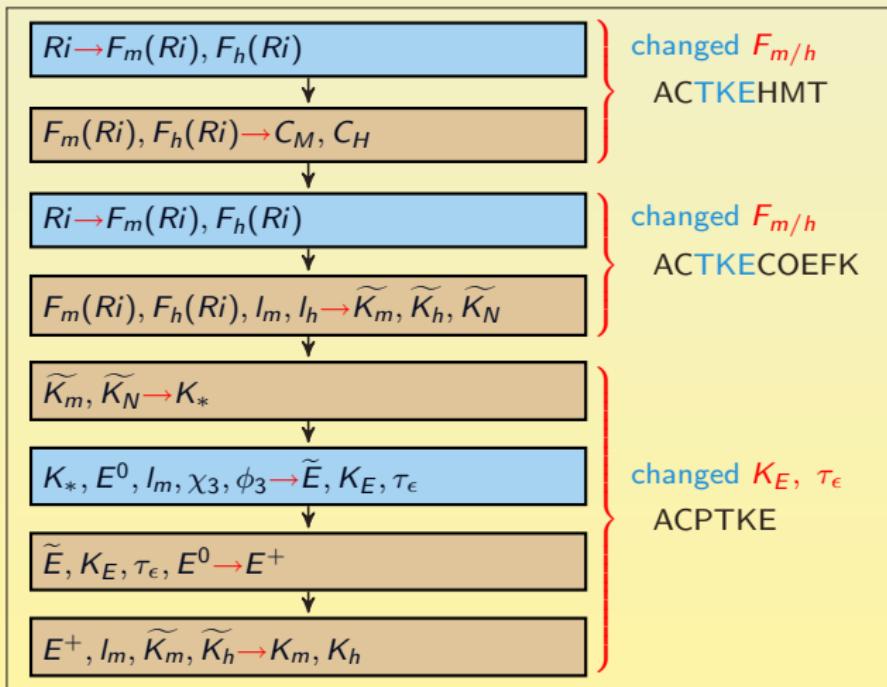
Modification in K_E , τ_ϵ

Relation for K_E , τ_ϵ in eTKE:

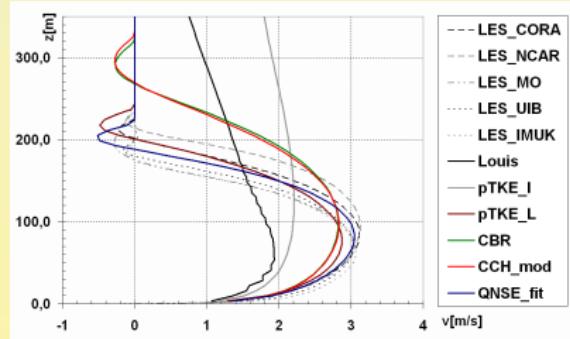
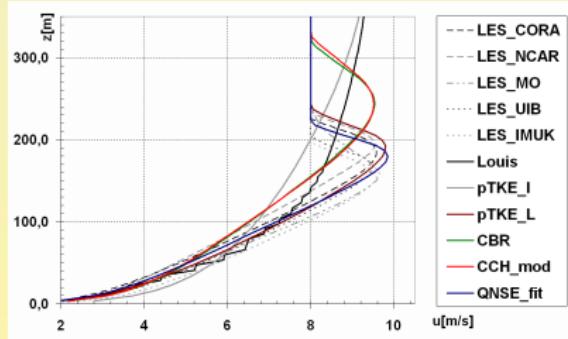
$$\tau_\epsilon = \frac{I_m}{\nu^3 \sqrt{E}} \frac{\chi_3(Ri)^{\frac{3}{2}}}{f(Ri)^{\frac{3}{4}}}$$

$$K_E = \frac{I_m \sqrt{E}}{\nu} \frac{f(Ri)^{\frac{3}{4}}}{\chi_3(Ri)^{\frac{3}{2}}}$$

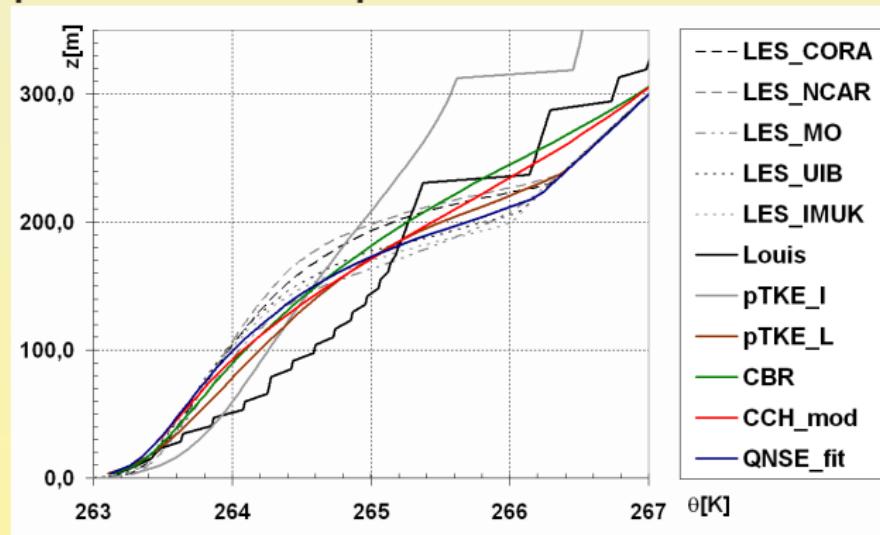
eTKE scheme - draft:



1D test: project GABLs wind components:



1D test: project GABLs potential temperature:



- inversion layer under top of PBL

'Dry' AF scheme

Antifibrillation scheme

-to avoid nonlinear instabilities in diffusion equation

Decentered diffusion equation:

$$\frac{\partial \psi}{\partial t} = \frac{\psi^+ - \psi^0}{\Delta t} = \frac{\partial \left[(1 - \beta) K_\psi \frac{\partial \psi^0}{\partial z} + \beta K_\psi \frac{\partial \psi^+}{\partial z} \right]}{\partial z}$$

β - decentering factor

Δt - timestep, t - time

'Dry' AF scheme

β is function of $\tilde{K}_{m/h}$, α_u and α_θ :

$$\begin{aligned}\alpha_u &= \frac{Ri}{F_m(Ri)} \left(\frac{dF_m(Ri)}{dRi} \right) \\ \alpha_\theta &= \frac{Ri}{F_h(Ri)} \left(\frac{dF_h(Ri)}{dRi} \right)\end{aligned}$$

We modified computation of α_u and α_θ

according to the 'new' $F_{m/h}$

'Dry' AF scheme

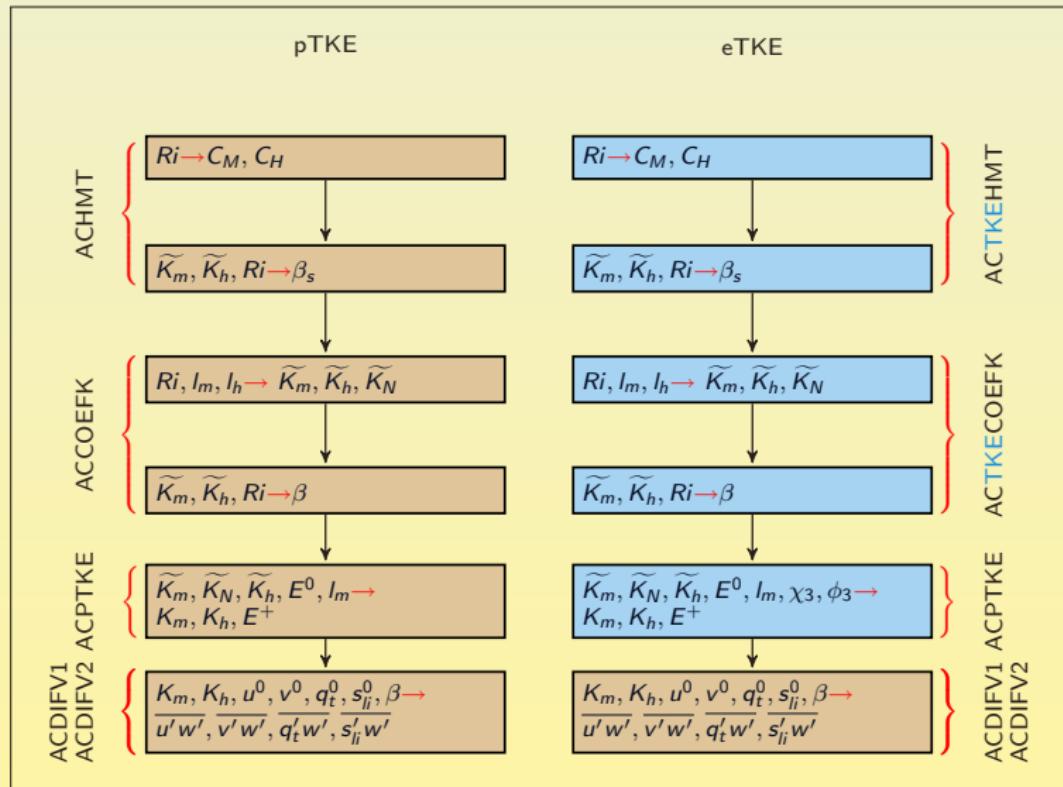
Conditions for use of 'dry' AF scheme
are not fulfilled for all Ri :

$$K_m \geq \frac{K_h}{3} \quad \text{or} \quad \alpha_\theta > -1 \quad (\text{for } Ri > 0)$$

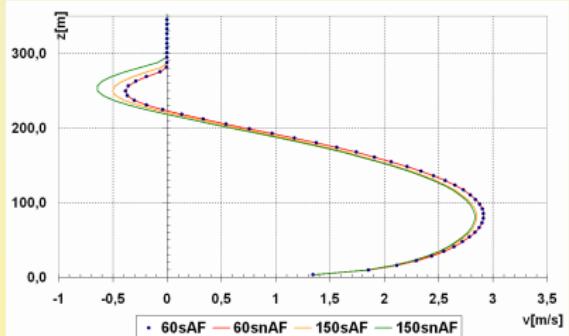
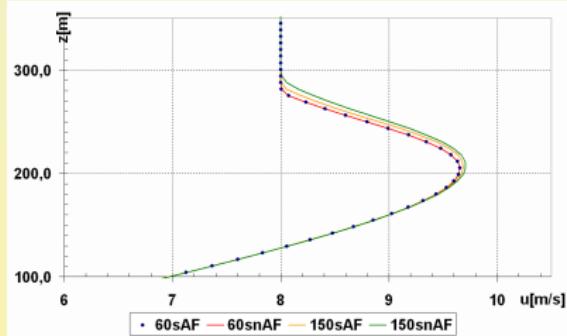
$$-2 < (\alpha_u, \alpha_\theta) < 1$$

$$2 < 3 - 2.\alpha_u + \alpha_\theta$$

$$0 < 2 - 3.\alpha_u + 2.\alpha_\theta \leq 2$$



Influence of AF scheme:



CCH_mod: $C_3 = 1.83$, $\nu = 0.477$, $R = 0.367$, $Ri_{fc} = 0.186$,
 $\alpha_{TKE} = 3.9$

Turbulent scheme

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Mixing lengths

oooooooooooooo

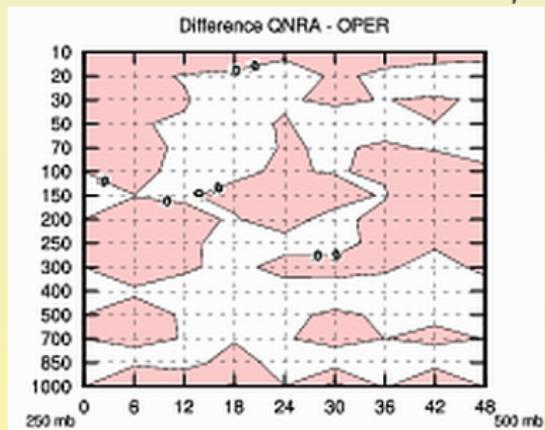
Preparations for TOMs

oooooo

Shallow conv. cloudiness

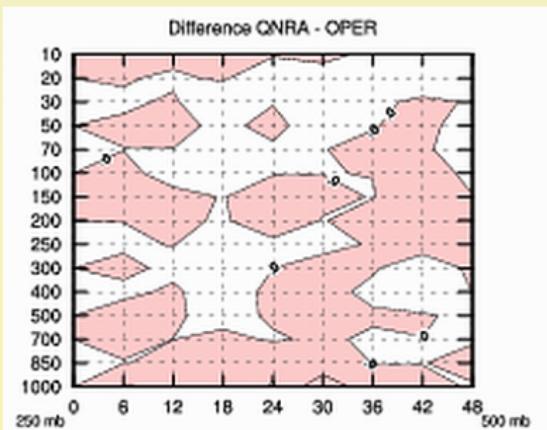
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3D test: eTKE(QNSE) vs pTKE - temperature:
01.01.2009-24.01.2009, 00:00 UTC



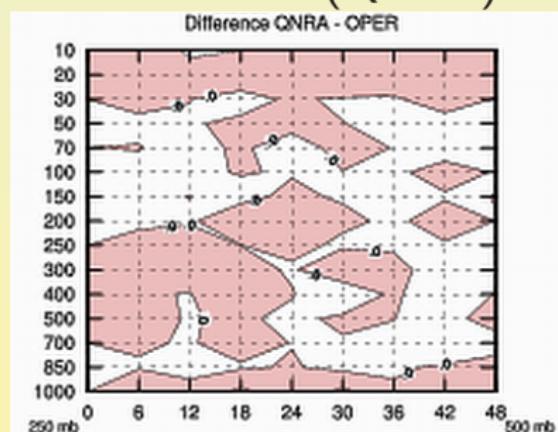
RMSE

-red - better score for eTKE



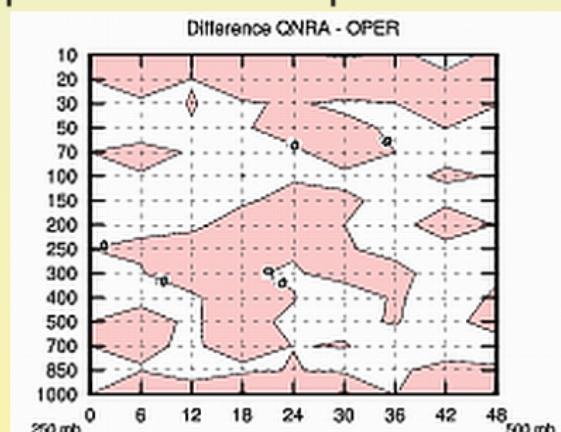
STDEV

3D test: eTKE(QNSE) vs pTKE - wind speed:



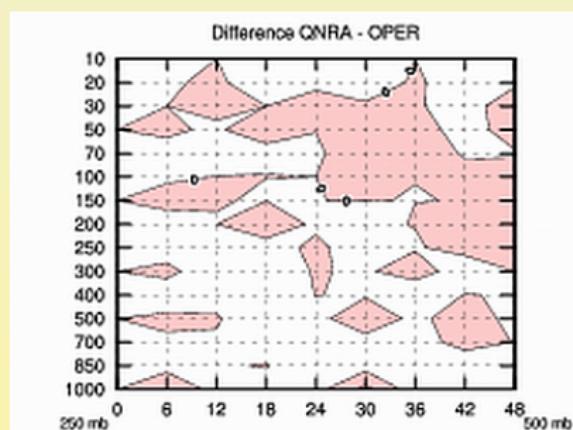
RMSE

-red - better score for eTKE

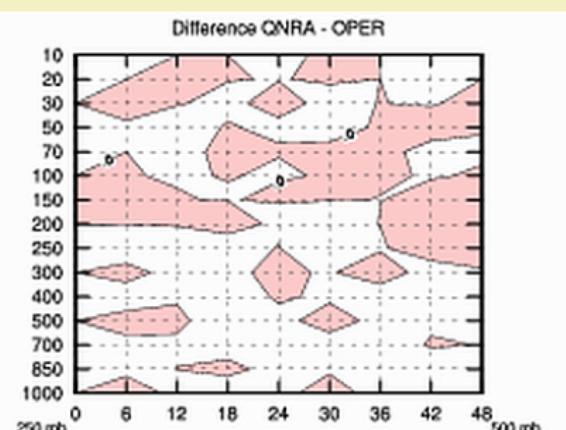


STDEV

3D test: eTKE(QNSE) vs pTKE - relative humidity:



RMSE



STDEV

-red - better score for eTKE

Mixing lengths

Prandtl-type mixing lengths
(CGMIXLEN='AY', in ALARO0='CG'):

$$l_{m/h}^{AY} = \frac{\kappa z}{1 + \frac{\kappa z}{\lambda_{m/h}} \left[\frac{1 + \exp(-a_{m/h}\sqrt{\frac{z}{H_{PBL}}} + b_{m/h})}{\beta_{m/h} + \exp(-a_{m/h}\sqrt{\frac{z}{H_{PBL}}} + b_{m/h})} \right]}$$

κ - Von Kármán constant, H_{PBL} - PBL height
 $a_{m/h}$, $b_{m/h}$, $\lambda_{m/h}$ - tuning constants

Mixing lengths

TKE mixing lengths:

$$L^{BL}(E') = \left(\frac{L_{up}^{-\frac{4}{5}} + L_{down}^{-\frac{4}{5}}}{2} \right)^{-\frac{5}{4}},$$

$$L^N(E') = \sqrt{\frac{2E'}{N^2}},$$

$$E' = \alpha_{TKE} E.$$

$L_{up/down}$ - represents the distance that a parcel originating from the given level, and having initial kinetic energy equal to the scaled mean TKE of the layer, can travel upward(downward) before being stopped by buoyancy effects

N - Brunt–Väisälä frequency

α_{TKE} -tunable degree of freedom

Mixing lengths

In the code we use I_m .

Conversion is made by $L_K(I_m)$:

$$L \equiv \sqrt{L_K L_\epsilon} = \frac{\nu}{C_K} I_m \frac{\chi_3(Ri)^{\frac{1}{2}}}{f(Ri)^{\frac{1}{4}}}$$

→ I_m becomes function of Ri .

Mixing lengths

Combinations of mixing lengths
CGMIXLEN=:

$$'EL1' \quad I_m = I_m^{BL}$$

$$'EL2' \quad Ri > 0 : I_m = \min(I_m^{BL}, I_m^N); \quad Ri < 0 : I_m = \sqrt{I_m^{BL} I_m^{AY}}$$

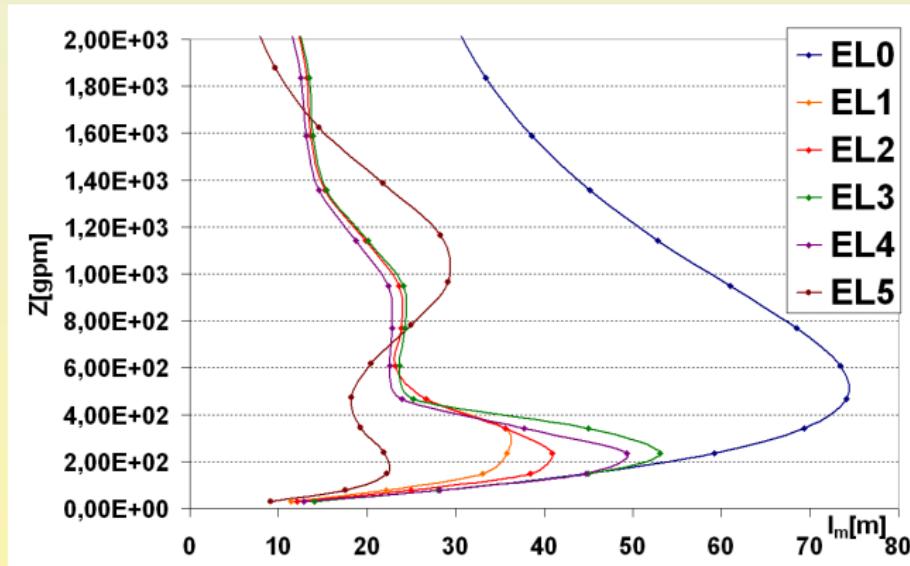
$$'EL3' \quad Ri > 0 : I_m = \min(I_m^N, I_m^{max}); \quad Ri < 0 : I_m = I_m^{AY}$$

$$'EL4' \quad Ri > 0 : I_m = \left(\frac{1}{(I_m^{AY})^2} + \frac{1}{(I_m^N)^2} \right)^{-2}; \quad Ri < 0 : I_m = I_m^{AY}$$

$$'EL5' \quad Ri > 0 : I_m = \min(I_m^{BL}, I_m^N); \quad Ri < 0 : I_m = I_m^{BL}$$

I_m^{max} - limitation for mixing length

Mixing lengths



CCH_mod:

$$C_3 = 1.83, \nu = 0.477, R = 0.367, Ri_{fc} = 0.186,$$
$$\alpha_{TKE} = 3.9, \delta_t = 360s, t = 360s$$

19.04.2009 00:00 UTC

Vertical profile of Prandtl number at neutrality

Trubulent Prandtl number:

$$Pr_t = \frac{K_m}{K_h}$$

In the code:

$$Pr_t(Ri = 0) \equiv Pr_{t0} = \frac{l_m}{l_h}$$

Conditions:

free atmosphere: $Pr_{t0} = \frac{1}{C_3}$

surface: $Pr_{t0} = 1$

Vertical profile of Prandtl number at neutrality

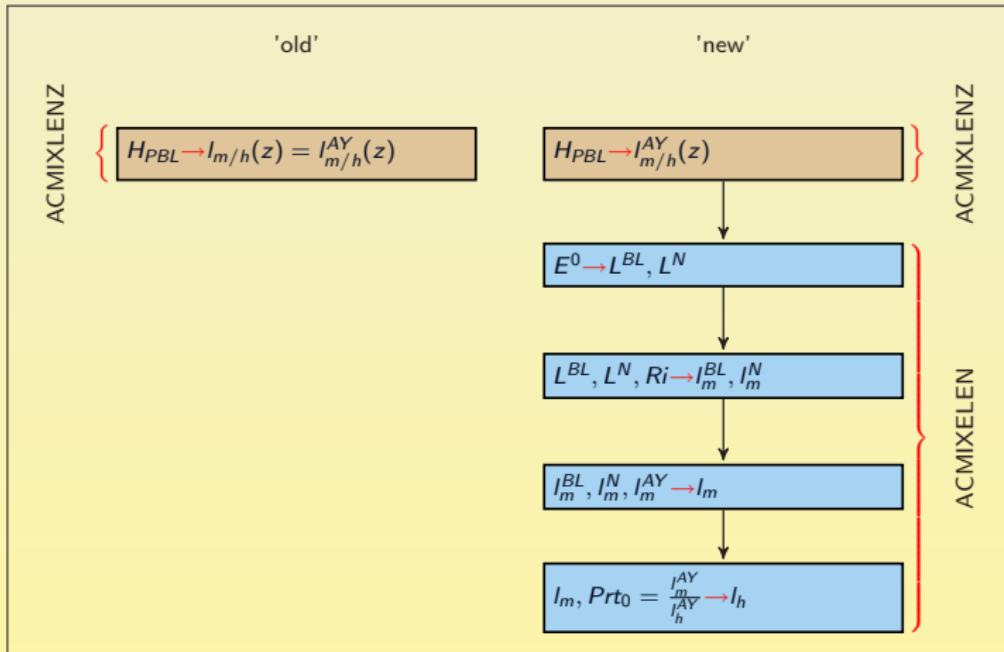
Solution with use of $I_{m/h}^{AY}$:

$$\frac{\lambda_m}{\lambda_h} = \frac{1}{C_3}$$

$$\frac{\beta_m}{\beta_h} = 1$$

Usage:

$$I_h = \frac{I_h^{AY}}{I_m^{AY}} I_m$$



We need to modify the code so, that there are no modification of exchange coefficients $K_{m/h}$ after their calculation from stability functions $F_{m/h}$.

Currently there are two modifications:

- 'moist' AF scheme
- parametrisation of moist gustiness

'Moist' antifibrillation scheme

Shallow convection parametrisation:

$$Ri^* = Ri_d + \frac{g}{c_p T} \frac{L_v \cdot \min \left[0, \frac{\partial(q - q_s)}{\partial z} \right]}{\left[\frac{\partial u}{\partial z} \right]^2 + \left[\frac{\partial v}{\partial z} \right]^2}$$

q - specific moisture, q_s - specific moisture for saturated air

L_v - latent heat of vaporization, c_p - specific heat capacity

Ri_d - 'dry' (without shallow convection parametrisation) Ri

'Moist' antifibrillation scheme

'Moist' antifibrillation scheme:

$$K'_{m/h}(Ri_d, Ri^*) = K_{m/h}(Ri_d) + \frac{K_{m/h}(Ri^*) - K_{m/h}(Ri_d)}{1 + (\beta_m - 1)(K_{m/h}(Ri^*) - K_{m/h}(Ri_d))\Delta t}$$
$$\beta_m = \frac{\frac{\partial(q_s^+)}{\partial z}}{\frac{\partial(q - q_s)}{\partial z}} \frac{1}{XDAMP}$$

q_s^+ - specific moisture for saturated air after mixing

$XDAMP$ - damping factor

β_m - decentering factor, obtained independently by considering the ratio of the vertical gradients before and after mixing

'Moist' antifibrillation scheme

We shifted 'moist' AF into computation of Ri

Modification in stability functions $F_{m/h}$ instead of $K_{m/h}$:

$$\begin{aligned} F_{m/h}(Ri') &= F'_{m/h}(Ri, Ri^*) = F_{m/h}(Ri_d) + \\ &+ \frac{F_{m/h}(Ri^*) - F_{m/h}(Ri_d)}{1 + (\beta_m - 1)(F_{m/h}(Ri^*) - F_{m/h}(Ri_d))I_m I_h \sqrt{\left(\frac{\partial \bar{u}}{\partial z}\right)^2 + \left(\frac{\partial \bar{v}}{\partial z}\right)^2} \Delta t} \end{aligned}$$

'Moist' antifibrillation scheme

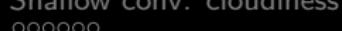
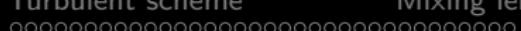
Special form of χ_3 , ϕ_3 in modified CCH02
derived by Daan Degrauwé:

$$\phi_3 = \frac{S - 1}{Ri_{fc} \cdot S - 1}$$

$$\chi_3 = \frac{\frac{S}{\sigma} - 1}{Ri_{fc} \cdot S - 1}$$

$$S = \frac{Ri_f}{Ri_{fc}} = \frac{1}{2} \left[\sigma(1 + \rho) - \sqrt{(1 + \rho)^2 \sigma^2 - 4\rho\sigma} \right]$$

$$\sigma = \frac{R}{Ri_{fc}}, \quad \rho = \frac{C_3 Ri}{Ri_{fc}}$$



'Moist' antifibrillation scheme

$$F_h = \phi_3 \sqrt{\chi_3(1 - Ri_f)} = \frac{S - 1}{Ri_{fc} \cdot S - 1} \sqrt{\frac{S}{\sigma} - 1}$$

Inversion of F_h in modified CCH02:

$$0 = S^3 + ((F_h^2 Ri_{fc}^2 - 1) \sigma - 2) S^2 + \\ + ((2 - 2 F_h^2 Ri_{fc}) \sigma + 1) S + (F_h^2 - 1) \sigma$$

$$Ri' = \frac{Ri_{fc}}{C_3} \frac{S}{\sigma} \frac{S - \sigma}{S - 1}$$

'Moist' antifibrillation scheme

QNSE:

- unable to invert F_h analytically
- we fitted QNSE functions χ_3 , ϕ_3
in modified CCH02 :
 R, C_3 - functions of Ri , $Ri_{fc} = 0.377$, $\nu = 0.464$

Moist gustiness modification

Gustiness:

$$\overline{w'\psi'} \sim \sqrt{\left[\left(\frac{\partial u}{\partial z} \right)^2 + \left(\frac{\partial v}{\partial z} \right)^2 \right]^{\frac{1}{2}}}$$

$$\left[\left(\frac{\partial \bar{u}}{\partial z} \right)^2 + \left(\frac{\partial \bar{v}}{\partial z} \right)^2 \right]^{\frac{1}{2}} < \sqrt{\left[\left(\frac{\partial u}{\partial z} \right)^2 + \left(\frac{\partial v}{\partial z} \right)^2 \right]^{\frac{1}{2}}}$$

NWP model

Moist gustiness modification

Moist gustiness
-induced by moist convection:

$$K_{m/h}^{PRC} = \gamma^{PRC} K_{m/h}, \quad C_{M/H}^{PRC} = \gamma^{PRC} C_{M/H}$$

$$\gamma^{PRC} = \sqrt{1 + \left(\left(\frac{J_{Pr}}{J_{Pr} + J_{Pr}^0} \right)^\gamma \tilde{U} \right)^2 \frac{\rho}{J_m}}$$

J_{Pr} - precipitation flux, J_{Pr}^0 - typical steadily strong precipitation flux
 J_m - momentum flux:

$$\text{above surface} = \rho \cdot K_m \cdot \sqrt{\left(\frac{\partial \bar{u}}{\partial z}\right)^2 + \left(\frac{\partial \bar{v}}{\partial z}\right)^2}, \text{ surface} = \rho \cdot C_M \cdot (\bar{u}^2 + \bar{v}^2)$$

\tilde{U} - typical surface friction velocity, $\gamma = 0.8$ - tuning constant

Moist gustiness modification

We shifted moist gustiness
in to the computation of $I_{m/h}$:

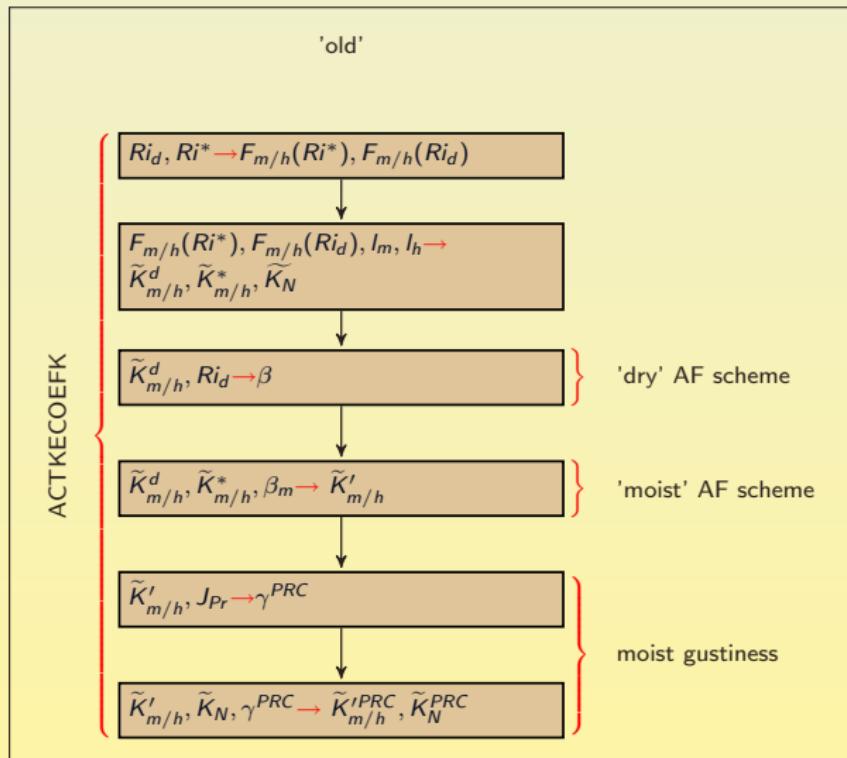
$$I_{m/h}^{PRC} = \sqrt{\gamma^{PRC}} I_{m/h}$$

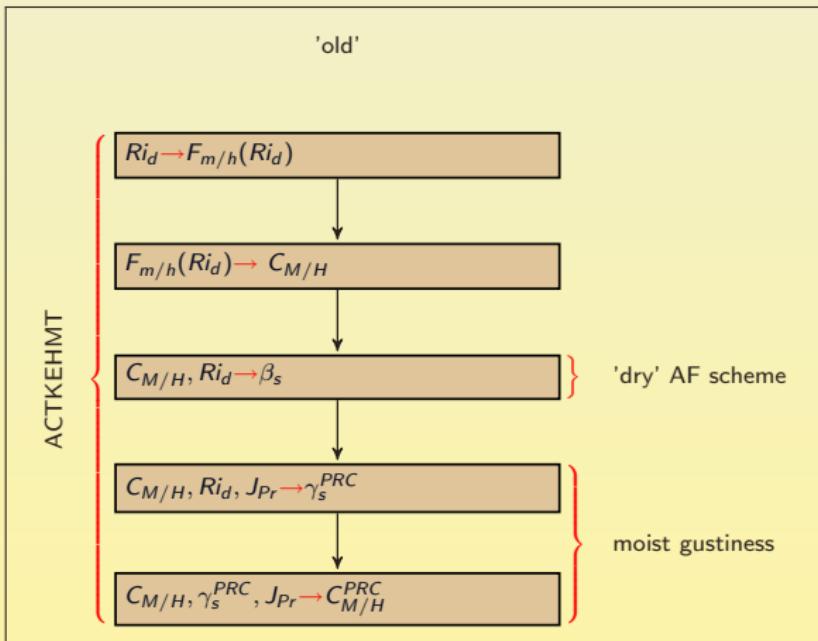
$$K_{m/h} \sim I_{m/h} I_m$$

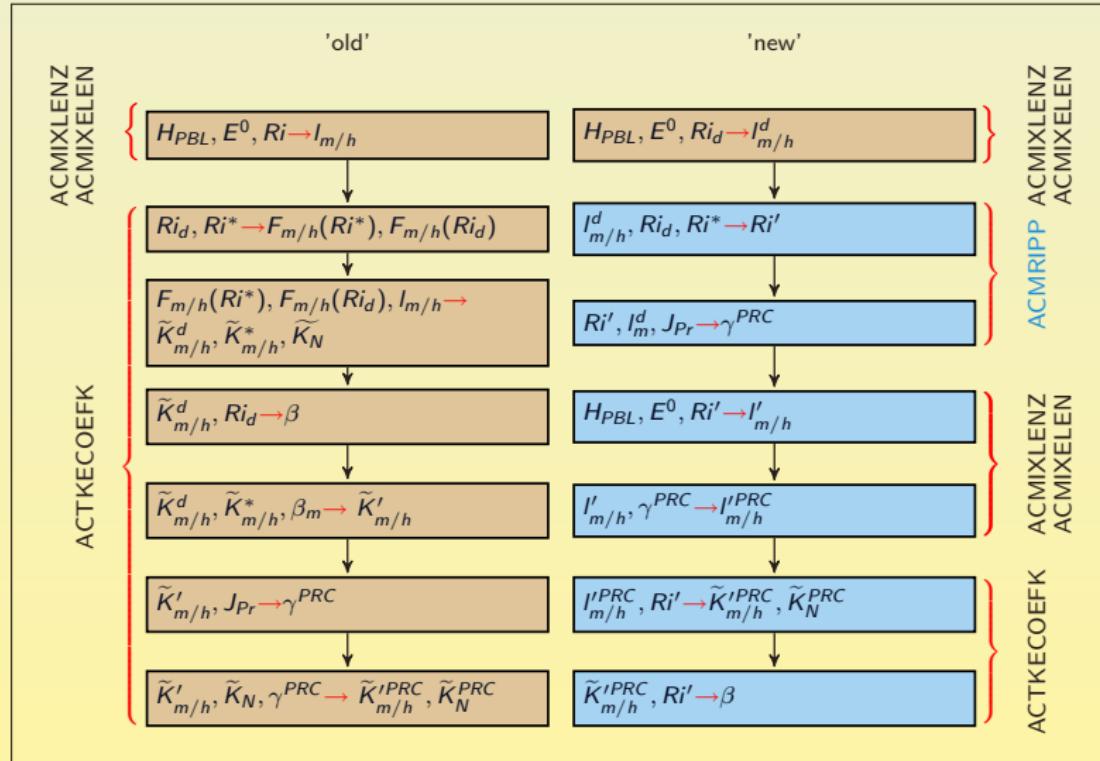
Mixing lengths

New 'moist' AF scheme (with Ri') and moist gustiness par. influence mixing lengths $I_{m/h}$, but $I_{m/h}$ are also inputs for them.

To avoid iterative methods we simply use I_m^d (without 'moist' AF scheme and 'moist' gustiness) in both schemes.







Shallow convection cloudiness

Ri' should be limited by:

Ri_d (no clouds in grid box) and

Ri_m (Richardson number for saturated air
- 100 % cloudiness in grid box):

$$Ri_m = g \frac{1 + \frac{L_v \cdot q_w}{R \cdot T}}{1 + \left(\frac{\frac{R_d}{R_v} \cdot L_v^2 \cdot q_w}{c_p \cdot R \cdot T^2} \right)} \left(\frac{d \ln \theta}{dz} + \frac{L_v}{c_p \cdot T} \frac{dq_w}{dz} \right) \frac{1}{\left(\frac{\partial \bar{u}}{\partial z} \right)^2 + \left(\frac{\partial \bar{v}}{\partial z} \right)^2}$$

q_w - specific moisture corresponding to wet bulb temperature

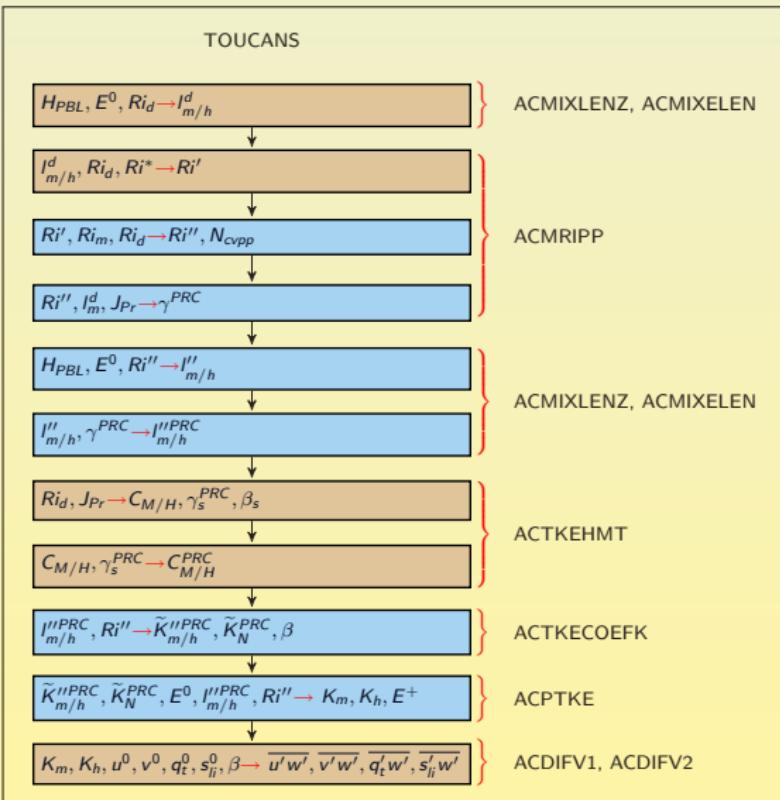
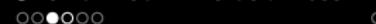
R_d - gas constant for dry air, R_v - gas constant for water vapor

Shallow convection cloudiness

Shallow convection cloudiness N_{cvpp} :

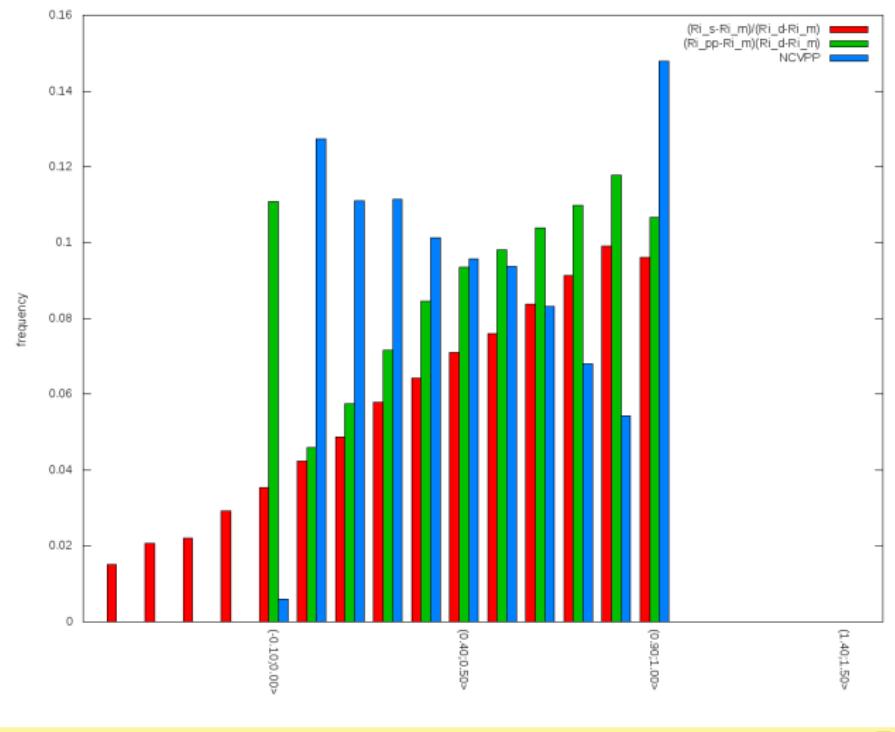
$$N_{cvpp} = \frac{Ri'' - Ri_d}{Ri_m - Ri_d}$$

$$Ri'' = \min(\max(Ri_d, Ri'), Ri_m)$$

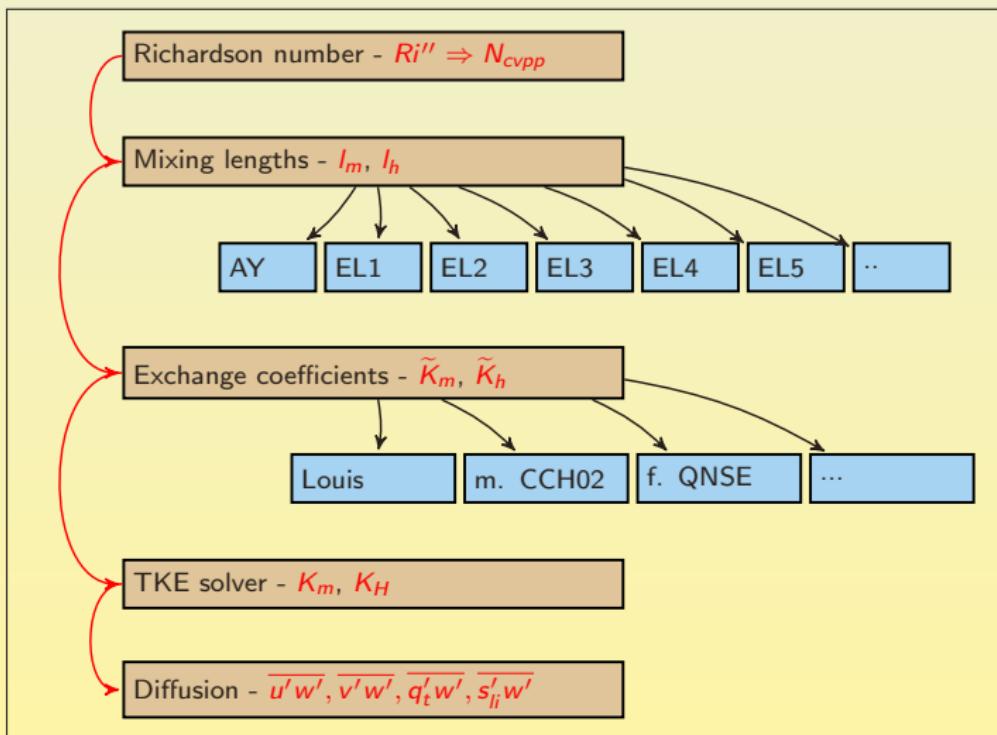


Shallow convection cloudiness distribution:

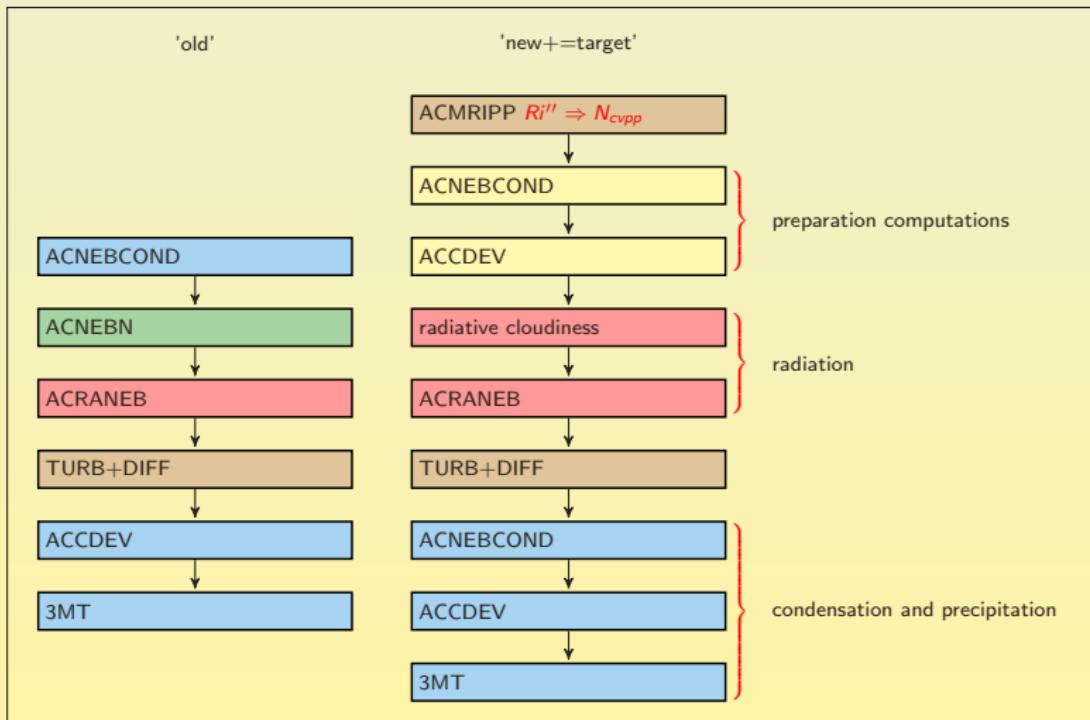
Ri differences frequency - 46086 cases with shall. conv. par.



Internal modularity



External identification



Summary

- New turbulent scheme:
 - equivalence with full TKE scheme
 - easy implementation
(new stability functions $F_{m/h}$)
 - modified TKE solver
 - modified 'dry' AF scheme
- Mixing lengths from TKE
- Preparations for TOMs:
 - modification in 'moist' AF scheme
 - modification in moist gustiness par.
- Shallow convection cloudiness
 - computation
 - used in cloudiness computations

Turbulent scheme

Mixing lengths

Preparations for TOMs

Shallow conv. cloudiness



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Thank you for your attention!