

Unsaturated downdraught in Alaro-1

Luc Gerard and Doina Banciu

13 May 2014



Which downdraught

Knupp & Cotton 1985:

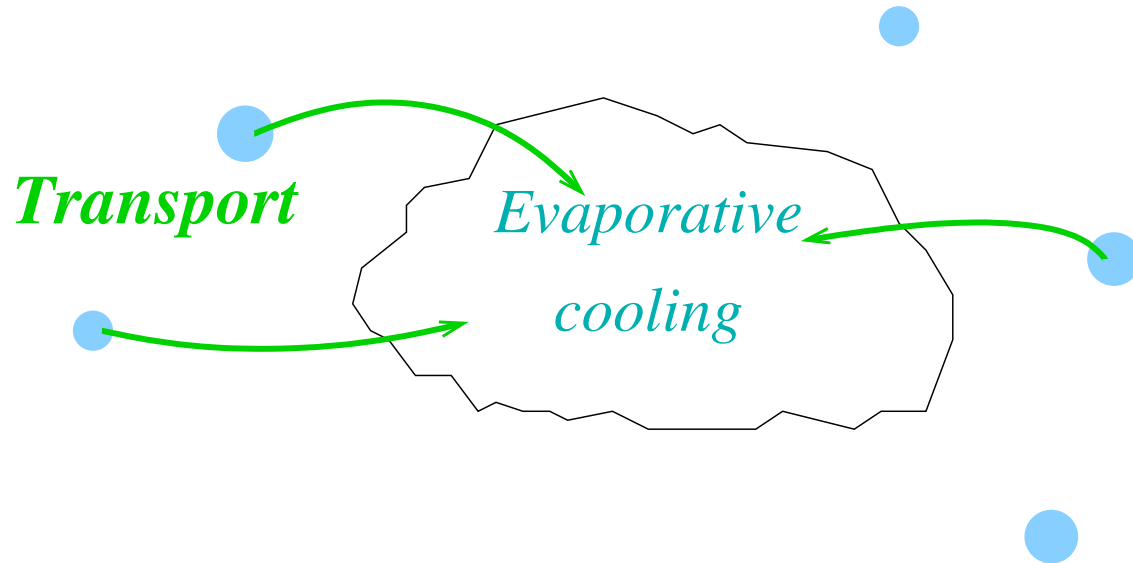
- Penetrative downdraught (non precipitating convection, width $< 1\text{km}$, depth $\sim 500\text{m}$ to 5km , $w \sim 1-15\text{ m/s}$)
- Cloud-edge downdraught (width $< 5\text{km}$, depth $\sim 1-5\text{ km}$, $w < 5\text{m/s}$)
- Overshooting downdraught (cloud top, width $\sim 500\text{m}$ to 5km , depth ~ 1 to 3km , $w \sim 1-40\text{ m/s}$)
- Precipitation-driven downdraught (Low level, width ~ 1 to 10 km , depth $\sim 1-5\text{ km}$, $w < 15$ to 20 m/s).

Subsaturation

Air parcel in precipitation: Evaporation of condensate

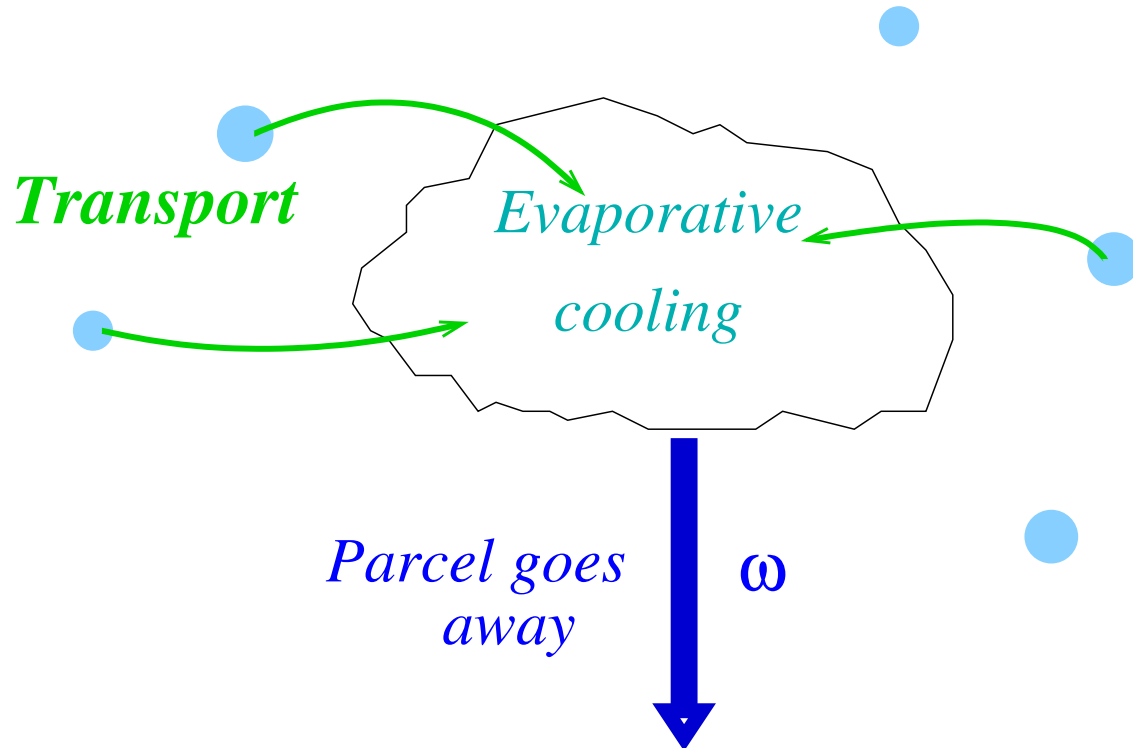
Subsaturation

Air parcel in precipitation: Evaporation of condensate



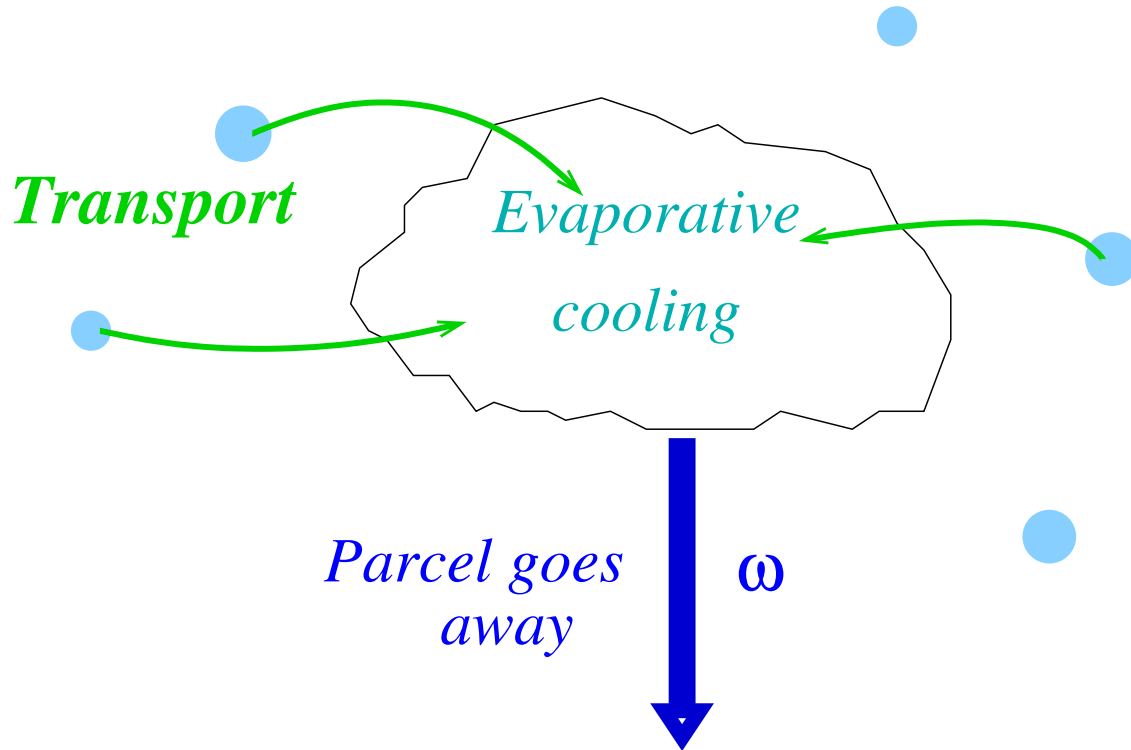
Subsaturation

Air parcel in precipitation: Evaporation of condensate



Subsaturation

Air parcel in precipitation: Evaporation of condensate

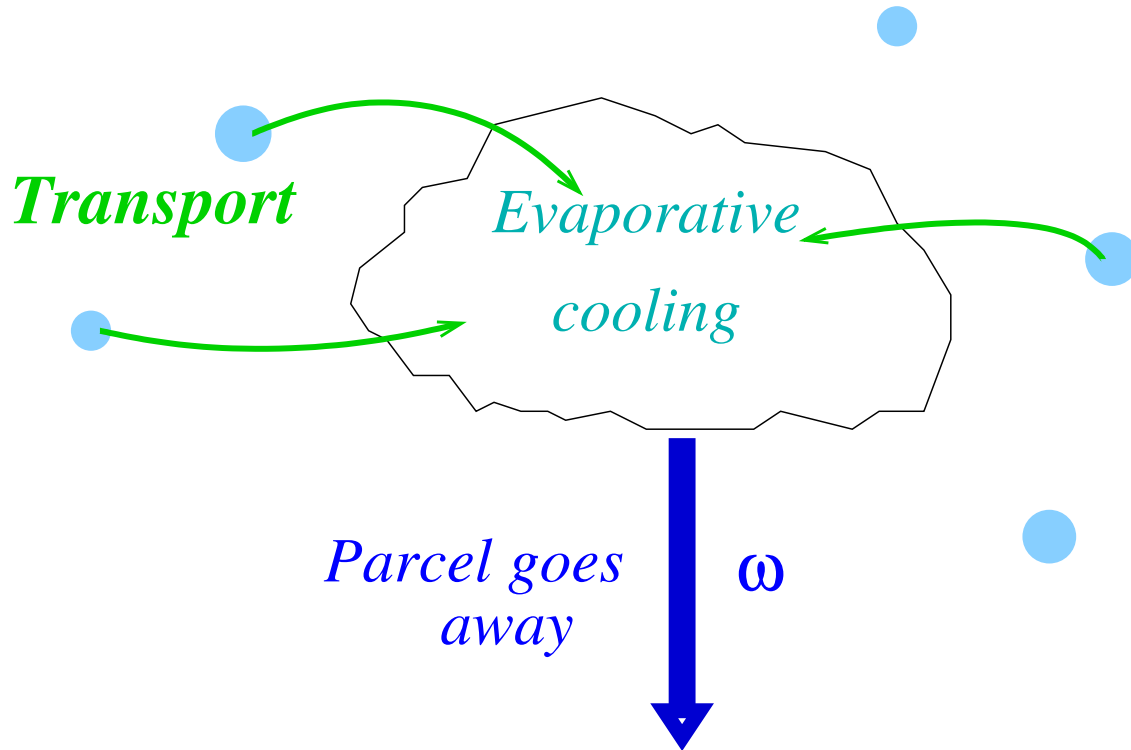


Evaporative cooling

- increases ω_d
- reduced by $\omega_d >$

Subsaturation

Air parcel in precipitation: Evaporation of condensate



Evaporative cooling

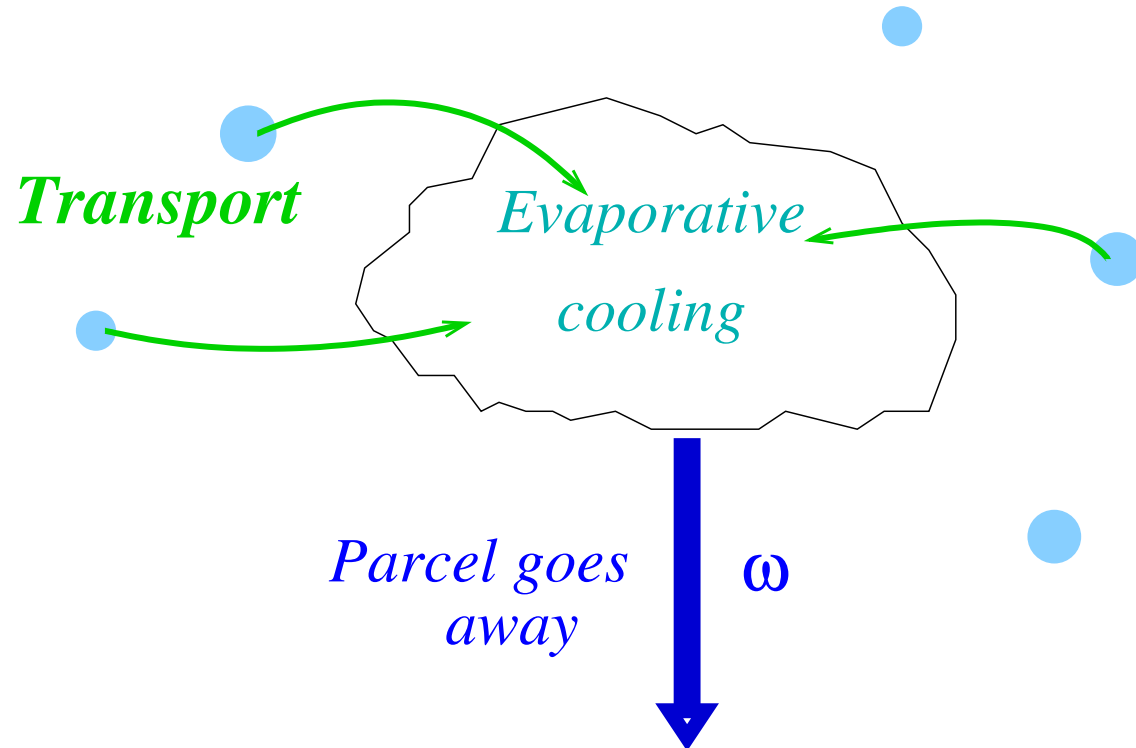
- increases ω_d
- reduced by $\omega_d >$

Adiabatic heating rate

- increased by $\omega_d >$
- reduces ω_d
- increases q_{sat}

Subsaturation

Air parcel in precipitation: Evaporation of condensate



Evaporative cooling

- increases ω_d
- reduced by $\omega_d >$

Adiabatic heating rate

- increased by $\omega_d >$
- reduces ω_d
- increases q_{sat}

The downdraught buoyancy results from a balance between **evaporative cooling** limited by ω_d and **adiabatic heating** increased by ω_d . Saturation requires the parcel to move very slowly ($\omega_d \sim 0$).

Precipitation-driven downdraught parametrization

Betts and Silva Dias 1979

ψ_d follows a path of constant θ_e while remaining unsaturated.

$$\frac{dq_d}{dp} = \frac{q_w - q_d}{\Pi_E} + \frac{q_e - q_d}{\mathcal{L}_e}, \quad \Pi_e = \frac{\omega_d}{\mathcal{F}(\mathcal{P})}$$

Water transfer: parameters derived from Marshall-Palmer's distribution (Kessler 1969)
+ fitting a curve :

$$\mathcal{F}(\mathcal{P}) = k_F \mathcal{P}^{\beta_F}, \quad k_F = \text{gddfp}[1] = 4.398 \cdot 10^{-2}, \quad \beta_f = \text{gddfp}[2] = 0.75$$

Precipitation-driven downdraught parametrization

Betts and Silva Dias 1979

ψ_d follows a path of constant θ_e while remaining unsaturated.

$$\frac{dq_d}{dp} = \frac{q_w - q_d}{\Pi_E} + \frac{q_e - q_d}{\mathcal{L}_e}, \quad \Pi_e = \frac{\omega_d}{\mathcal{F}(\mathcal{P})}$$

Water transfer: parameters derived from Marshall-Palmer's distribution (Kessler 1969)
+ fitting a curve :

$$\mathcal{F}(\mathcal{P}) = k_F \mathcal{P}^{\beta_F}, \quad k_F = \text{gddfp}[1] = 4.398 \cdot 10^{-2}, \quad \beta_f = \text{gddfp}[2] = 0.75$$

Mixing with environment

$$\frac{1}{\mathcal{L}_e} = \frac{1}{M_d} \left. \frac{dM_d}{dp} \right|_e = \lambda_d \frac{d\phi}{dp}, \quad \lambda_d = \text{tentrd} \quad + \text{tddfr in } \omega \text{ equation}$$

Precipitation-driven downdraught parametrization

Betts and Silva Dias 1979

ψ_d follows a path of constant θ_e while remaining unsaturated.

$$\frac{dq_d}{dp} = \frac{q_w - q_d}{\Pi_E} + \frac{q_e - q_d}{\mathcal{L}_e}, \quad \Pi_e = \frac{\omega_d}{\mathcal{F}(\mathcal{P})}$$

Water transfer: parameters derived from Marshall-Palmer's distribution (Kessler 1969)
+ fitting a curve :

$$\mathcal{F}(\mathcal{P}) = k_F \mathcal{P}^{\beta_F}, \quad k_F = \text{gddfp}[1] = 4.398 \cdot 10^{-2}, \quad \beta_f = \text{gddfp}[2] = 0.75$$

Mixing with environment

$$\frac{1}{\mathcal{L}_e} = \frac{1}{M_d} \left. \frac{dM_d}{dp} \right|_e = \lambda_d \frac{d\phi}{dp}, \quad \lambda_d = \text{tentrd} \quad + \text{tddfr in } \omega \text{ equation}$$

q_d, T_d directly affected by ω_d :

vertical motion equation must be solved at the same time as downdraught profile.

Descent computation

- start at level of minimum θ_e close to 650hPa (Sud and Walker 1993).

Descent computation

- start at level of minimum θ_e close to 650hPa (Sud and Walker 1993).
- Saturated entraining moist adiabat: mixed $\psi_b \rightarrow \psi_n$

$$T_b^{l-1} = \psi_n^{l-1} + \xi^{\overline{l-1}} (\overline{T_w}^{l-1} - T_n^{l-1})$$

Descent computation

- start at level of minimum θ_e close to 650hPa (Sud and Walker 1993).
- Saturated entraining moist adiabat: mixed $\psi_b \rightarrow \psi_n$

$$T_b^{l-1} = \psi_n^{l-1} + \xi^{\overline{l-1}} (\overline{T_w}^{l-1} - T_n^{l-1})$$

- parallel computation of

$$\alpha \widetilde{\omega}_d^3 + \beta \widetilde{\omega}_d^2 + \gamma \widetilde{\omega}_d + \delta = 0, \quad q_d^l = \frac{m \widetilde{\omega}_d + n}{c' \widetilde{\omega}_d + 1}, \quad T_d^l = \frac{a' \widetilde{\omega}_d + b'}{c' \widetilde{\omega}_d + 1}$$

Descent computation

- start at level of minimum θ_e close to 650hPa (Sud and Walker 1993).
- Saturated entraining moist adiabat: mixed $\psi_b \rightarrow \psi_n$

$$T_b^{l-1} = \psi_n^{l-1} + \xi^{\overline{l-1}} (\overline{T_w}^{l-1} - T_n^{l-1})$$

- parallel computation of

$$\alpha \widetilde{\omega}_d^3 + \beta \widetilde{\omega}_d^2 + \gamma \widetilde{\omega}_d + \delta = 0, \quad q_d^l = \frac{m \widetilde{\omega}_d + n}{c' \widetilde{\omega}_d + 1}, \quad T_d^l = \frac{a' \widetilde{\omega}_d + b'}{c' \widetilde{\omega}_d + 1}$$

- Control arrival level:
 - not saturated
 - remaining precipitation
 - $k \widetilde{\omega}_d > 1.E - 12$

$$\delta q_{ev}^{\overline{l-1}} = \frac{q_w - q_d}{\Pi_e} \Delta p^{\overline{l-1}}$$

Closure: mesh fraction

Süd & Walker 1993: allocate $1/3$ of total rain evaporation to downdraught cores:

Closure: mesh fraction

Süd & Walker 1993: allocate $1/3$ of total rain evaporation to downdraught cores:

- rain evaporation efficiency η depends on mean mass M , N_0 (number), residence time $\Delta t = \Delta z/w$;
- M related to precipitation rate $R_i(N_0, M, z) = \frac{\overline{R}I_d}{f_c}$ (Kessler),
 I_d = rain intensity distribution function under a convective cloud cover f_c ,
 \overline{R} = average convective rainfall in the grid cell.

Closure: mesh fraction

Süd & Walker 1993: allocate 1/3 of total rain evaporation to downdraught cores:

- rain evaporation efficiency η depends on mean mass M , N_0 (number), residence time $\Delta t = \Delta z/w$;
- M related to precipitation rate $R_i(N_0, M, z) = \frac{\bar{R}I_d}{f_c}$ (Kessler),
 I_d = rain intensity distribution function under a convective cloud cover f_c ,
 \bar{R} = average convective rainfall in the grid cell.

α_i	0.52	0.34	0.09	0.04	0.01
I_d	0	0.40	2.6	11.25	18
%	0	23.6	23.4	45	18

(Ruprecht & Gray 1976)

Closure: mesh fraction

Süd & Walker 1993: allocate $1/3$ of total rain evaporation to downdraught cores:

- rain evaporation efficiency η depends on mean mass M , N_0 (number), residence time $\Delta t = \Delta z/w$;
- M related to precipitation rate $R_i(N_0, M, z) = \frac{\bar{R}I_d}{f_c}$ (Kessler),
 I_d = rain intensity distribution function under a convective cloud cover f_c ,
 \bar{R} = average convective rainfall in the grid cell.

α_i	0.52	0.34	0.09	0.04	0.01
I_d	0	0.40	2.6	11.25	18
%	0	23.6	23.4	45	18

(Ruprecht & Gray 1976)

Simplified approach: assume that downdraught covers $\text{GDDFRAC} \approx 1/3$ of precipitating area: $\sigma_d = \frac{1}{3}\sigma_{\mathcal{P}}$ with $\sigma_{\mathcal{P}}$ estimated from the maximum of cloud fraction along the vertical.

Closure: mesh fraction

Süd & Walker 1993: allocate $1/3$ of total rain evaporation to downdraught cores:

- rain evaporation efficiency η depends on mean mass M , N_0 (number), residence time $\Delta t = \Delta z/w$;
- M related to precipitation rate $R_i(N_0, M, z) = \frac{\bar{R}I_d}{f_c}$ (Kessler),
 I_d = rain intensity distribution function under a convective cloud cover f_c ,
 \bar{R} = average convective rainfall in the grid cell.

α_i	0.52	0.34	0.09	0.04	0.01
I_d	0	0.40	2.6	11.25	18
%	0	23.6	23.4	45	18

(Ruprecht & Gray 1976)

Simplified approach: assume that

downdraught covers $\text{GDDFRAC} \approx 1/3$ of precipitating area: $\sigma_d = \frac{1}{3}\sigma_{\mathcal{P}}$

with $\sigma_{\mathcal{P}}$ estimated from the maximum of cloud fraction along the vertical.

maybe $\sigma_{\mathcal{P}}$ presently quite crudely estimated

High resolution: LCSD=T

- Environment vertical velocity does matter: geometrical $\omega_e \neq 0$, i.e.
 - $\omega_e < 0$: resolved part of the updraughts in the grid box
 - $\omega_e > 0$: resolved downdraught: then σ_d no longer limited to $\frac{1}{3}$.
- Representation of a complement to the resolved part of the downdraught;
- Separation of organized entrainment vs turbulent mixing;
- Accounting for mesh fraction on the estimation of downdraught vs environment properties.
- parameters:
 - $gddalbu=0.9$ buoyancy coefficient csd motion equation (instead of $tddbu \sim 0.5$);
 - $gddendymx=10^{-4}$ limitation of organized entrainment.
 - $tentrd$ represents only turbulent entrainment.

Other tunings

- braking towards the surface:

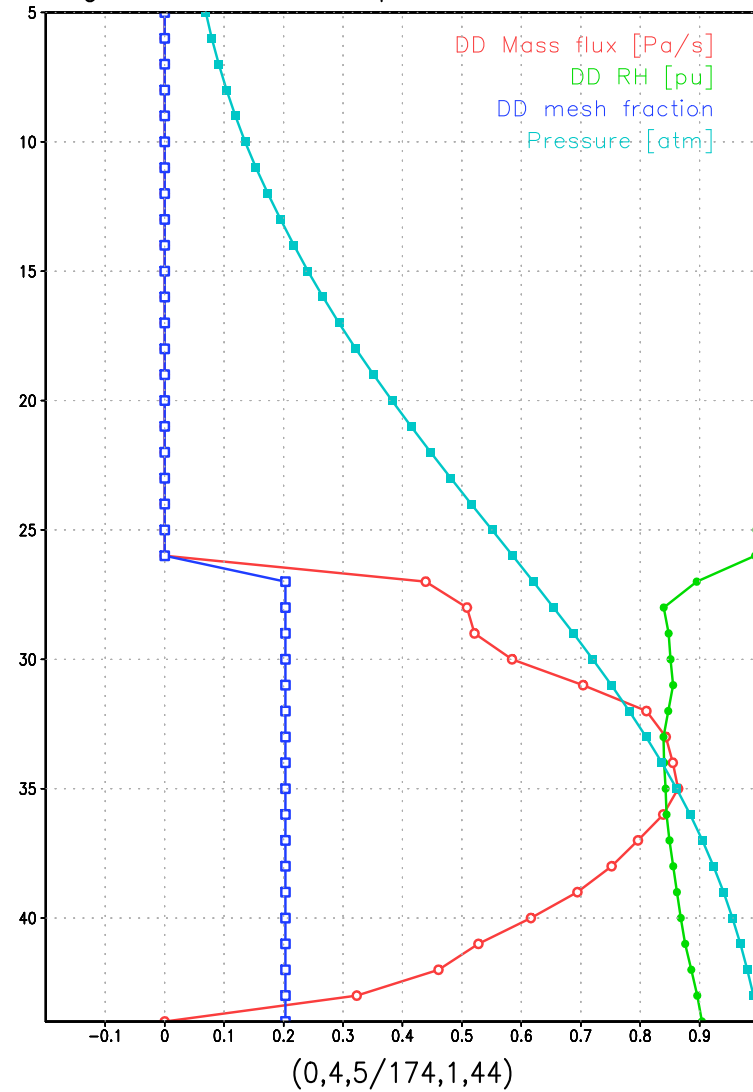
$$\frac{gddd_p}{(p^{\bar{L}} - p^l)^{gddb\beta}}$$

now $(gddb\beta, gddd_p) = (3, 8 \cdot 10^7)$ instead of $(2, 10^4)$ in acmodo.

- Fixing some other aspects: n_{eq} , wrongly interpreted the stratiform fraction in Alaro-0 – could require a re-tuning of updraught / microphysics.

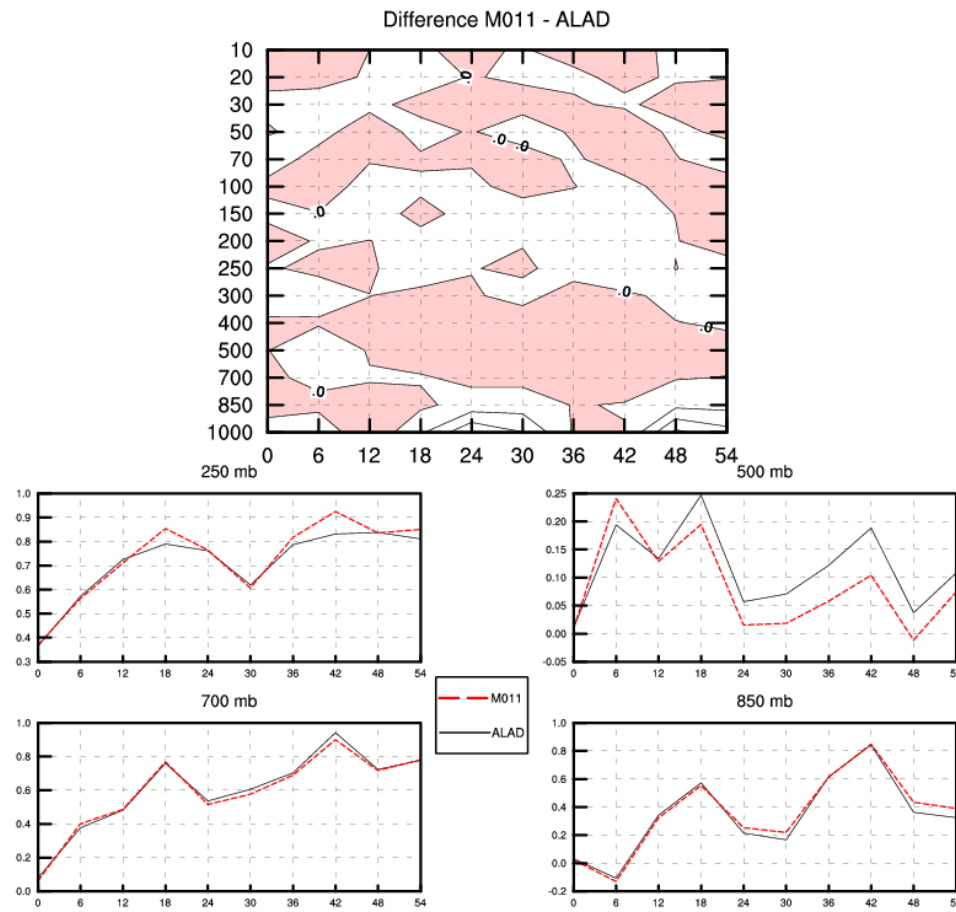
1-D model profiles

Toga 1D Downdraft profile, +6h24, dt=36s



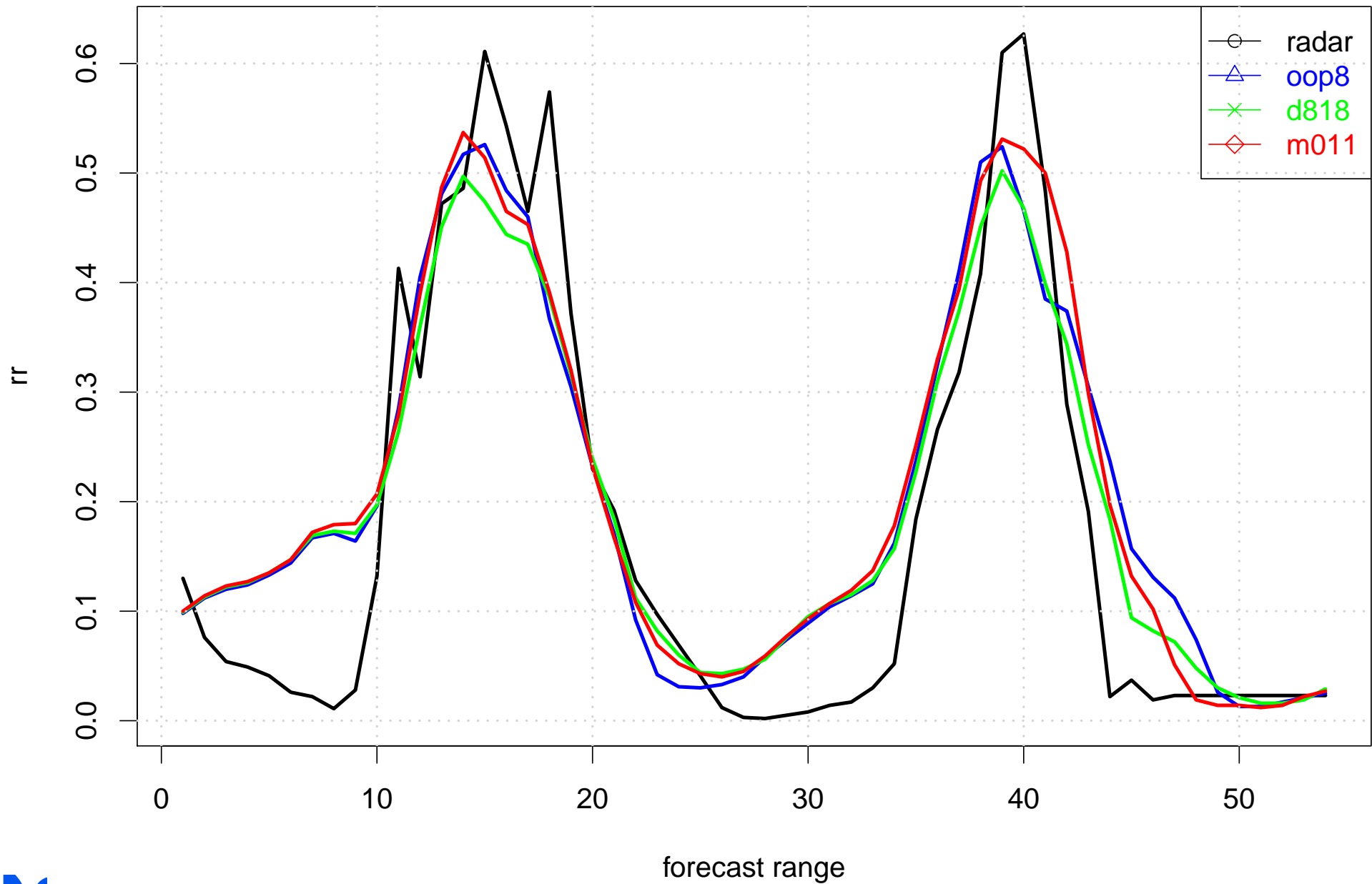
Main scores

- Scores are sometimes neutral, sometimes it appears that a new fix in n_{eq} and some other aspects may require a wider re-tuning of both microphysics and updraught.

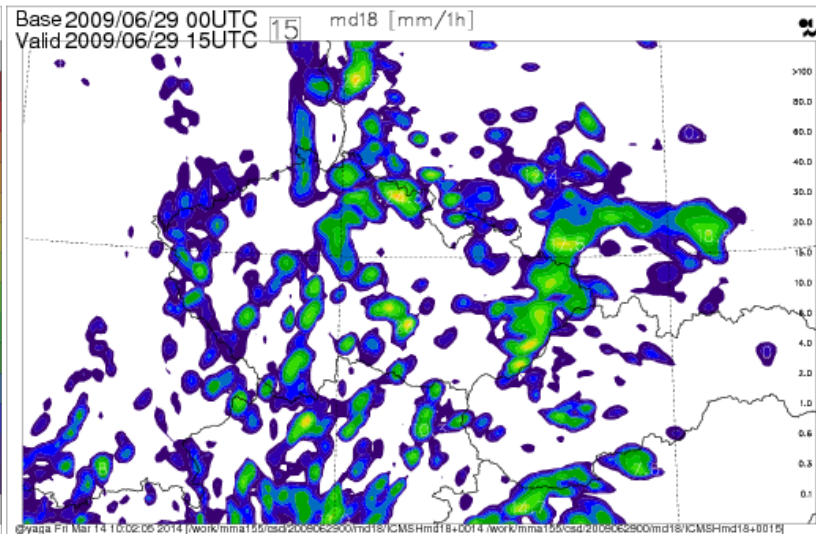
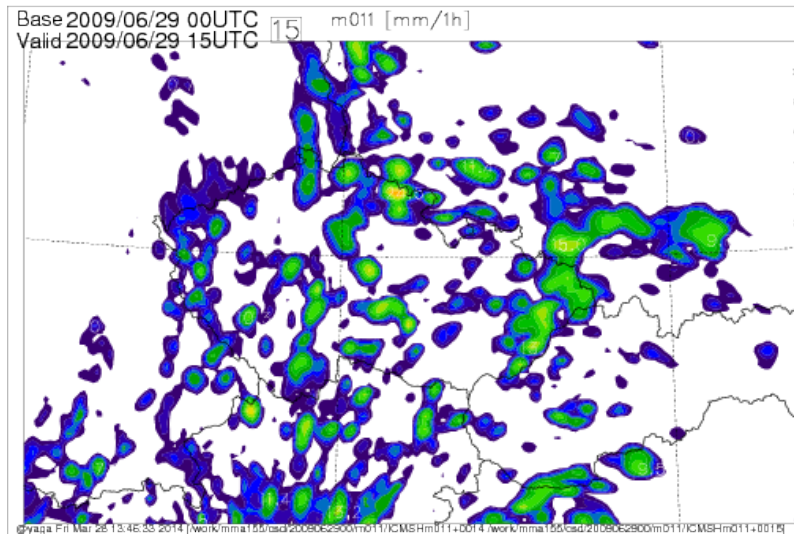
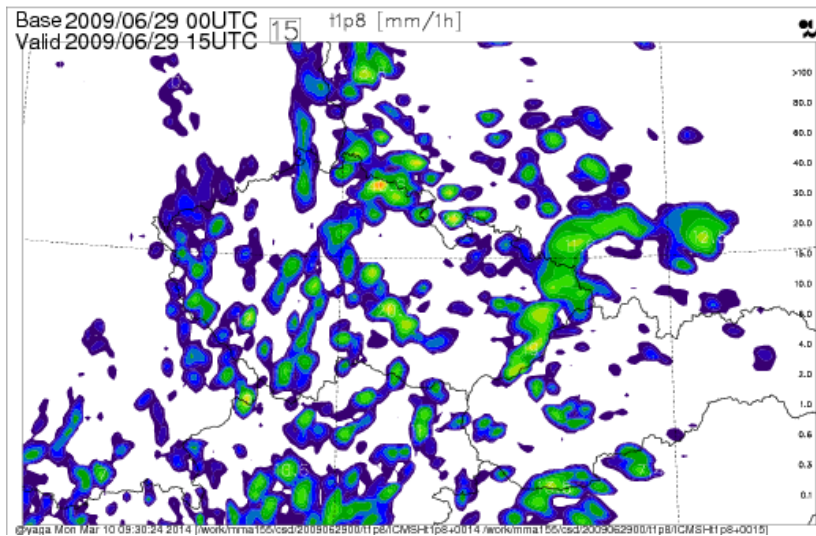
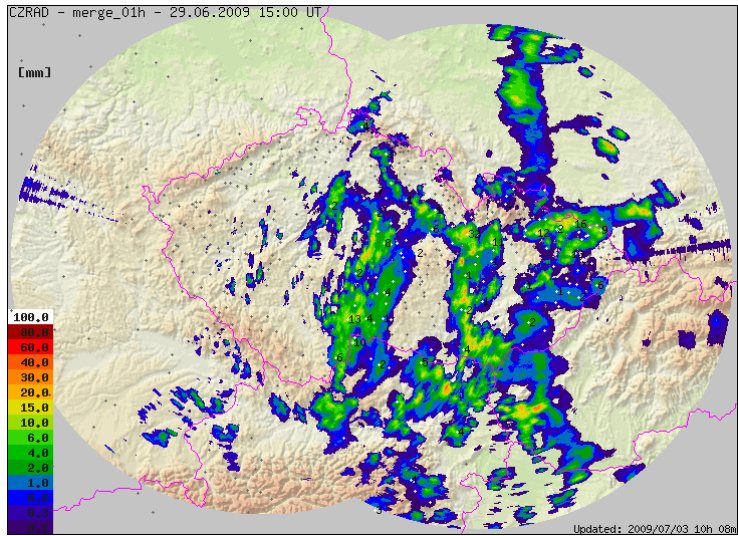


A first tuning of the unsaturated downdraught main parameters, with $LCSD=T$: GDDDP, TENTRD, TDDFR.

Diurnal cycle



Travel pictures



Travel pictures

