

# TOUCANS

- internal architecture of turbulence part

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# Stability functions $\chi_3$ , $\phi_3$

Fitted QNSE scheme:

$$\text{for } Ri \geq 0 \quad \chi_3(Ri) = \frac{1 + 0.75Ri(1 + a.Ri)}{1 + 3.23Ri(1 + a.Ri)} ,$$

$$\text{for } Ri < 0 \quad \chi_3(Ri) = \frac{1 - b.Ri}{1 - (b - 2.48).Ri} ,$$

$a = 13.0$ ,  $b = 4.16$  - tuning constants

Stability function  $\phi_3(Ri)$  is computed from quadratic equation derived in modified CCH02:

$$C_3 Ri \phi_3(Ri)^2 - \left[ \chi_3(Ri) + \frac{C_3 Ri}{Ri_{fc}} \right] \phi_3(Ri) + \chi_3(Ri) = 0$$







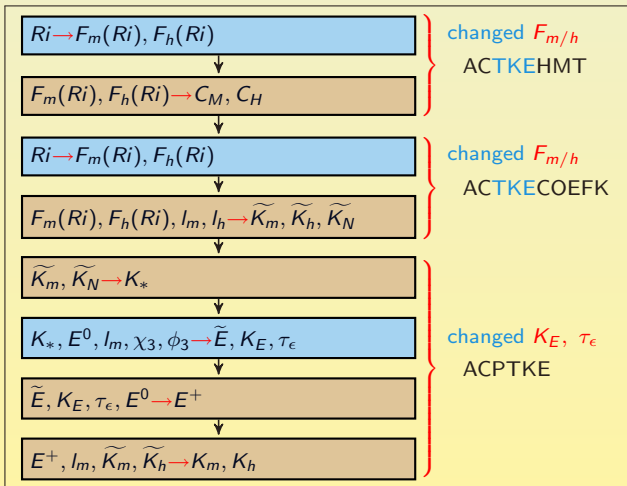
# Modification in $K_E$ , $\tau_\epsilon$

Relation for  $K_E$ ,  $\tau_\epsilon$  in eTKE:

$$\tau_\epsilon = \frac{l_m}{\nu^3 \sqrt{E}} \frac{\chi_3(Ri)^{\frac{3}{2}}}{f(Ri)^{\frac{3}{4}}}$$

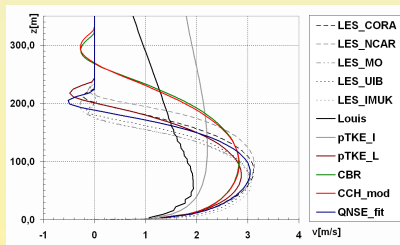
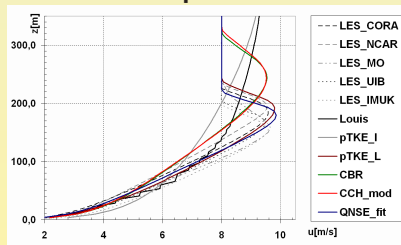
$$K_E = \frac{l_m \sqrt{E}}{\nu} \frac{f(Ri)^{\frac{3}{4}}}{\chi_3(Ri)^{\frac{3}{2}}}$$

## eTKE scheme - draft:



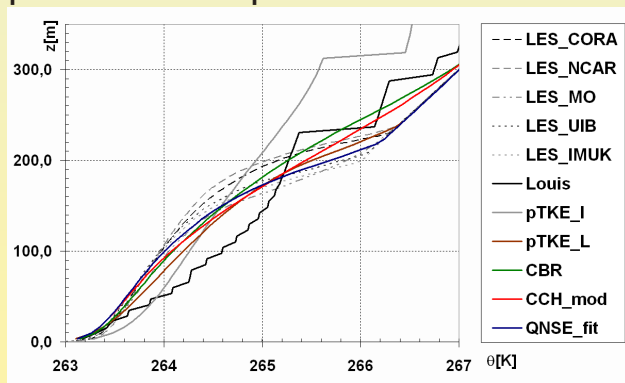
# 1D test: project GABLS

## wind components:



# 1D test: project GABLS

## potential temperature:



- inversion layer under top of PBL

# 'Dry' AF scheme

## Antifibrillation scheme

-to avoid nonlinear instabilities in diffusion equation

Decentered diffusion equation:

$$\frac{\partial \psi}{\partial t} = \frac{\psi^+ - \psi^0}{\Delta t} = \frac{\partial \left[ (1 - \beta) K_\psi \frac{\partial \psi^0}{\partial z} + \beta K_\psi \frac{\partial \psi^+}{\partial z} \right]}{\partial z}$$

$\beta$  - decentering factor

$\Delta t$  - timestep,  $t$  - time



# 'Dry' AF scheme

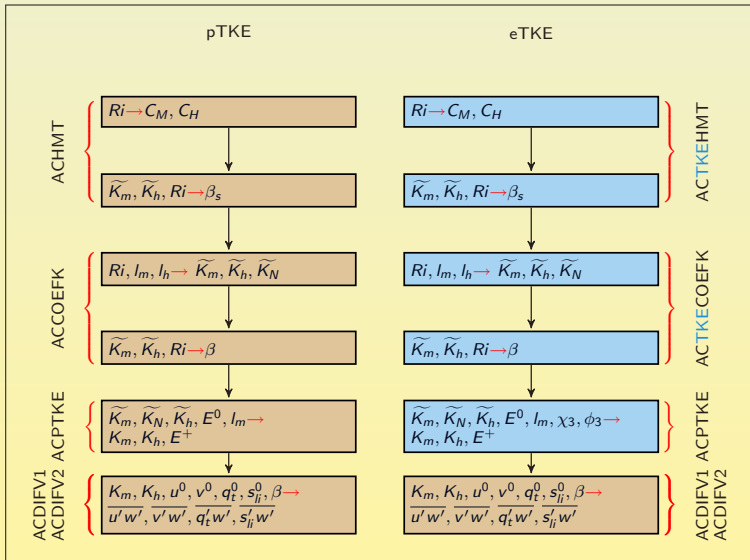
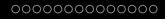
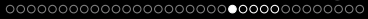
Conditions for use of 'dry' AF scheme  
are not fulfilled for all  $Ri$ :

$$K_m \geq \frac{K_h}{3} \quad \text{or} \quad \alpha_\theta > -1 \quad (\text{for } Ri > 0)$$

$$-2 < (\alpha_u, \alpha_\theta) < 1$$

$$2 < 3 - 2\alpha_u + \alpha_\theta$$

$$0 < 2 - 3\alpha_u + 2\alpha_\theta \leq 2$$



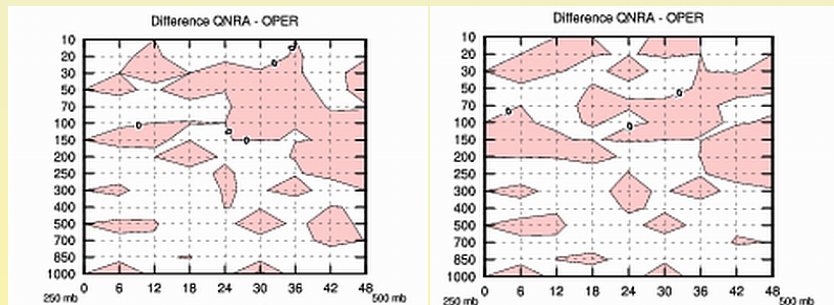








## 3D test: eTKE(QNSE) vs pTKE - relative humidity:



RMSE

STDEV

-red - better score for eTKE

# Mixing lengths

Prandtl-type mixing lengths  
(CGMIXLEN='AY', in ALARO0='CG'):

$$l_{m/h}^{AY} = \frac{\kappa Z}{1 + \frac{\kappa Z}{\lambda_{m/h}} \left[ \frac{1 + \exp\left(-a_{m/h} \sqrt{\frac{z}{H_{PBL}} + b_{m/h}}\right)}{\beta_{m/h} + \exp\left(-a_{m/h} \sqrt{\frac{z}{H_{PBL}} + b_{m/h}}\right)} \right]}$$

$\kappa$  - Von Kármán constant,  $H_{PBL}$  - PBL height

$a_{m/h}$ ,  $b_{m/h}$ ,  $\lambda_{m/h}$  - tuning constants

# Mixing lengths

TKE mixing lengths:

$$L^{BL}(E') = \left( \frac{L_{up}^{-\frac{4}{5}} + L_{down}^{-\frac{4}{5}}}{2} \right)^{-\frac{5}{4}},$$

$$L^N(E') = \sqrt{\frac{2E'}{N^2}},$$

$$E' = \alpha_{TKE} E.$$

$L_{up/down}$  - represents the distance that a parcel originating from the given level, and having initial kinetic energy equal to the scaled mean TKE of the layer, can travel upward(downward) before being stopped by buoyancy effects

$N$  - Brunt-Väisälä frequency

$\alpha_{TKE}$  - tunable degree of freedom











# Vertical profile of Prandtl number at neutrality

Solution with use of  $l_m^{AY}$ :

$$\frac{\lambda_m}{\lambda_h} = \frac{1}{C_3}$$

$$\frac{\beta_m}{\beta_h} = 1$$

Usage:

$$l_h = \frac{l_h^{AY}}{l_m^{AY}} l_m$$



We need to modify the code so, that there are no modification of exchange coefficients  $K_{m/h}$  after their calculation from stability functions  $F_{m/h}$ .

Currently there are two modifications:

- 'moist' AF scheme
- parametrisation of moist gustiness

# 'Moist' antibrillation scheme

Shallow convection parametrisation:

$$Ri^* = Ri_d + \frac{g}{c_p T} \frac{L_v \cdot \min \left[ 0, \frac{\partial(q - q_s)}{\partial z} \right]}{\left[ \frac{\partial u}{\partial z} \right]^2 + \left[ \frac{\partial v}{\partial z} \right]^2}$$

$q$  - specific moisture,  $q_s$  - specific moisture for saturated air

$L_v$  - latent heat of vaporization,  $c_p$  - specific heat capacity

$Ri_d$  - 'dry' (without shallow convection parametrisation)  $Ri$



# 'Moist' antibrillation scheme

We shifted 'moist' AF into computation of  $Ri$

Modification in stability functions  $F_{m/h}$  instead of  $K_{m/h}$ :

$$F_{m/h}(Ri') = F'_{m/h}(Ri, Ri^*) = F_{m/h}(Ri_d) + \frac{F_{m/h}(Ri^*) - F_{m/h}(Ri_d)}{1 + (\beta_m - 1)(F_{m/h}(Ri^*) - F_{m/h}(Ri_d))l_m l_h \sqrt{\left(\frac{\partial \bar{u}}{\partial z}\right)^2 + \left(\frac{\partial \bar{v}}{\partial z}\right)^2} \Delta t}$$



# 'Moist' antibrillation scheme

Special form of  $\chi_3$ ,  $\phi_3$  in modified CCH02  
derived by Daan Degrauwe:

$$\phi_3 = \frac{S - 1}{Ri_{fc} \cdot S - 1}$$

$$\chi_3 = \frac{\frac{S}{\sigma} - 1}{Ri_{fc} \cdot S - 1}$$

$$S = \frac{Ri_f}{Ri_{fc}} = \frac{1}{2} \left[ \sigma(1 + \rho) - \sqrt{(1 + \rho)^2 \sigma^2 - 4\rho\sigma} \right]$$

$$\sigma = \frac{R}{Ri_{fc}}, \quad \rho = \frac{C_3 Ri}{Ri_{fc}}$$

# 'Moist' antibrillation scheme

$$F_h = \phi_3 \sqrt{\chi_3 (1 - Ri_f)} = \frac{S - 1}{Ri_{fc} \cdot S - 1} \sqrt{\frac{S}{\sigma} - 1}$$

Inversion of  $F_h$  in modified CCH02:

$$0 = S^3 + ((F_h^2 Ri_{fc}^2 - 1) \sigma - 2) S^2 +$$

$$+ ((2 - 2 F_h^2 Ri_{fc}) \sigma + 1) S + (F_h^2 - 1) \sigma$$

$$Ri' = \frac{Ri_{fc}}{C_3} \frac{S}{\sigma} \frac{S - \sigma}{S - 1}$$

# 'Moist' antibrillation scheme

QNSE:

- unable to invert  $F_h$  analytically
- we fitted QNSE functions  $\chi_3$  ,  $\phi_3$   
in modified CCH02 :  
 $R, C_3$  - functions of  $Ri$ ,  $Ri_{fc} = 0.377$ ,  $\nu = 0.464$

# Moist gustiness modification

Gustiness:

$$\overline{w'\psi'} \sim \overline{\left[ \left( \frac{\partial u}{\partial z} \right)^2 + \left( \frac{\partial v}{\partial z} \right)^2 \right]^{\frac{1}{2}}}$$

$$\left[ \left( \frac{\partial \bar{u}}{\partial z} \right)^2 + \left( \frac{\partial \bar{v}}{\partial z} \right)^2 \right]^{\frac{1}{2}} < \overline{\left[ \left( \frac{\partial u}{\partial z} \right)^2 + \left( \frac{\partial v}{\partial z} \right)^2 \right]^{\frac{1}{2}}}$$

*NWP model*

# Moist gustiness modification

## Moist gustiness

-induced by moist convection:

$$K_{m/h}^{PRC} = \gamma^{PRC} K_{m/h}, \quad C_{M/H}^{PRC} = \gamma^{PRC} C_{M/H}$$

$$\gamma^{PRC} = \sqrt{1 + \left( \left( \frac{J_{Pr}}{J_{Pr} + J_{Pr}^0} \right)^\gamma \tilde{U} \right)^2 \frac{\rho}{J_m}}$$

$J_{Pr}$  - precipitation flux,  $J_{Pr}^0$  - typical steadily strong precipitation flux

$J_m$  - momentum flux:

above surface =  $\rho \cdot K_m \cdot \sqrt{\left( \frac{\partial \bar{u}}{\partial z} \right)^2 + \left( \frac{\partial \bar{v}}{\partial z} \right)^2}$ , surface =  $\rho \cdot C_M \cdot (\bar{u}^2 + \bar{v}^2)$

$\tilde{U}$  - typical surface friction velocity,  $\gamma = 0.8$  - tuning constant

# Moist gustiness modification

We shifted moist gustiness  
in to the computation of  $I_{m/h}$ :

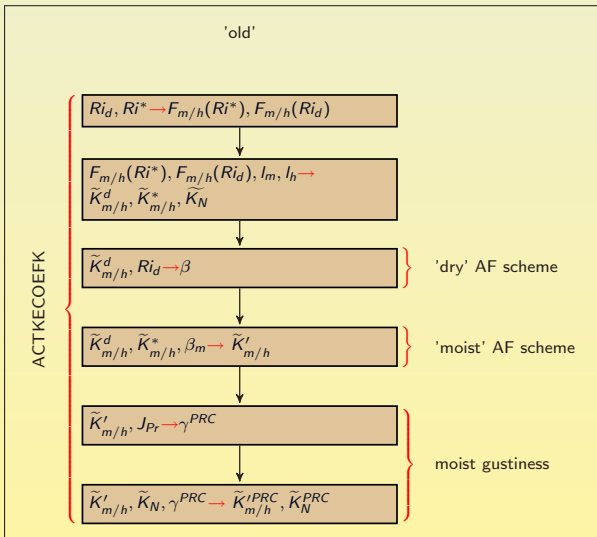
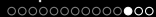
$$I_{m/h}^{PRC} = \sqrt{\gamma^{PRC}} I_{m/h}$$

$$K_{m/h} \sim I_{m/h} I_m$$

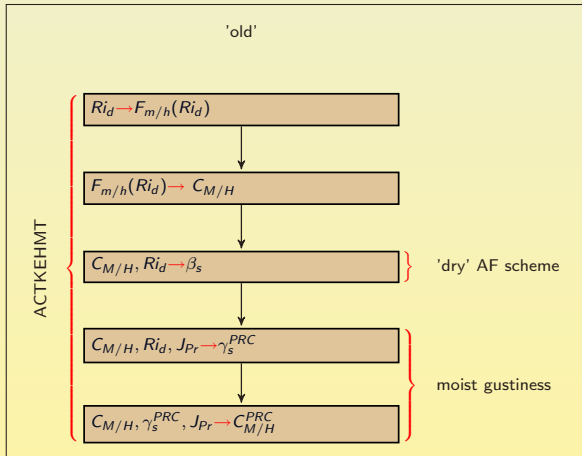
# Mixing lengths

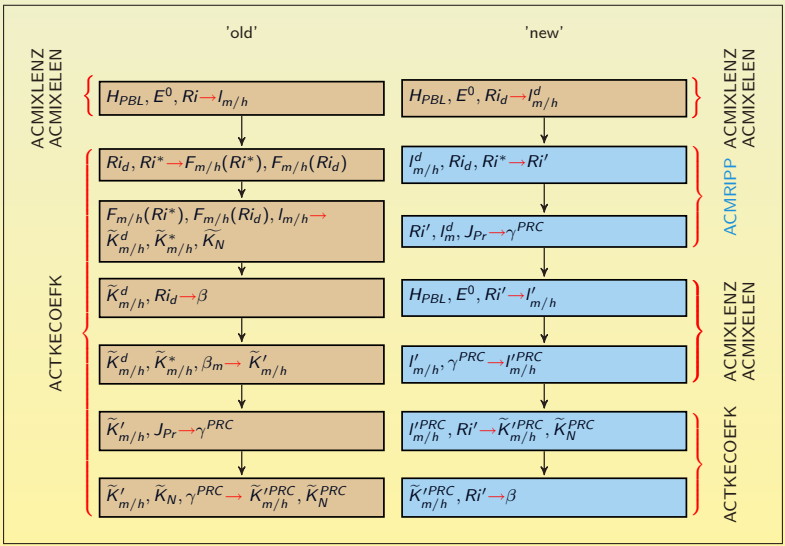
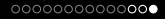
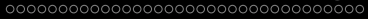
New 'moist' AF scheme (with  $Ri'$ ) and moist gustiness par. influence mixing lengths  $l_{m/h}$ , but  $l_{m/h}$  are also inputs for them.

To avoid iterative methods we simply use  $l_m^d$  (without 'moist' AF scheme and 'moist' gustiness) in both schemes.









# Shallow convection cloudiness

$Ri'$  should be limited by:

$Ri_d$  (no clouds in grid box) and

$Ri_m$  (Richardson number for saturated air  
- 100 % cloudiness in grid box):

$$Ri_m = g \frac{1 + \frac{L_v \cdot q_w}{R \cdot T}}{1 + \left( \frac{\frac{R_d}{R_v} \cdot L_v^2 \cdot q_w}{c_p \cdot R \cdot T^2} \right)} \left( \frac{d \ln \theta}{dz} + \frac{L_v}{c_p \cdot T} \frac{dq_w}{dz} \right) \frac{1}{\left( \frac{\partial \bar{u}}{\partial z} \right)^2 + \left( \frac{\partial \bar{v}}{\partial z} \right)^2}$$

$q_w$  - specific moisture corresponding to wet bulb temperature

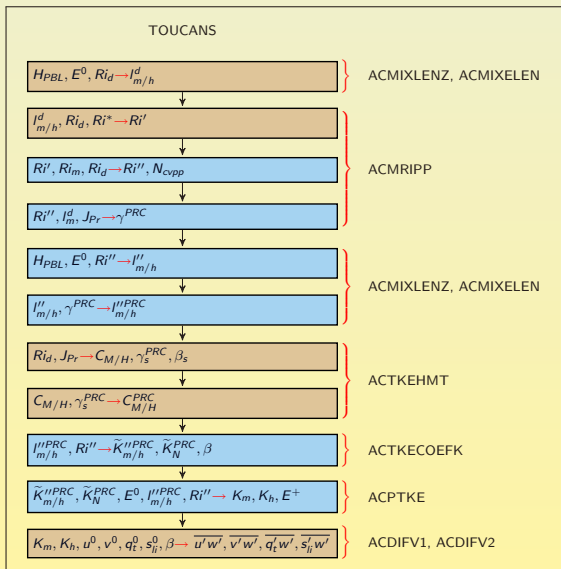
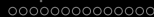
$R_d$  - gas constant for dry air,  $R_v$  - gas constant for water vapor

# Shallow convection cloudiness

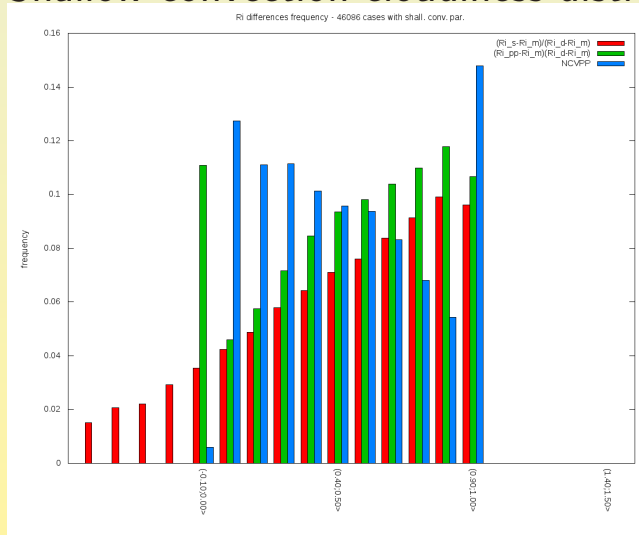
Shallow convection cloudiness  $N_{cvpp}$ :

$$N_{cvpp} = \frac{Ri'' - Ri_d}{Ri_m - Ri_d}$$

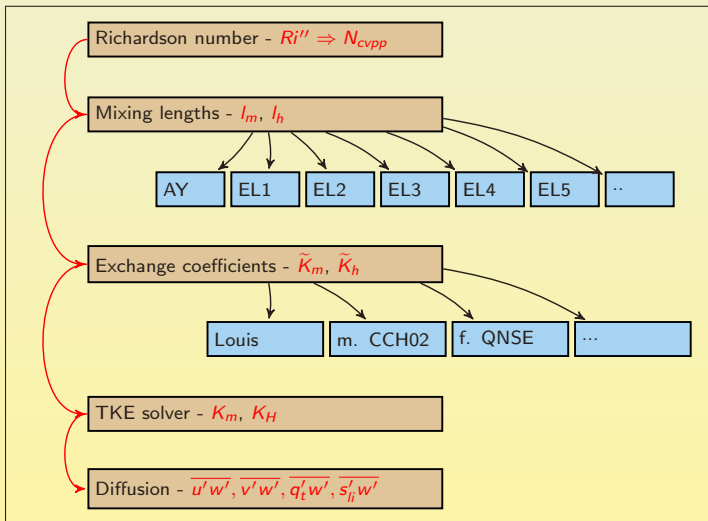
$$Ri'' = \min(\max(Ri_d, Ri'), Ri_m)$$



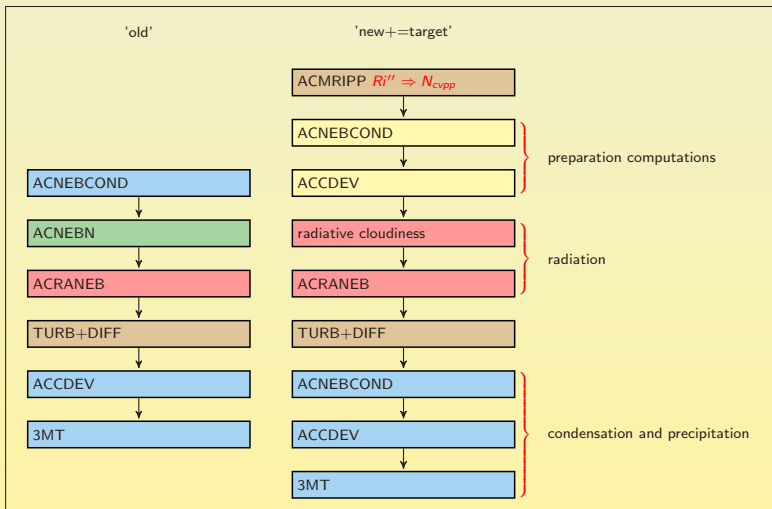
# Shallow convection cloudiness distribution:



# Internal modularity



# External identification





# Summary

- New turbulent scheme:
  - equivalence with full TKE scheme
  - easy implementation
    - (new stability functions  $F_{m/h}$ )
  - modified TKE solver
  - modified 'dry' AF scheme
- Mixing lengths from TKE
- Preparations for TOMs:
  - modification in 'moist' AF scheme
  - modification in moist gustiness par.
- Shallow convection cloudiness
  - computation
  - used in cloudiness computations

Thank you for your attention!