

Unsaturated downdraft in Alaro-1

Luc Gerard

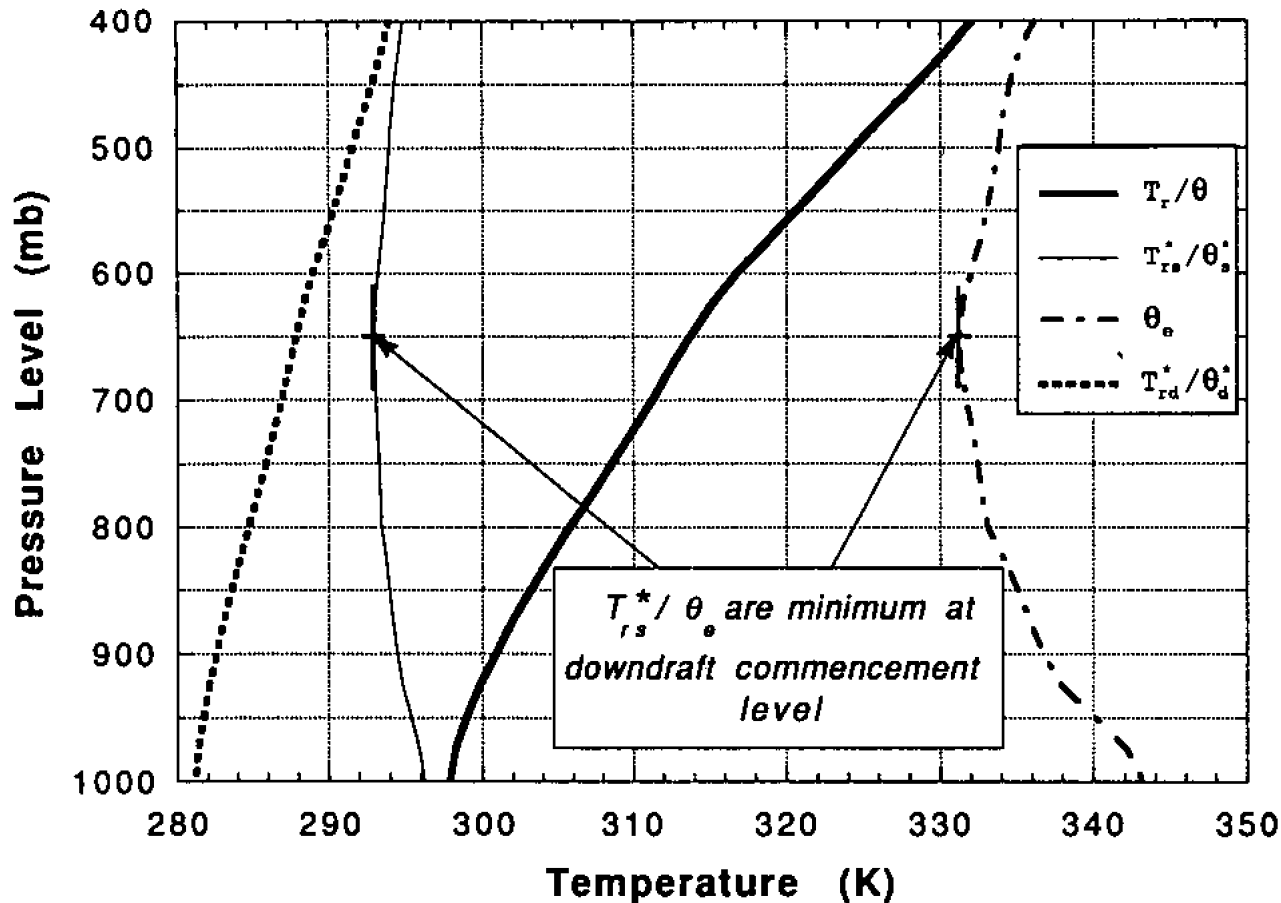
13 June 2012

Which downdraft

Knupp & Cotton 1985:

- Penetrative downdraft (non precipitating convection, width $< 1\text{km}$, depth $\sim 500\text{m}$ to 5km , $w \sim 1-15\text{ m/s}$)
- Cloud-edge downdraft (width $< 5\text{km}$, depth $\sim 1-5\text{ km}$, $w < 5\text{m/s}$)
- Overshooting downdraft (cloud top, width $\sim 500\text{m}$ to 5km , depth ~ 1 to 3km , $w \sim 1-40\text{ m/s}$)
- Precipitation-driven downdraft (Low level, width ~ 1 to 10 km , depth $\sim 1-5\text{ km}$, $w < 15$ to 20 m/s).

From where and how much ?



(GATE, time and space mean)

$$T_r = \frac{s}{c_p} = T + \frac{\phi - \phi_{\text{surf}}}{c_p}$$

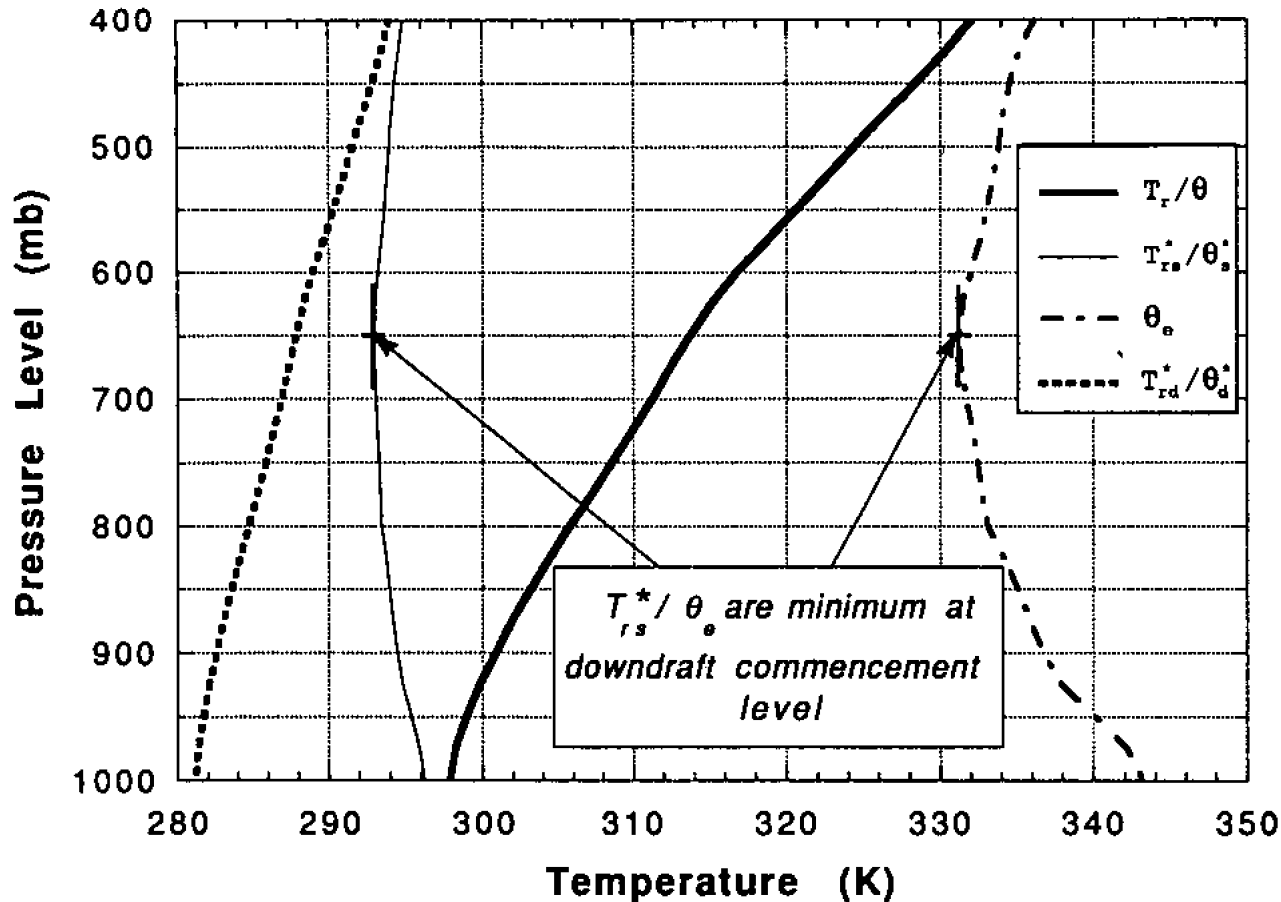
$$T_{rd}^* = T_{wd} + \frac{\phi - \phi_{\text{surf}}}{c_p}$$

(assuming dry air)

$$T_{rs}^* = T_w + \frac{\phi - \phi_{\text{surf}}}{c_p}$$

Sud and Walker 1993:
level of minimum θ_e close to 650hPa.

From where and how much ?



(GATE, time and space mean)

$$T_r = \frac{s}{c_p} = T + \frac{\phi - \phi_{\text{surf}}}{c_p}$$

$$T_{rd}^* = T_{wd} + \frac{\phi - \phi_{\text{surf}}}{c_p}$$

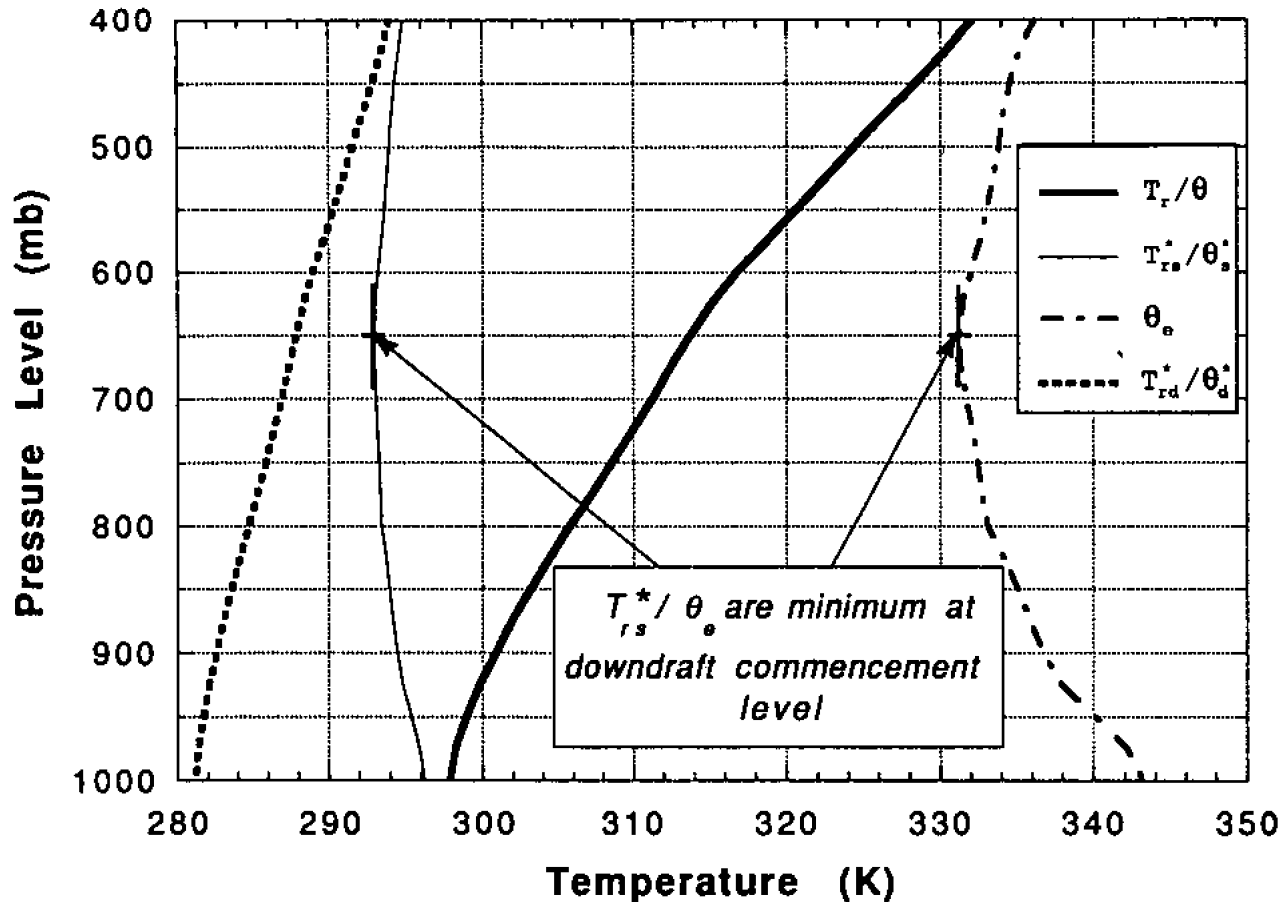
(assuming dry air)

$$T_{rs}^* = T_w + \frac{\phi - \phi_{\text{surf}}}{c_p}$$

- no dd in dry stable envt

Sud and Walker 1993:
level of minimum θ_e close to 650hPa.

From where and how much ?



(GATE, time and space mean)

$$T_r = \frac{s}{c_p} = T + \frac{\phi - \phi_{\text{surf}}}{c_p}$$

$$T_{rd}^* = T_{wd} + \frac{\phi - \phi_{\text{surf}}}{c_p}$$

(assuming dry air)

$$T_{rs}^* = T_w + \frac{\phi - \phi_{\text{surf}}}{c_p}$$

- no dd in dry stable envt
- higher moisture below helps to produce negative buoyancy in dd

Sud and Walker 1993:
level of minimum θ_e close to 650hPa.

Subsaturation

Downdraft are usually appreciably subsaturated:

1. transport of condensate to be entrained and evaporated by the downdraft → dependency to number/size of droplets or drops (especially in penetrative downdrafts)
2. cooling rate (evap + melting) < adiabatic warming rate.
Balance:
 - negative buoyancy increases downwards velocity
 - greater velocity
 - reduces residence time
 - increases the adiabatic warming rate

Precipitation-driven downdraft parametrization

Betts and Silva Dias 1979

ψ_d follows a path of constant θ_e while remaining unsaturated.

$$\frac{dq_d}{dp} = \frac{q_w - q_d}{\Pi_E} + \frac{q_e - q_d}{\mathcal{L}_e}, \quad \Pi_e = \frac{\rho g w_d}{4\pi D F}, \quad \frac{1}{\mathcal{L}_e} = \frac{1}{M_d} \frac{dM_d}{dp} \Big|_e = \frac{\lambda_d d\phi}{dp}$$

Precipitation-driven downdraft parametrization

Betts and Silva Dias 1979

ψ_d follows a path of constant θ_e while remaining unsaturated.

$$\frac{dq_d}{dp} = \frac{q_w - q_d}{\Pi_E} + \frac{q_e - q_d}{\mathcal{L}_e}, \quad \Pi_e = \frac{\rho g w_d}{4\pi D F}, \quad \frac{1}{\mathcal{L}_e} = \frac{1}{M_d} \frac{dM_d}{dp} \Big|_e = \frac{\lambda_d d\phi}{dp}$$

Diffusion coefficient $D(T_w, p) \approx 2.E - 5m^2s^{-1}$

$$F = \int_0^{\infty} n(r) C_v(r) r dr, \quad n(r) = n_0 (2r)^\mu \exp(-2b\mathcal{P}^{-\beta} r)$$

$$C_v(r) = 1 + cr^{3/4} \quad (\text{ventilation coefficient})$$

\mathcal{P} =rainfall rate, r =droplet radius, $\mu(\text{conv|strat})$ taken ~ 0

$$F(\mathcal{P}) \approx a_1 \mathcal{P}^{e_1} + a_2 \mathcal{P}^{e_2}, \quad \frac{2\Pi_E}{[l-1 \rightarrow l]} \approx \frac{\alpha}{\mathcal{P}^{3/4} \Delta p} \widetilde{\omega}_d \Delta p = k^{\overline{l-1}} \widetilde{\omega}^{\overline{l-1}} \Delta p^{\overline{l-1}}$$

Downdraft properties

$$q_d^l = \frac{q_d^{l-1} + (q_w^{l-1} - q_d^{l-1} + q_w^l) \frac{\Delta p^{\overline{l-1}}}{2\Pi_E} + (q_e^{l-1} - q_d^{l-1} + q_e^l) \frac{\xi^{\overline{l-1}}}{2}}{1 + \frac{\Delta p^{\overline{l-1}}}{2\Pi_E} + \frac{\xi^{\overline{l-1}}}{2}} = \frac{m \widetilde{\omega}_d + n}{c' \widetilde{\omega}_d + 1}$$

$$T_d^l = \dots = \frac{a' \widetilde{\omega}_d + b'}{c' \widetilde{\omega}_d + 1}$$

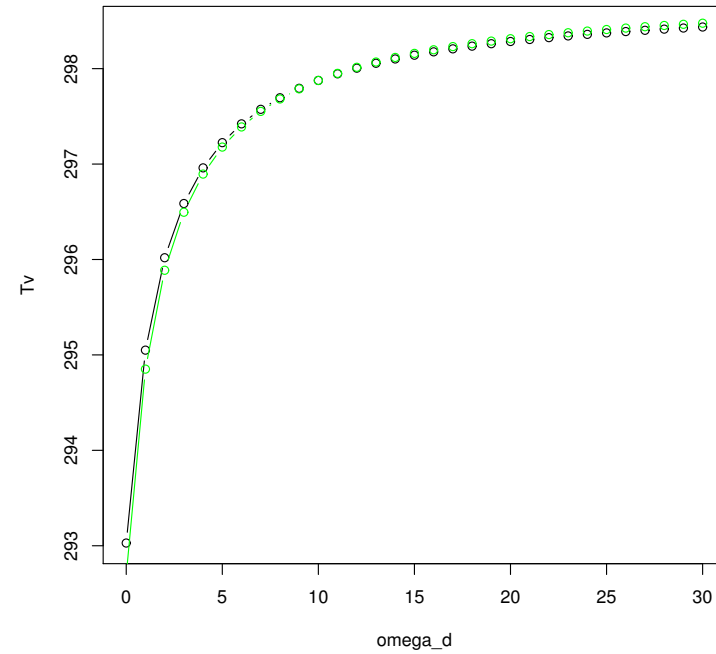
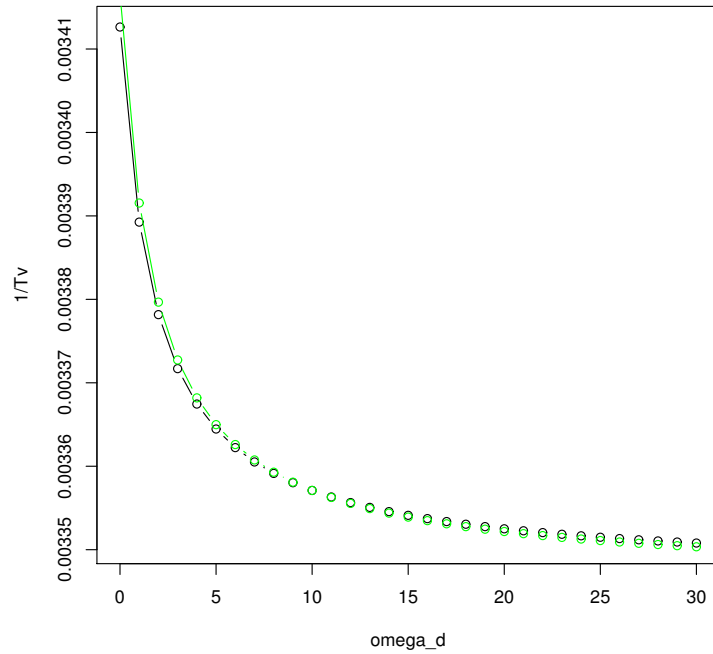
Downdraft properties

$$q_d^l = \frac{q_d^{l-1} + (q_w^{l-1} - q_d^{l-1} + q_w^l) \frac{\Delta p^{\overline{l-1}}}{2\Pi_E} + (q_e^{l-1} - q_d^{l-1} + q_e^l) \frac{\xi^{\overline{l-1}}}{2}}{1 + \frac{\Delta p^{\overline{l-1}}}{2\Pi_E} + \frac{\xi^{\overline{l-1}}}{2}} = \frac{m \widetilde{\omega}_d + n}{c' \widetilde{\omega}_d + 1}$$

$$T_d^l = \dots = \frac{a' \widetilde{\omega}_d + b'}{c' \widetilde{\omega}_d + 1}$$

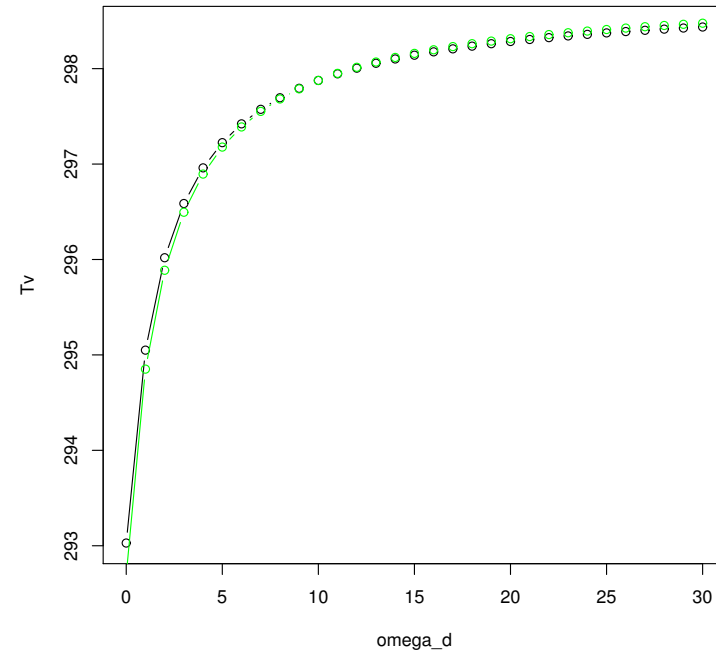
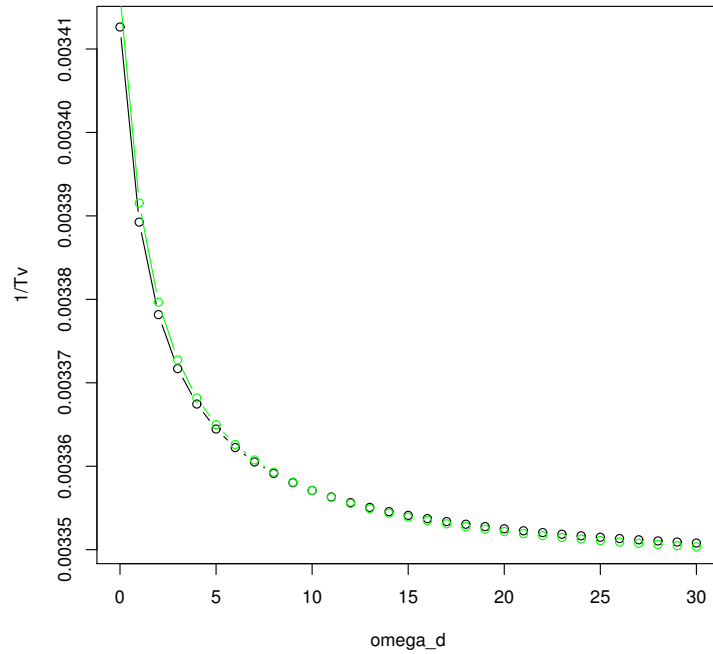
$$\frac{1}{T_{vd}} \approx \frac{1}{T_d(1 + \nu q_d)} \approx \frac{(c' \widetilde{\omega}_d + 1)}{(a' \widetilde{\omega}_d + b')} \cdot \left\{ \frac{(c' \widetilde{\omega}_{d0} + 1)}{[(c' + \nu m) \widetilde{\omega}_{d0} + (1 + \nu n)]} \right\}$$

Downdraft properties



$$\frac{1}{T_{vd}} \approx \frac{1}{T_d(1 + \nu q_d)} \approx \frac{(c' \bar{\omega}_d + 1)}{(a' \bar{\omega}_d + b')} \cdot \left\{ \frac{(c' \bar{\omega}_{d0} + 1)}{[(c' + \nu m) \bar{\omega}_{d0} + (1 + \nu n)]} \right\}$$

Downdraft properties



$$\frac{1}{T_{vd}} \approx \frac{1}{T_d(1 + \nu q_d)} \approx \frac{(c' \widetilde{\omega}_d + 1)}{(a' \widetilde{\omega}_d + b')} \cdot \left\{ \frac{(c' \widetilde{\omega}_{d0} + 1)}{[(c' + \nu m) \widetilde{\omega}_{d0} + (1 + \nu n)]} \right\}$$

$$\approx \frac{(c \widetilde{\omega}_d + d)}{(a \widetilde{\omega}_d + b)}$$

Vertical velocity equation

$$\frac{\partial \omega_d^\diamond}{\partial t} = -D\omega_d^{\diamond 2} - \omega_d^\diamond \left(\frac{\partial \omega_d^\diamond}{\partial p} + \frac{\partial \bar{\omega}}{\partial p} \right) + \frac{g^2 p}{2R_a} \left[\frac{(c\omega_d^\diamond + d)}{(a\omega_d^\diamond + b)} - \frac{1}{\overline{T_v}} \right]$$

D : drag, \ni entrainment, friction, surface ∇p

Vertical velocity equation

$$\frac{\partial \omega_d^\diamond}{\partial t} = -D\omega_d^{\diamond 2} - \omega_d^\diamond \left(\frac{\partial \omega_d^\diamond}{\partial p} + \frac{\partial \bar{\omega}}{\partial p} \right) + \frac{g^2 p}{2R_a} \left[\frac{(c\omega_d^\diamond + d)}{(a\omega_d^\diamond + b)} - \frac{1}{\bar{T}_v} \right]$$

D : drag, \ni entrainment, friction, surface ∇p

$$\alpha(F_{n+1}^{\bar{l}-1})^3 + \beta(F_{n+1}^{\bar{l}-1})^2 + \gamma(F_{n+1}^{\bar{l}-1}) + \delta = 0, \quad F_n^{\bar{l}} = \frac{\omega_d^{\diamond l} + \omega_d^{\diamond l+1}}{2} \text{ at time } n$$

Up to 3 analytical solutions (Tartaglia-Cardano)

\Rightarrow retain the smallest non negative one.

Vertical velocity equation

$$\frac{\partial \omega_d^\diamond}{\partial t} = -D\omega_d^\diamond - \omega_d^\diamond \left(\frac{\partial \omega_d^\diamond}{\partial p} + \frac{\partial \bar{\omega}}{\partial p} \right) + \frac{g^2 p}{2R_a} \left[\frac{(c\omega_d^\diamond + d)}{(a\omega_d^\diamond + b)} - \frac{1}{\bar{T}_v} \right]$$

D : drag, \ni entrainment, friction, surface ∇p

$$\alpha(F_{n+1}^{\bar{l}-1})^3 + \beta(F_{n+1}^{\bar{l}-1})^2 + \gamma(F_{n+1}^{\bar{l}-1}) + \delta = 0, \quad F_n^{\bar{l}} = \frac{\omega_d^{\diamond l} + \omega_d^{\diamond l+1}}{2} \text{ at time } n$$

Up to 3 analytical solutions (Tartaglia-Cardano)

\Rightarrow retain the smallest non negative one.

$$D^l = \frac{1}{2(1 - \sigma_d^l)^2} \left[\frac{R_a T_{vd}^l}{p^l} \left(\underbrace{\lambda_d^l}_{\text{TENTRD}} + \frac{1}{g} \underbrace{\mathcal{K}_{dd}}_{\text{TDDFR}} \right) + \frac{\text{GDDDP}}{(p^{\bar{L}} - p^l)^{\text{GDDBETA}}} \right]$$

Descent computation

- Saturated entraining moist adiabat: mixed $\psi_b \rightarrow \psi_n$

$$T_b^{l-1} = \psi_n^{l-1} + \xi^{\overline{l-1}} (\overline{T_w}^{l-1} - T_n^{l-1})$$

- parallel computation of

$$\alpha \widetilde{\omega}_d^3 + \beta \widetilde{\omega}_d^2 + \gamma \widetilde{\omega}_d + \delta = 0, \quad q_d^l = \frac{m \widetilde{\omega}_d + n}{c' \widetilde{\omega}_d + 1}, \quad T_d^l = \frac{a' \widetilde{\omega}_d + b'}{c' \widetilde{\omega}_d + 1}$$

- Control arrival level:
 - not saturated
 - remaining precipitation
 - $k \widetilde{\omega}_d > 1.E - 12$

$$\delta q_{ev}^{\overline{l-1}} = \frac{q_w - q_d}{\Pi_e} \Delta p^{\overline{l-1}}$$

Closure: mesh fraction

Süd & Walker 1993: allocate $1/3$ of total rain evaporation to downdraft cores:

Closure: mesh fraction

Süd & Walker 1993: allocate $1/3$ of total rain evaporation to downdraft cores:

- rain evaporation efficiency η depends on mean mass M , N_0 (number), residence time $\Delta t = \Delta z/w$;
- M related to precipitation rate $R_i(N_0, M, z) = \frac{\overline{R}I_d}{f_c}$ (Kessler),
 I_d = rain intensity distribution function under a convective cloud cover f_c ,
 \overline{R} = average convective rainfall in the grid cell.

Closure: mesh fraction

Süd & Walker 1993: allocate 1/3 of total rain evaporation to downdraft cores:

- rain evaporation efficiency η depends on mean mass M , N_0 (number), residence time $\Delta t = \Delta z/w$;
- M related to precipitation rate $R_i(N_0, M, z) = \frac{\bar{R}I_d}{f_c}$ (Kessler),
 I_d = rain intensity distribution function under a convective cloud cover f_c ,
 \bar{R} = average convective rainfall in the grid cell.

α_i	0.52	0.34	0.09	0.04	0.01
I_d	0	0.40	2.6	11.25	18
%	0	23.6	23.4	45	18

(Ruprecht & Gray 1976)

Closure: mesh fraction

Süd & Walker 1993: allocate $1/3$ of total rain evaporation to downdraft cores:

- rain evaporation efficiency η depends on mean mass M , N_0 (number), residence time $\Delta t = \Delta z/w$;
- M related to precipitation rate $R_i(N_0, M, z) = \frac{\bar{R}I_d}{f_c}$ (Kessler),
 I_d = rain intensity distribution function under a convective cloud cover f_c ,
 \bar{R} = average convective rainfall in the grid cell.

α_i	0.52	0.34	0.09	0.04	0.01
I_d	0	0.40	2.6	11.25	18
%	0	23.6	23.4	45	18

(Ruprecht & Gray 1976)

Simplified approach: assume downdraft covers $1/3$ of precipitating area: $\sigma_d = \frac{1}{3}\sigma_P$
 with σ_P estimated from the maximum of cloud fraction along the vertical.

Closure: mesh fraction

Süd & Walker 1993: allocate $1/3$ of total rain evaporation to downdraft cores:

- rain evaporation efficiency η depends on mean mass M , N_0 (number), residence time $\Delta t = \Delta z/w$;
- M related to precipitation rate $R_i(N_0, M, z) = \frac{\bar{R}I_d}{f_c}$ (Kessler),
 I_d = rain intensity distribution function under a convective cloud cover f_c ,
 \bar{R} = average convective rainfall in the grid cell.

α_i	0.52	0.34	0.09	0.04	0.01
I_d	0	0.40	2.6	11.25	18
%	0	23.6	23.4	45	18

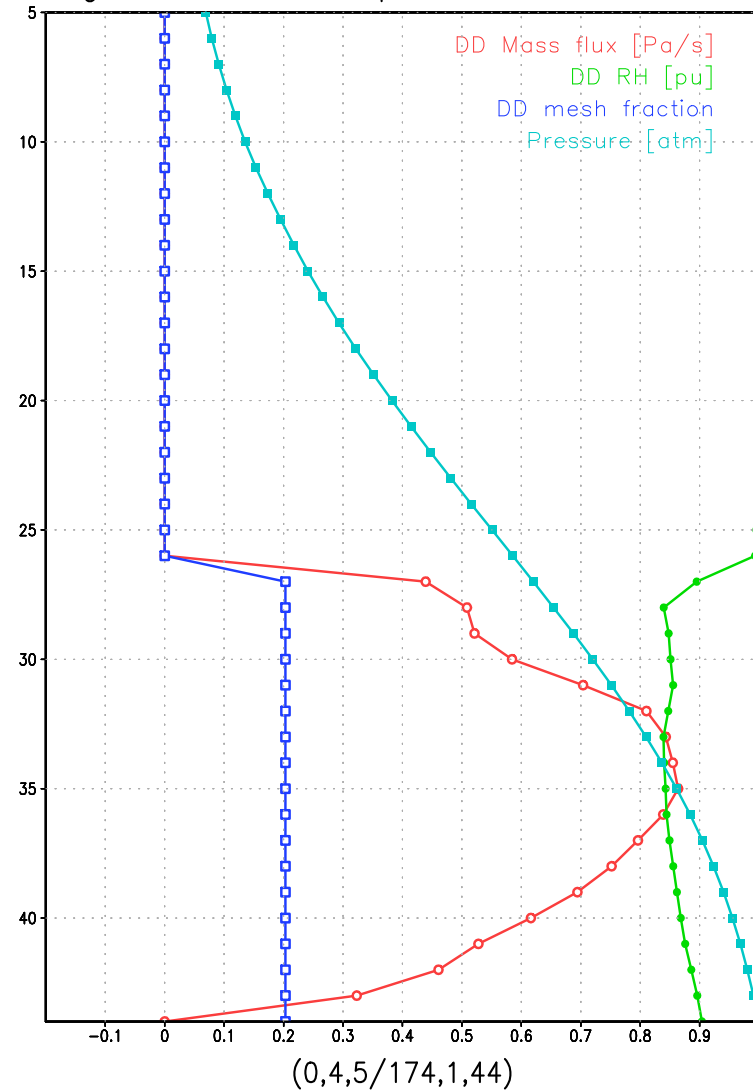
(Ruprecht & Gray 1976)

Simplified approach: assume downdraft covers $1/3$ of precipitating area: $\sigma_d = \frac{1}{3}\sigma_P$
 with σ_P estimated from the maximum of cloud fraction along the vertical.

maybe σ_P presently quite crudely estimated

1-D model profiles

Toga 1D Downdraft profile, +6h24, dt=36s



Downdraft effect on updraft closure

CAPE closure: express a relaxation of CAPE under the effect of convective activity...

$$\frac{\partial \text{CAPE}}{\partial t} = -\frac{\text{CAPE}}{\tau}$$

Downdraft effect on updraft closure

CAPE closure: express a relaxation of CAPE under the effect of convective activity...

$$\frac{\partial \text{CAPE}}{\partial t} = -\frac{\text{CAPE}}{\tau}$$

CAPE is affected by

- resolved and subgrid convergence
- resolved and subgrid precipitation
- radiative transfers
- deep convective updraft
- boundary layer transfers
- downdraft
- ...

Downdraft effect on updraft closure

CAPE closure: express a relaxation of CAPE under the effect of convective activity...

$$\frac{\partial \text{CAPE}}{\partial t} = -\frac{\text{CAPE}}{\tau}$$

My vision: the relaxation time τ is related to the deep convective process: it gives the rate of CAPE release *if this process was alone*.

Downdraft effect on updraft closure

CAPE closure: express a relaxation of CAPE under the effect of convective activity...

$$\frac{\partial \text{CAPE}}{\partial t} = -\frac{\text{CAPE}}{\tau}$$

My vision: the relaxation time τ is related to the deep convective process: it gives the rate of CAPE release *if this process was alone*.

In reality, convergence and other processes can bring new energy to the column, so that the phenomena last longer.

All these external processes (if represented by the model) intervene from one time step to the next anyway.

Downdraft effect on updraft closure

CAPE closure: express a relaxation of CAPE under the effect of convective activity...

$$\frac{\partial \text{CAPE}}{\partial t} = -\frac{\text{CAPE}}{\tau}$$

My vision: the relaxation time τ is related to the deep convective process: it gives the rate of CAPE release *if this process was alone*.

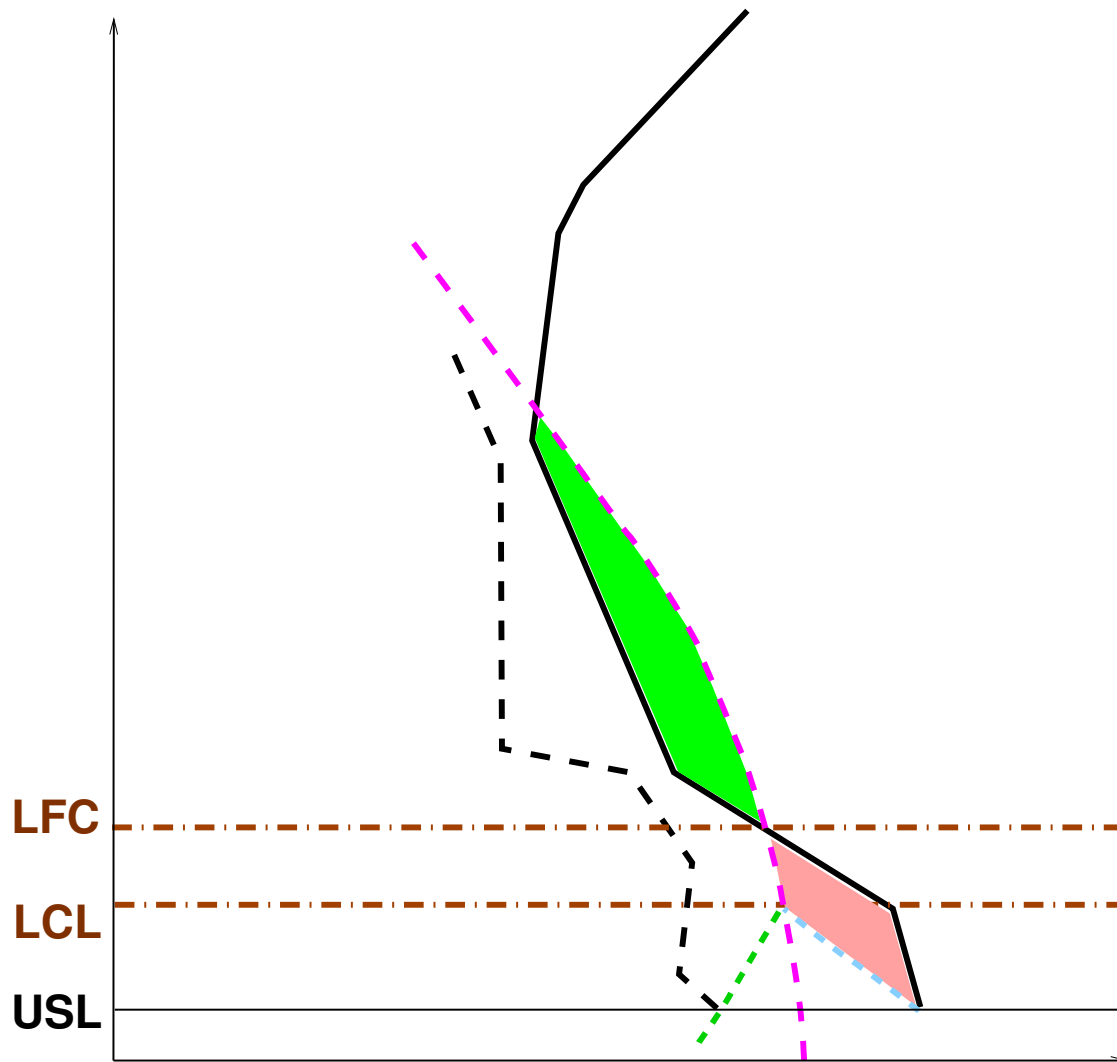
In reality, convergence and other processes can bring new energy to the column, so that the phenomena last longer.

All these external processes (if represented by the model) intervene from one time step to the next anyway.

⇒ it could be seen as a *subjective choice* to include or not the effect of downdraft on CAPE in the updraft parameterization itself.

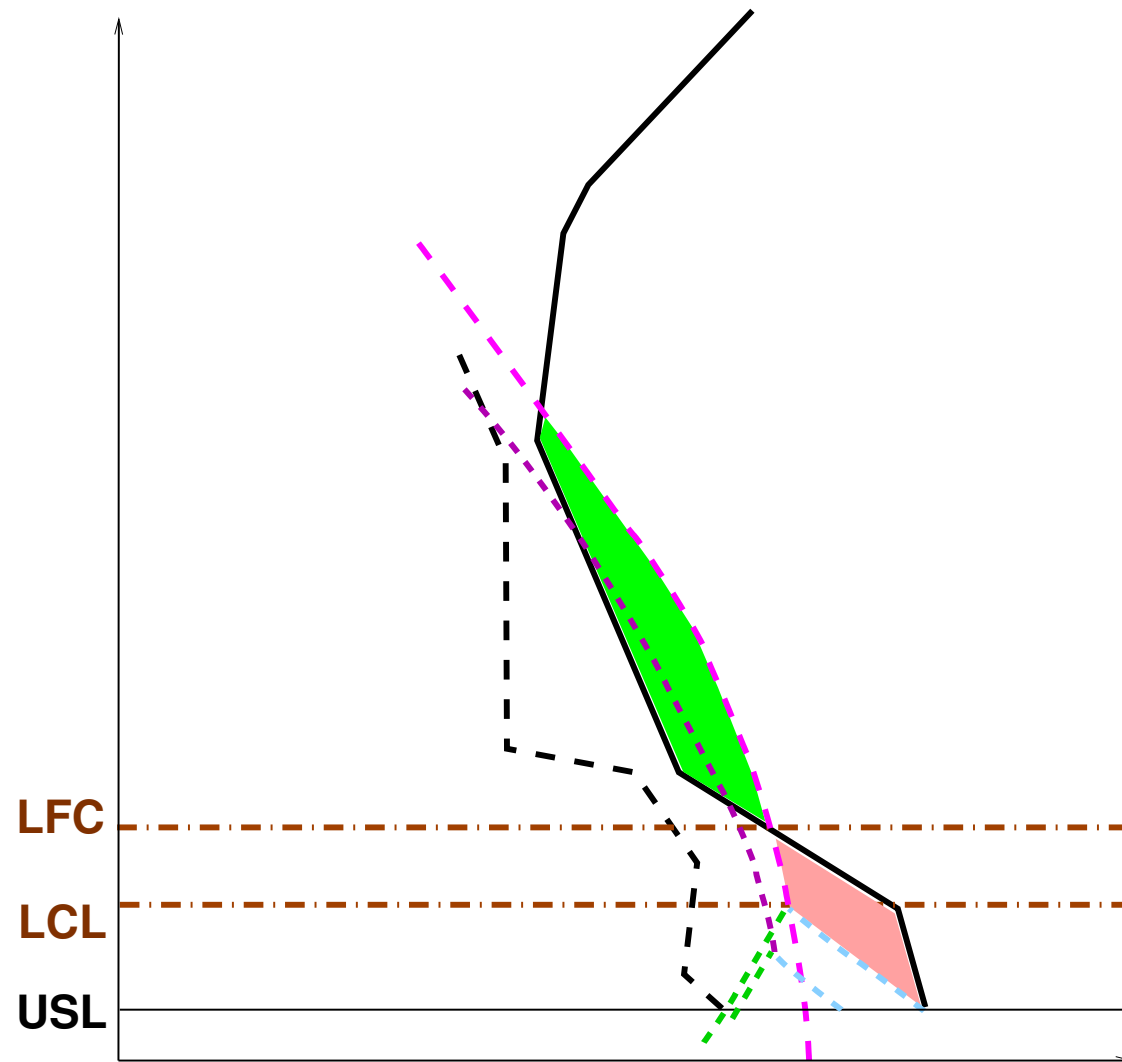
Downdraft effect on updraft closure

Main effect of downdraft is cooling and moistening USL



Downdraft effect on updraft closure

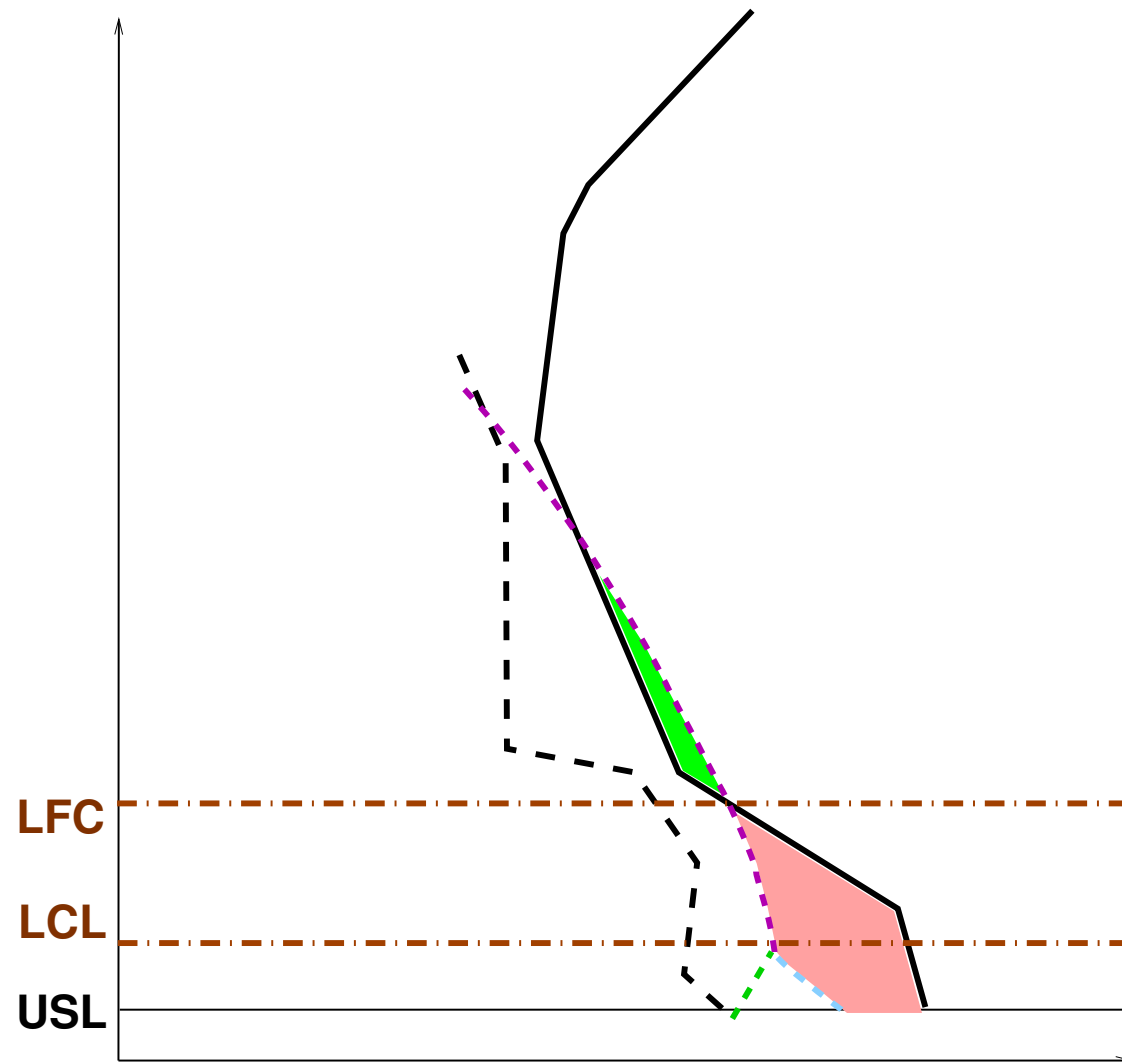
Main effect of downdraft is cooling and moistening USL



- Change LCL temperature and pressure level

Downdraft effect on updraft closure

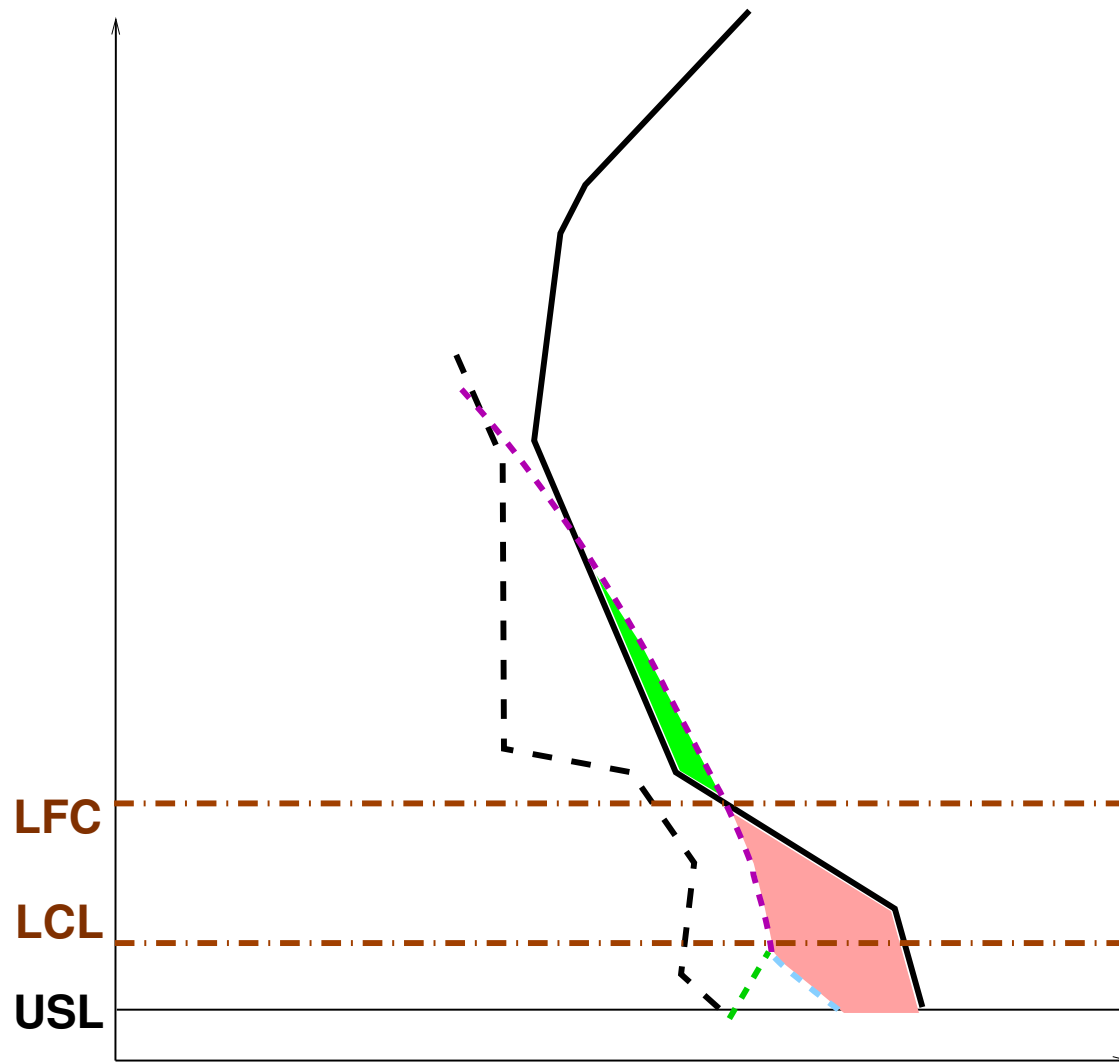
Main effect of downdraft is cooling and moistening USL



- Change LCL temperature and pressure level
- Change LFC \Rightarrow increased CIN
- Decreased CAPE

Downdraft effect on updraft closure

Main effect of downdraft is cooling and moistening USL



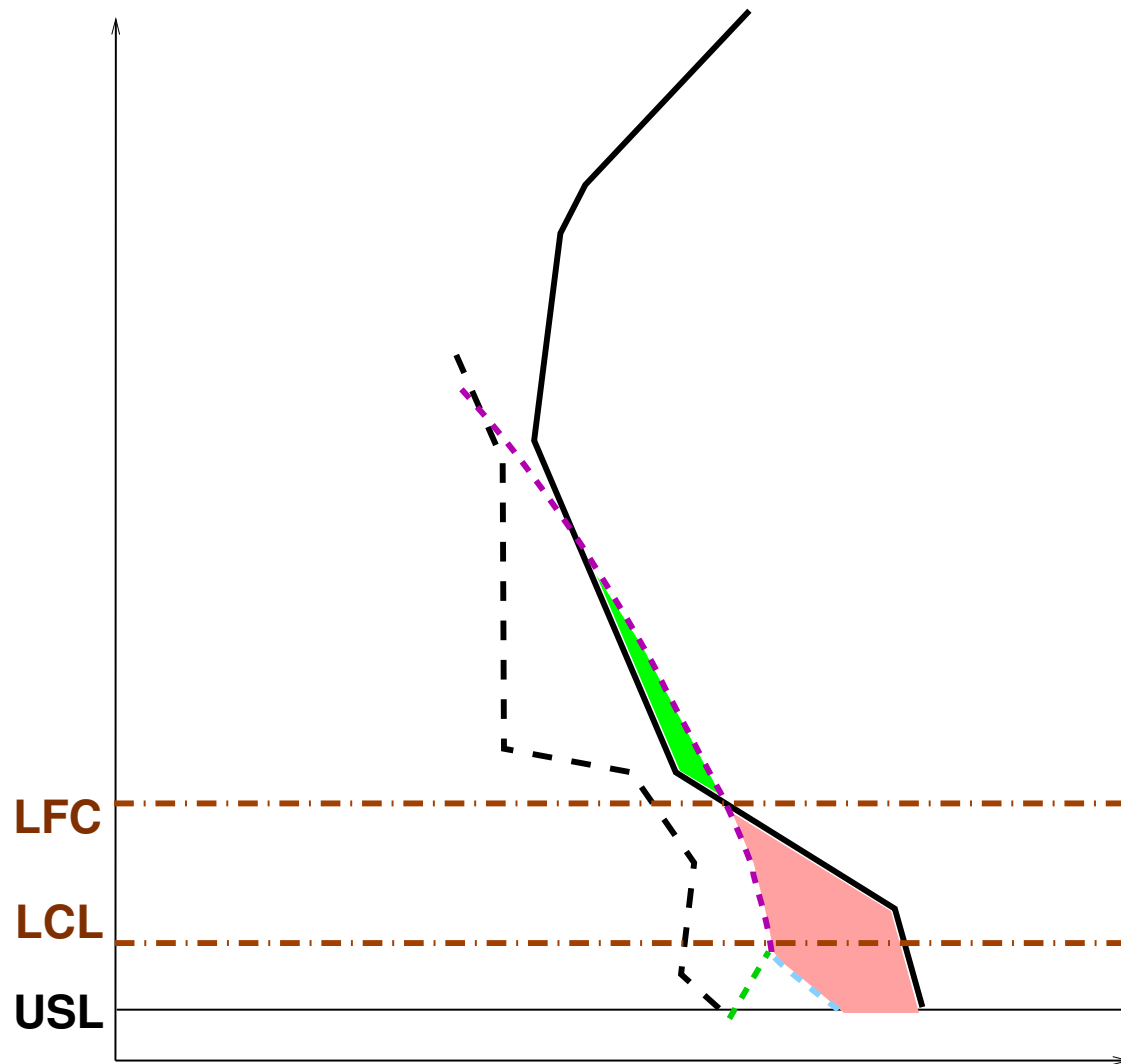
- Change LCL temperature and pressure level
- Change LFC \Rightarrow increased CIN
- Decreased CAPE

$$\int_b^t \frac{\theta_{vu} - \bar{\theta}_v}{\bar{\theta}_v} d\phi = -R_a \int_b^t (T_{vu} - \bar{T}_v) \frac{dp}{p}$$

$$\frac{\partial \text{CAPE}}{\partial t} \sim -\frac{\text{CAPE}}{\tau}$$

Downdraft effect on updraft closure

Main effect of downdraft is cooling and moistening USL



- Change LCL temperature and pressure level
- Change LFC \Rightarrow increased CIN
- Decreased CAPE

$$\int_b^t \frac{\theta_{vu} - \bar{\theta}_v}{\bar{\theta}_v} d\phi = -R_a \int_b^t (T_{vu} - \bar{T}_v) \frac{dp}{p}$$

$$\frac{\partial \text{CAPE}}{\partial t} \sim -\frac{\text{CAPE}}{\tau}$$

$$\left. \frac{\partial \text{CAPE}}{\partial t} \right|_{dd} \approx -R_a \int_b^t \left. \frac{\partial (T_{vu} - \bar{T}_v)}{\partial t} \right|_{dd} \frac{dp}{p}$$

Downdraft effect on updraft closure

M_d^* advected from previous time step

$$\left. \frac{\partial \bar{T}^{USL}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{1}{c_p} \frac{\partial \bar{s}}{\partial p} \Delta p}{\Delta p^{mix}}, \quad \left. \frac{\partial \bar{q}^{USL}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{\partial \bar{q}}{\partial p} \Delta p}{\Delta p^{mix}}, \quad \left. \frac{\partial p^{USL}}{\partial t} \right|_{dd} \sim 0$$

Downdraft effect on updraft closure

M_d^* advected from previous time step

$$\left. \frac{\partial \bar{T}^{\text{USL}}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{1}{c_p} \frac{\partial \bar{s}}{\partial p} \Delta p}{\Delta p^{\text{mix}}}, \quad \left. \frac{\partial \bar{q}^{\text{USL}}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{\partial \bar{q}}{\partial p} \Delta p}{\Delta p^{\text{mix}}}, \quad \left. \frac{\partial p^{\text{USL}}}{\partial t} \right|_{dd} \sim 0$$

Bolton (1980)

$$T^{\text{LCL}} = \frac{2840}{3.5 \ln T^{\text{USL}} - \ln \frac{e^{\text{USL}}}{100} - 4.805} + 55., \quad e^{\text{USL}} = \frac{q^{\text{USL}}}{q^{\text{USL}} + \frac{R_a}{R_v} (1 - q^{\text{USL}})} p^{\text{USL}}$$

$$\Rightarrow \frac{\partial T^{\text{LCL}}}{\partial t} = - \frac{(T^{\text{LCL}} - 55)^2}{2840} \left[\frac{3.5}{T^{\text{USL}}} \frac{\partial T^{\text{USL}}}{\partial t} - \frac{1}{q^{\text{USL}}} \frac{\partial q^{\text{USL}}}{\partial t} \frac{R_a}{R_a + q^{\text{USL}} (R_v - R_a)} \right] < 0,$$

Downdraft effect on updraft closure

M_d^* advected from previous time step

$$\left. \frac{\partial \bar{T}^{\text{USL}}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{1}{c_p} \frac{\partial \bar{s}}{\partial p} \Delta p}{\Delta p^{\text{mix}}}, \quad \left. \frac{\partial \bar{q}^{\text{USL}}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{\partial \bar{q}}{\partial p} \Delta p}{\Delta p^{\text{mix}}}, \quad \left. \frac{\partial p^{\text{USL}}}{\partial t} \right|_{dd} \sim 0$$

Bolton (1980)

$$T^{\text{LCL}} = \frac{2840}{3.5 \ln T^{\text{USL}} - \ln \frac{e^{\text{USL}}}{100} - 4.805} + 55., \quad e^{\text{USL}} = \frac{q^{\text{USL}}}{q^{\text{USL}} + \frac{R_a}{R_v} (1 - q^{\text{USL}})} p^{\text{USL}}$$

$$\Rightarrow \frac{\partial T^{\text{LCL}}}{\partial t} = - \frac{(T^{\text{LCL}} - 55)^2}{2840} \left[\frac{3.5}{T^{\text{USL}}} \frac{\partial T^{\text{USL}}}{\partial t} - \frac{1}{q^{\text{USL}}} \frac{\partial q^{\text{USL}}}{\partial t} \frac{R_a}{R_a + q^{\text{USL}} (R_v - R_a)} \right] < 0,$$

$$\frac{\partial q^{\text{LCL}}}{\partial t} \approx \frac{\partial \bar{q}^{\text{USL}}}{\partial t} > 0, \quad \frac{\partial p^{\text{LCL}}}{\partial t} = p^{\text{LCL}} \frac{c_{pa}}{R_a} \left(\frac{1}{T^{\text{LCL}}} \frac{\partial T^{\text{LCL}}}{\partial t} - \frac{1}{T^{\text{USL}}} \frac{\partial T^{\text{USL}}}{\partial t} \right)$$

Downdraft effect on updraft closure

M_d^* advected from previous time step

$$\left. \frac{\partial \bar{T}^{\text{USL}}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{1}{c_p} \frac{\partial \bar{s}}{\partial p} \Delta p}{\Delta p^{\text{mix}}}, \quad \left. \frac{\partial \bar{q}^{\text{USL}}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{\partial \bar{q}}{\partial p} \Delta p}{\Delta p^{\text{mix}}}, \quad \left. \frac{\partial p^{\text{USL}}}{\partial t} \right|_{dd} \sim 0$$

Bolton (1980)

$$T^{\text{LCL}} = \frac{2840}{3.5 \ln T^{\text{USL}} - \ln \frac{e^{\text{USL}}}{100} - 4.805} + 55., \quad e^{\text{USL}} = \frac{q^{\text{USL}}}{q^{\text{USL}} + \frac{R_a}{R_v}(1 - q^{\text{USL}})} p^{\text{USL}}$$

$$\Rightarrow \frac{\partial T^{\text{LCL}}}{\partial t} = - \frac{(T^{\text{LCL}} - 55)^2}{2840} \left[\frac{3.5}{T^{\text{USL}}} \frac{\partial T^{\text{USL}}}{\partial t} - \frac{1}{q^{\text{USL}}} \frac{\partial q^{\text{USL}}}{\partial t} \frac{R_a}{R_a + q^{\text{USL}}(R_v - R_a)} \right] < 0,$$

$$\frac{\partial q^{\text{LCL}}}{\partial t} \approx \frac{\partial \bar{q}^{\text{USL}}}{\partial t} > 0, \quad \frac{\partial p^{\text{LCL}}}{\partial t} = p^{\text{LCL}} \frac{c_{pa}}{R_a} \left(\frac{1}{T^{\text{LCL}}} \frac{\partial T^{\text{LCL}}}{\partial t} - \frac{1}{T^{\text{USL}}} \frac{\partial T^{\text{USL}}}{\partial t} \right)$$

Assume a constant $\Delta \theta_{vu}$ along the updraft

Downdraft effect on updraft closure

M_d^* advected from previous time step

$$\left. \frac{\partial \bar{T}^{\text{USL}}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{1}{c_p} \frac{\partial \bar{s}}{\partial p} \Delta p}{\Delta p^{\text{mix}}}, \quad \left. \frac{\partial \bar{q}^{\text{USL}}}{\partial t} \right|_{dd} \approx - \frac{\sum_{uslb}^{uslt} M_d^* \frac{\partial \bar{q}}{\partial p} \Delta p}{\Delta p^{\text{mix}}}, \quad \left. \frac{\partial p^{\text{USL}}}{\partial t} \right|_{dd} \sim 0$$

Bolton (1980)

$$T^{\text{LCL}} = \frac{2840}{3.5 \ln T^{\text{USL}} - \ln \frac{e^{\text{USL}}}{100} - 4.805} + 55., \quad e^{\text{USL}} = \frac{q^{\text{USL}}}{q^{\text{USL}} + \frac{R_a}{R_v}(1 - q^{\text{USL}})} p^{\text{USL}}$$

$$\Rightarrow \frac{\partial T^{\text{LCL}}}{\partial t} = - \frac{(T^{\text{LCL}} - 55)^2}{2840} \left[\frac{3.5}{T^{\text{USL}}} \frac{\partial T^{\text{USL}}}{\partial t} - \frac{1}{q^{\text{USL}}} \frac{\partial q^{\text{USL}}}{\partial t} \frac{R_a}{R_a + q^{\text{USL}}(R_v - R_a)} \right] < 0,$$

$$\frac{\partial q^{\text{LCL}}}{\partial t} \approx \frac{\partial \bar{q}^{\text{USL}}}{\partial t} > 0, \quad \frac{\partial p^{\text{LCL}}}{\partial t} = p^{\text{LCL}} \frac{c_{pa}}{R_a} \left(\frac{1}{T^{\text{LCL}}} \frac{\partial T^{\text{LCL}}}{\partial t} - \frac{1}{T^{\text{USL}}} \frac{\partial T^{\text{USL}}}{\partial t} \right)$$

Assume a constant $\Delta \theta_{vu}$ along the updraft

$$\left. \frac{\partial T_{vu} - \bar{T}_v}{\partial t} \right|_{dd} = \left. \frac{\partial T^{\text{LCL}}}{\partial t} \right|_{dd} (1 + \kappa q_u) + \left. \frac{\partial q^{\text{LCL}}}{\partial t} \right|_{dd} \kappa T_u - \frac{1}{c_p} M_d^* \frac{\partial \bar{s}}{\partial p} (1 + \kappa q_u) + M_d^* \frac{\partial \bar{q}}{\partial p} \kappa T_u$$

Current status: plug and play

- **LNSDO** allows to choose the unsaturated downdraft (acnsdo instead of acmodo), both 3MT (ω_d) and Alaro-1 (ω_d^\diamond) versions available.
- Tuning parameters:
 - **gddevf** : σ_d/σ_P (0.33)
 - **tentr** : entrainment rate (1.E-4), **tddfr** : drag (6.E-4, def)
 - **gddb**=5., **gddd** =8.E15 : braking applied to ω_d towards the surface.
 - **lcddev**=F, **jddev**=1 (in acupm: update input profile with total evaporation)

Current status: plug and play

- **LNSDO** allows to choose the unsaturated downdraft (acnsdo instead of acmodo), both 3MT (ω_d) and Alaro-1 (ω_d^\diamond) versions available.
- Tuning parameters:
 - **gddevf** : $\sigma_d/\sigma_{\mathcal{P}}$ (0.33)
 - **tentr** : entrainment rate (1.E-4), **tddfr** : drag (6.E-4, def)
 - **gddb**=5., **gddd** =8.E15 : braking applied to ω_d towards the surface.
 - **lcddevpro**=F, **jddevpro**=1 (in acupm: update input profile with total evaporation)
- Profiles are realistic, further tuning should be based on model scores.
- Possible re-tuning of hard-coded constants.
- Further refinements: better estimation of $\sigma_{\mathcal{P}}$